

USARTL TR-78-23D INTERACTIONAL AERODYNAMICS OF THE SINGLE ROTOR HELICOPTER CONFIGURATION VOLUME IV-G. One-Third Octave Band Spectrograms of Wake Split-Film Data, Fairings and Surface Devices Philip F./Sheridan **Boeing Vertol Company** P.O. Box 16858 Philadelphia, Pa. 19142 9 9 Final Report, for Period March 777 - February 778 Approved for public release; distribution unlimited. 95 DAAJØ2-77-C-ØØ2Ø 16 11262209AH76 Prepared for APPLIED TECHNOLOGY LABORATORY U. S. ARMY RESEARCH AND TECHNOLOGY LABORATORIES (AVRADCOM) Fort Eustis, Va. 23604 79 01 08 031

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#### APPLIED TECHNOLOGY LABORATORY POSITION STATEMENT

In 1975 a wind tunnel test program was conducted in the Boeing-Vertol 20-foot V/STOL Wind Tunnel on a 1/5th-scale UTTAS model to investigate and find solutions for several aerodynamic problems encountered during the UTTAS flight-testing. Specifically, these tests focused upon (a) the structure of the hub/rotor wake in the vicinity of the empennage, (b) the formulation of the ground vortex and its relation to hub loads and fuselage loads during transition, and (c) the occurrence of vibratory air pressures from the blade passing over the fuselage. Only portions of the above-mentioned wind tunnel test data were reduced and analyzed in addressing the flight-test problems of the UTTAS aircraft.

Under Contract DAAJ02-77-C-0020, Boeing-Vertol completed analyses on the data to understand more completely the aerodynamic interactions that are involved and to formulate instructions for the guidance of designers in these respects. The results of these studies are applicable to all existing and future single-rotor/tail rotor helicopters. The data have been segregated according to aerodynamic interactions and associated phenomena/problem areas. From this body of knowledge, a generalized set of design guidelines meaningful to the single-rotor helicopter design concept formulation were developed and are included in these reports.

Mr. Robert P. Smith of the Aeronautical Technology Division, Aeromechanics Technical Area, served as project engineer for this effort.

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## **PREFACE**

The entire report describing the investigation of INTERACTIONAL AERODYNAMICS OF THE SINGLE-ROTOR HELICOPTER CONFIGURATION comprises eight numbered volumes bound as 33 separate documents. The complete list of these documents is as follows:

Volume I, Final Report

Volume II, Harmonic Analyses of Airframe Surface Pressure Data

- A Runs 7-14, Forward Section
- B Runs 7-14, Mid Section
- C Runs 7-14, Aft Section
- D Runs 15-22, Forward Section
- E Runs 15-22, Mid Section
- F Runs 15-22, Aft Section
- G Runs 23-33, Forward Section
- H Runs 23-33, Mid Section
- I Runs 23-33, Aft Section

Volume III, Flow Angle and Velocity Wake Profiles in Low-Frequency Band

- A Basic Investigations and Hubcap Variations
- B Air Ejector Systems and Other Devices

Volume IV, One-Third Octave Band Spectrograms of Wake Split-Film Data

- A Buildup to Baseline
- B Basic Configuration Wake Explorations
- C Solid Hubcaps
- D Open Hubcaps
- E Air Ejectors
- F Air Ejectors With Hubcaps; Wings
- G Fairings and Surface Devices

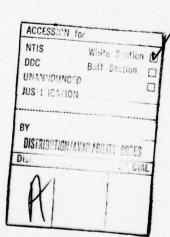
Volume V, Harmonic Analyses of Hub Wake

Volume VI, One-Third Octave Band Spectrograms of Wake Single Film Data

- A Buildup to Baseline
- B Basic Configuration Wake Exploration
- C Hubcaps and Air Ejectors

Volume VII, Frequency Analyses of Wake Split-Film Data

- A Buildup to Baseline
- B Basic Configuration Wake Explorations
- C Solid Hubcaps



Open Hubcaps D

E Air Ejectors

Air Ejectors With Hubcaps; Wings Fairings and Surface Devices F

G

Volume VIII, Frequency Analyses of Wake Single Film Data

Buildup to Baseline A

В Basic Configuration Wake Exploration

Hubcaps and Air Ejectors C

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#### INTRODUCTION

Volume IV presents spectrograms of the flow angles and velocity components for each run and its test points. Specifically, these machine plots show the root mean square value of each wake parameter over discrete frequency intervals one-third of an octave band in width. The octave arrangement is selected to provide 19 spectral increments from 3.9 to 250.0 Hz centerband frequency. A special computer program is employed to derive wake parameters within these bands consistent with corresponding basic spectral functions depicted in Volume VII.

The graphs showing the one-third octave band values are sequenced in the same order as the Outline of Wake Investigations (Table 1). These graphs are distributed among Volumes IV-A through IV-G by the major categories of Table I in the following arrangement:

Volume IV-A	Build-up to Baseline
Volume IV-B	Basic Configuration
Volume IV-C	Effect of Hub Caps Section 1 & 2
Volume IV-D	Effect of Hub Caps Section 3 & 4
Volume IV-E	Effect of Hub Caps Section 5 and
	Effect of Air Ejectors
Volume IV-F	Air Ejectors with Open Hub Caps and
	Effect of Wings and Misc. Section
Volume IV-G	Effect of Wings and Misc. Sections
	2 and 3

The Table I outline and other material is included for reference and as a context to the work of each sub-volume. Table 2, the List of Test Runs, arranges the runs in numerical order and gives pertinent text parameters.

The Index of Rake Positions, Table 3, lists the hot film transducer rake positions in the model coordinate system for each run and its test points. The main feature of Table 3 is the indexing of the test point number to the model waterline station and butt line as it varied from run to run. The table groups the runs as they shared the indexing correspondence of point with position. It is emphasized that the runs in a group do not necessarily all share the same number of test points but they do have same correspondence within their respective ranges of test points.

The orientation of the rake is shown pictorially in Figures 1 through 6 for the various test runs. Figure 7 presents a scaled drawing of the model with reference to the three-axis coordinate system. Table 4 lists the center frequency and the upper and lower band limits for each of the numbered one-third octave bands.

TABLE 1			
OUTLINE OF WAKE IN	VESTIGATIONS		
Description	Configuration Code		Base- line
Build-up to Baseline	LOUIS CONTRACTOR PRO		
1. Nacelles removed	K <sub>13</sub> +H <sub>1</sub> -N	149	150
2. Blades off, rotating hub	K <sub>13</sub> -M+H <sub>1.0</sub>	160	156
3. " , non-rotating hub	K <sub>13</sub> -M+H <sub>1.0</sub>	158	156
4. " ", hub off	K <sub>13</sub> -M-H <sub>1.0</sub>	159	156
Basic Configuration			
1. Wake Explorations near Empennage			
(a) 15" Long. + traverse at T/R C.L.	K <sub>11</sub>	111	
(b) 9" Vert. + " above T/R " (c) 2" " in vortex	"	112	
(d) 8" " (continue 112)	п	114	
(e) 13" " behind stab. (f) Lateral traverse, left stab.	11	115	
(One T.P. only)			
(g) Same continued (h) Same continued (One T.P. only)	"	117	
(i) Lateral traverse right stab.	" 0	119	
(j) T/R effect on wake	$K_{11}+T_2^0$	121	115
2. Climb/Descent Studies			
(a) Climb 900 FPM (b) Descent 800 FPM	K <sub>1 1</sub>	135 136	
Effect Of Hub Caps			
1. Solid Caps on Canister			
(a) 7.6" diam. 2.17" ht. soft	K <sub>11</sub> -H <sub>1.0</sub> +H <sub>1.2</sub>	137	136
(b) 7.6" diam. 2.17" ht. stiff	K <sub>13</sub> +H <sub>1.2</sub>	153	156
Pitch Arms (b) 7.6" diam. 2.45" ht. flt. test config.	K <sub>13</sub> +H <sub>1-2-1</sub> +I <sub>1</sub> +E <sub>1.0</sub>	207	188

# TABLE 1 (CONTINUED)

# OUTLINE OF WAKE INVESTIGATIONS

OUTLINE OF WAKE INVE	STIGATIONS		
Description	Configuration Code*	Run No.	Base- line
Effect of Hub Caps (Continued)	2007		
2. Solid Caps Raised Above Canister	District 1		
(a) 7.6" diam. 2.45" ht. 70"	H <sub>1.2.2</sub> +I <sub>1</sub> +E <sub>1.0</sub>	208	188
depth, .55 gap (b) 10.0" diam. 3.25" ht. 1.55" depth, .50" gap	H <sub>1.8.1</sub> +I <sub>1</sub> +E <sub>1.0</sub>	189	188
(c) 10.0" diam. 4.125" ht.	H <sub>1.8.2</sub> +I <sub>1</sub> +E <sub>1.0</sub>	190	. 188
2.05" depth, .875" gap (d) Repeat of 189		210	188
3. Open Caps Without Underbody			
(a) 10.0" diam. 1.25" gap,blades (b) " " " gap, no blades	H <sub>1</sub> ·0·2+I <sub>1</sub> +E <sub>1</sub> ·0	193 166	188/166 158
	H <sub>1.0.1</sub> -H <sub>1.0</sub> +E <sub>1.0</sub>	211 165	188 158
	H <sub>1</sub> · 7 · 1 - M	191 168 167	188 156/167 -158
(h) " " 4.00" gap,blades	H <sub>1.7.2</sub>	169	156
4. Open Caps with Underbody			
(a) 7.6" diam. 1.25" gap (b) " " " " center	H <sub>1.11.1</sub> +I <sub>2</sub> +E <sub>1.0</sub> H <sub>1.11.1</sub> +I <sub>2</sub> +E <sub>4.0</sub> H <sub>1.11.2</sub> +I <sub>2</sub>	194 198 202	188 188 194
(d) 10.0" diam5" gap, no	H <sub>1.5.1</sub> -M	164	158
blades (e) " " 1.25" gap, no	H <sub>1.5.2</sub> -M	161	158
blades (f) " " 2.0" gap, no	H <sub>1.5.4</sub> -M	163	158
(g) " " 4.0" gap, no	H <sub>1.5.3</sub> -M	162	158
blades		1	1

# TABLE 1 (CONTINUED)

# OUTLINE OF WAKE INVESTIGATIONS

Description	Configuration Code*	Run No.	Base- line
5. Miscellaneous Hub Covers  (a) Hub fairing 16" diam. (b) Wham-O-Frisbee 10" diam. (c) Fab. glass Frisbee 16" diam.	H <sub>1.3</sub> H <sub>1.9.0</sub> +E <sub>1.2</sub> H <sub>1.9.1</sub> +E <sub>1.2</sub>	151 182 183	150 181 181
Effect of Air Ejectors			
1. Basic system no blowing 2. " " 40 psi 3. " " 150 psi 4. Wide chord shroud 40 psi 5. Wide " " 150 psi 6. W/C shroud w. lip 40 psi 7. Same Contoured Parallel 150 psi 8. Bifurcated duct 0 psi 9. " " 40 psi 10. " " 150 psi	H <sub>1.0</sub> +E <sub>1.0</sub> H <sub>1.0</sub> +E <sub>2.5.1</sub> H <sub>1.0</sub> +E <sub>3.5.2</sub> H <sub>1.0</sub> +E <sub>3.5.4</sub> 1.0  1.0  1.0  1.0  1.0  1.0  1.0  1.	174 175 176 184 187 203 204	156 156/172 156/173 156/174 156/173 156/174 156 156/203 156/203
Air Ejectors with Open Hub Caps with Underbodies			
1. 7.6" diam. 1.25" gap, 0 psi 2. " " " 20 psi 3. " " " 40 psi 4. " " " 150 psi 5. " " " 40 psi 6. " " " 40 psi 7. " " 150 psi	H <sub>1.11.1</sub> +I <sub>2</sub> +E <sub>4.0</sub> H <sub>1.11.2</sub> +I <sub>2</sub> +E <sub>4.6</sub>	195 196 197 198 199 200	188/172 188 188/173 188/174 188/194 188/196 188/196 188/200 156/176
Effect of Wings and Misc.			
1. Wings  (a) Nacelle-mounted stub wing  (b) Single slotted flapped wing  (c) Dougle slotted flapped wing  (d) Boom-mounted stub wing	H <sub>1.0</sub> +W <sub>1.0</sub> +E <sub>1.1</sub> H <sub>1.0</sub> +W <sub>3.0</sub> +E <sub>1.0</sub> H <sub>1.0</sub> +W <sub>2.0</sub> +E <sub>1.0</sub> H <sub>1.0</sub> +W <sub>4.0</sub>	178 180 179 186	181 181 181 156
*Basic Code is Kl3.			

TABLE 1 (CONTINUED)

# OUTLINE OF WAKE INVESTIGATIONS

	Description	Configuration Code*	Run No.	Base- line
2.	Crown Fairings  (a) Flat top behind shaft  (b) Round top behind shaft  (c) Extended flat top fairing  (d) Flat top + 16" cap, 4" gap  (e) Forward fairing/nacelle fairing	K <sub>11+D1</sub> K <sub>11+D2</sub> H <sub>1+D4</sub> H <sub>1·7·2+D4</sub> P <sub>1·0</sub>	-140 141 170 171 152	138 138 156 170 156
3.	Surface Devices (a) Vortex generators (b) Guidevane between nacelles (c) Longitudinal strakes (d) 14% porosity spoiler	K <sub>11</sub> +VG <sub>2.1</sub> K <sub>11</sub> +FV <sub>1</sub> H <sub>1•5.3</sub> +S <sub>4</sub> K <sub>11</sub> +X <sub>1</sub>	139 142 155 143	138 138 156 138

\*Basic Code is Kl3 unless noted otherwise.

	TAIL	ROTOR	Off	=	=	=	=	=	=	=	=	u <sub>O</sub>	) J J O E E	=
	MR HT.	p/q	8			=	=	=	=	=	=	=		5
	MODEL	0 1	-2.0		u		=	=	=	=	=	=	-4.5	-2.0
	MODEL	οD	0.9	u	B	H.	=	=	=	8	=	=	0.9-	0.9
AKE	DISK	LDG. psf	8	u	u		=	=			=		=	=
US HE HUB W	RPM	MR/TR	1433/0	н	н	н	=	=			=	1433/ 4500	=	F
2 TEST RUN	VTUN	KNOTS	80	н			=		п		=	=	=	=
TABLE 2  LIST OF TEST RUNS  BASIC INVESTIGATIONS OF THE HUB WAKE	CONFIGURATION		$K_{11}/15$ " Long. wake traverse at TR center line	" /9" Vert. wake traverse above TR ænter line	" /2" Vert traverse through MR vortex	" /8" Vert. traverse below TR center line	" /13" Vert. traverse behind stabilizer	" /Lateral traverse - left stabilizer	" /116 continued	" /116 continued	" /Lateral traverse - right stabilizer	K <sub>11</sub> +T <sub>2</sub> /Effect of tail rotor flow on wake	$K_{11}/W$ ake in 900 fpm climb	" /Wake in 800 fpm descent
	RUN	NO.	111	112	113	114	115	116	117	118	119	121	135	136

<del></del>		TABLE 2 (CONTINUED)  LIST OF TEST RUNS  EVALUATION OF WAKE-ALTERING DEVICES	(CONTINUED) TEST RUNS KE-ALTERIN	) IS ING DEVIC	CES		2 9		
K11-H1.0+H1.2/Effect of 7.6 inch diam. solid hub cap K11/Repeat of base run A11+VG2.1/Effect of vortex generators on aft crown K11+D1/Flat-topped "doghouse" fair- ing on aft crown K11+FV1/Deflection vane on crown between nacelles K11+X1/Variable porosity spoiler K13+H1-N1/Effect of nacelles off also A13+H1-N1/Effect of nacelles off also K13+H1,3/16 inch diam. helmet fair- ing K13+H1.3/16 inch diam. helmet fair- ing K13+H1.2/Repeat 137 with K13 pitch arms	RUN	CONFIGURATION/CONDITTION	VTUN	RPM	DISK	MODEL	MODEL	MR HT.	TAIL
K11-H1.0+H1.2/Effect of 7.6 in diam. solid hub K11/Repeat of base run K11+VG2.1/Effect of vortex gen ators on aft crown K11+D1/Flat-topped "doghouse"  K11+D2/Rounded-top fairing K11+FV1/Deflection vane on crobetween nacelles K11+X1/Variable porosity spoil K13+H1-N1/Effect of nacelles of add stiff pitch arms (K13) K13+H1.3/16 inch diam. helmet K13+H1.3/16 inch diam. helmet K13+H1.3/16 inch diam. helmet K13+H1.3/16 with K13 pitch	NO.		KNOTS	MR/TR	rng.	9	0	p/q	ROTOR
K <sub>11</sub> /Repeat of base run  K <sub>11</sub> +VG <sub>2</sub> .1/Effect of vortex gen  K <sub>11</sub> +D <sub>1</sub> /Flat-topped "doghouse"  K <sub>11</sub> +D <sub>2</sub> /Rounded-top fairing  K <sub>11</sub> +FV <sub>1</sub> /Deflection vane on cro  K <sub>11</sub> +K <sub>1</sub> /Variable porosity spoil  K <sub>13</sub> +H <sub>1</sub> -N <sub>1</sub> /Effect of nacelles off a stiff pitch arms (K <sub>13</sub> )  K <sub>13</sub> +H <sub>1</sub> /60 knot baseline  K <sub>13</sub> +H <sub>1</sub> .3/16 inch diam. helmet  K <sub>13</sub> +H <sub>1</sub> .0/Pylon and intake fair  K <sub>13</sub> +H <sub>1</sub> .2/Repeat 137 with K <sub>13</sub> pitch	137	2/Effect diam.	80	1433/0	8	9	-3.8	8	Off
Kll+VG2.1/Effect of vortex gen ators on aft crown Kll+Dl/Flat-topped "doghouse" ing on aft crown Kll+D2/Rounded-top fairing Kll+Yl/Deflection vane on cro between nacelles Kll+Xl/Variable porosity spoil Kl3+Hl-Nl/Effect of nacelles off a Kl3+Hl/60 knot baseline Kl3+Hl/60 knot baseline Kl3+Hl.3/16 inch diam. helmet ing Kl3+Pl.0/Pylon and intake fair Kl3+Hl.2/Repeat 137 with Kl3 pitch	138	K <sub>11</sub> /Repeat of base run		=	=	•			•.
K <sub>11</sub> +D <sub>1</sub> /Flat-topped "doghouse" ing on aft crown  K <sub>11</sub> +D <sub>2</sub> /Rounded-top fairing  K <sub>11</sub> +FV <sub>1</sub> /Deflection vane on cro between nacelles  K <sub>11</sub> +X <sub>1</sub> /Variable porosity spoil  K <sub>13</sub> +H <sub>1</sub> -N <sub>1</sub> /Effect of nacelles off a action stiff pitch arms (K <sub>13</sub> )  K <sub>13</sub> +H <sub>1</sub> /60 knot baseline  K <sub>13</sub> +H <sub>1</sub> , 3/16 inch diam. helmet ing  K <sub>13</sub> +H <sub>1</sub> , 3/16 inch diam. helmet ing	139	K <sub>11</sub> +VG <sub>2,1</sub> /Effect of vortex gener- ators on aft crown	=	=	=	=	=	=	-
K <sub>11</sub> +D <sub>2</sub> /Rounded-top fairing  K <sub>11</sub> +FV <sub>1</sub> /Deflection vane on crobetween nacelles  K <sub>11</sub> +X <sub>1</sub> /Variable porosity spoil  K <sub>13</sub> +H <sub>1</sub> -N <sub>1</sub> /Effect of nacelles off add stiff pitch arms (K <sub>13</sub> )  K <sub>13</sub> +H <sub>1</sub> /60 knot baseline  K <sub>13</sub> +H <sub>1</sub> ,3/16 inch diam. helmet ing  K <sub>13</sub> +P <sub>1</sub> ,0/Pylon and intake fair  K <sub>13</sub> +H <sub>1</sub> ,2/Repeat 137 with K <sub>13</sub> pitch	140	"doghouse" rown	=	=	=	=	=		=
Kll+FVl/Deflection vane on crobetween nacelles  Kll+Xl/Variable porosity spoil  Kl3+Hl-Nl/Effect of nacelles off a  Kl3+Hl/60 knot baseline  Kl3+Hl.3/16 inch diam. helmet  Kl3+Hl.3/16 inch diam. helmet  Kl3+Hl.0/Pylon and intake fair  Kl3+Hl.2/Repeat 137 with Kl3 pitch	141			=	=		=		=
K <sub>13</sub> +K <sub>1</sub> /Variable porosity spoil  K <sub>13</sub> +H <sub>1</sub> -N <sub>1</sub> /Effect of nacelles off a  K <sub>13</sub> +H <sub>1</sub> /60 knot baseline  K <sub>13</sub> +H <sub>1</sub> ,3/16 inch diam. helmet  K <sub>13</sub> +P <sub>1</sub> ,0/Pylon and intake fair  K <sub>13</sub> +H <sub>1,2</sub> /Repeat 137 with K <sub>13</sub> pitch	142	vane on	=	=	=	•	=		
K <sub>13</sub> +H <sub>1</sub> -N <sub>1</sub> /Effect of nacelles off a stiff pitch arms (K <sub>13</sub> )  K <sub>13</sub> +H <sub>1</sub> /60 knot baseline  K <sub>13</sub> +H <sub>1</sub> .3/16 inch diam. helmet  K <sub>13</sub> +P <sub>1</sub> .0/Pylon and intake fair  K <sub>13</sub> +H <sub>1,2</sub> /Repeat 137 with K <sub>13</sub> pitch	143	porosity			<b>.</b> .		=		
K <sub>13</sub> +H <sub>1</sub> /60 knot baseline  K <sub>13</sub> +H <sub>1.3</sub> /16 inch diam. helmet ing  K <sub>13</sub> +P <sub>1.0</sub> /Pylon and intake fair  K <sub>13</sub> +H <sub>1.2</sub> /Repeat 137 with K <sub>13</sub> pitch	149		. 09	1075/0	4.5		=		=
K <sub>13</sub> +H <sub>1.3</sub> /16 inch diam. helmet ing K <sub>13</sub> +P <sub>1.0</sub> /Pylon and intake fair K <sub>13</sub> +H <sub>1.2</sub> /Repeat 137 with K <sub>13</sub> pitch	150	$K_{13}+H_{1}/60$ knot baseline	•			:			
	151	inch diam. helmet	=	=	=		2		=
	152	and intake	80	1433/0	8	=	=		
	153	$K_{13}^{+H}_{1.2}$ /Repeat 137 with $K_{13}$ pitch arms		=					=

ROTOR Off = = = = = = HT. h/d 8 = = = = = = = = = = -3.8 0 ANGLES = = = = = = = = = = MODEL 0 9 = = = = = = = DISK LDG. psf œ = = = = = = = = EVALUATION OF WAKE-ALTERING DEVICES RPM MR/TR 1433/0 1433/0 0/0 0/0 = = = = = = LIST OF TEST RUNS TABLE 2 (CONTINUED) KNOTS VTUN 80 = = = = = = = K<sub>13</sub>-M+H<sub>1.0</sub>/Same as 158 except hub is rotating K<sub>13</sub>-M-H<sub>1.0</sub>/Wake studies with hub of K<sub>13</sub>-M+H<sub>1.0</sub>/Wake studies with blades K<sub>13</sub>-M+H<sub>1.0.1</sub>/10" open hub cap, no underbody, same cap vert.position as Run 154 K<sub>13</sub>-M+H<sub>1.5.2</sub>/Repeat of 154 without blades K<sub>13</sub>-M+H<sub>1.5.3</sub>/Same as 161 except 4" strakes on aft crown 5 K13-M+H1.0.2/Same as 165 with cap K<sub>13</sub>+H<sub>1.5.2</sub>+S<sub>4</sub>/Same as 154 except off, hub not rotating K13+H1.0/Baseline with K13,i.e., 161 except K<sub>13</sub>-M+H<sub>1.5.1</sub>/Same as 161 except 0.5" gap Kl3+Hl.5.2/10" open hub cap, 7" underbody, 1.25" gap CONFIGURATION/CONDITION lowered by 0.5" stiff pitch arms as K<sub>13</sub>-M+H<sub>1.5.4</sub>/Same 156 154 158 160 164 165 166 155 159 162 163 161 RUN NO.

	TAIL		Off	•	=				•		•			
	MR HT.	p/q	8	=	=	•	:	•	•	=	•		=	:
	MODEL	• 1	-3.8	=	=	=	=		=				=	=
	ANG	° g	9	:	=	•	-	=	=	:	:		=	=
Š	DISK	pst pst	∞	=	-	u		=	=	•		=	•	:
NS G DEVICE	RPM	MR/TR	0/0	1433/0			u					-		
(CONTINUED) TEST RUNG -ALTERING	VTUN	KNOTS	- 80	=	=				•		•			
TABLE 2 (CONTINUED)  LIST OF TEST RUNS  EVALUATION OF WAKE-ALTERING DEVICES	CONFIGURATION		K <sub>13</sub> -M+H <sub>1.7.1</sub> /16" open cap, no underbody, 2" gap	K <sub>13</sub> +H <sub>1,7,1</sub> /Blades on, same cap config. as 167	K <sub>13</sub> +H <sub>1,7,2</sub> /16" open cap, no under- body, 4" gap	K <sub>13</sub> +H <sub>1.0</sub> +D <sub>4.0</sub> /Extended flat top fairing on aft crown	K <sub>13</sub> +H <sub>1.7.2</sub> +D <sub>4.0</sub> /Same fairing as 170 same cap as 169	K <sub>13</sub> +H <sub>1,0</sub> +E <sub>1,0</sub> (0psi)/Basic air ejector zero blowing baseline	K <sub>13</sub> +H <sub>1.0</sub> +E <sub>1.0</sub> (40 psi)/Same as 172 with 40 psi supply	$K_{13}^{+H_1,0}^{+E_1,0}(150 \text{ psi})/\text{Same as } 172$ with 150 psi supply	K13+H1,0+E2,5,1(40 psi)/Ejector with wide chord shroud at 40 psi	K <sub>13</sub> +H <sub>1.0</sub> +E <sub>2.5.1</sub> (150 psi)/Same as 174 with 150 psi supply	$K_{13}^{+H_1.5}_{176}$ with 10" cap like 163	K <sub>13</sub> +H <sub>1.0</sub> +W <sub>1.0</sub> +E <sub>1.1</sub> (0 psi)/Nacelle mounted wing
	RUN	NO.	167	168	169	170	171	172	173	174	175	176	177	178

		TAIL		Off	•		•	•	=	=	•	•	•	=	:
		MR HT.	p/q	8	=	:	=	:	•	=	-	•		=	=
		MODEL	. 4	-3.8			•	=	=	=	=		=	=	=
		MOL	• B	9	=	=	=	=	=	=	=			=	=
	ι.	DISK	pst.	8	=				=					=	
SI	3 DEVICE	RPM	MR/TR	1433/0	=	=	=		=	=	=			=	
TEST RUN	ALTERING	VTUN	KNOTS	80	=	=		:	=						
LIST OF TEST RUNS	EVALUATION OF WAKE-ALTERING DEVICES	CONFIGURATION		K <sub>13</sub> +H <sub>1.0</sub> +W <sub>2.0</sub> +E <sub>1.0</sub> (0 psi)/Double slotted flapped wing	K <sub>13</sub> +H <sub>1.0</sub> +W <sub>3.0</sub> +E <sub>1.0</sub> (0 psi)/Single slotted flapped wing	Kl3+Hl.0+El.2 (0 psi)/Baseline with ejector tube moved aft	K <sub>13</sub> +H <sub>1.9.0</sub> +E <sub>1.2</sub> (0 psi)/Standard 10" frisbee	K <sub>13</sub> +H <sub>1.9.1</sub> +E <sub>1.2</sub> (0 psi)/16" fabri- cated frisbee	Kl3+Hl.0+E3.5.2 (40 psi)/Wide chord with lip at 40 psi	i)/ 15(	Kl3+Hl.0+W4.0/Boom mounted stub wing	Kl3+Hl.0+E3.5.4 (150 psi)/Like 185 with modified shroud	K <sub>13</sub> +H <sub>1.0</sub> +I <sub>1</sub> +E <sub>1.0</sub> (0 psi)/Baseline with I, instr. ring	0 .	
		RUN	NO.	179	180	181	182	183	184	185	186	187	188	189	190

LIST OF TEST RUN  EVALUATION OF WAKE-ALTERING  1.0 (0 psi)/10" cap,	ICES	-	psf a h h/d	/0 8 6 -3.8 ~ Off		:	:	=		:		 :	=	:
114E1. 124E1.	(CONTINUED) TEST RUNS -ALTERING DEVICES	RPM	S MR/TR	80 1433/0		_		=					B	:
	LIST OF T EVALUATION OF WAKE-P	NOTHIT UNION NOTH REGIS	N/ CONDITION	(0 psi)/10" 87" gap	(0 psi)/10" .25" gap	I <sub>2</sub> +E <sub>1.0</sub> (0 psi)/7.6"	12+E1.0(20 psi)/Same 20 psi air	12+E1 0(40 psi)/Same 40 psi air	12+El.0(150 psi)/Same 150 psi air	psi)/Same cube 2" aft	psi)/Same	Kl3+Hl.11.2+I2+E4.0 (150 psi)/Same as 200 except center support cap	I <sub>2</sub> /Baseline with I <sub>2</sub> q tube	K <sub>13</sub> +H <sub>1.0</sub> +E <sub>5.0</sub> (0 psi)/Bifurcated air

	TABLE 2 (CONTINUED) LIST OF TEST RUNS EVALUATION OF WAKE-ALTERING DEVICES	(CONTINUED) TEST RUNS -ALTERING	) IS IS DEVICE:	60			30.00	
RUN		V <sub>T</sub> (I)	RPM	DISK	MODEL	MODEL	MR HT.	TAIL
NO.	CONFIGURATION/ CONDITION	KNOTS	MR/TR	rbg.	<b>9</b> 5	•	p/q	ROTOR
204	K <sub>13</sub> +H <sub>1.0</sub> +E <sub>5.0</sub> (150 psi)/Bifurcated duct with 150 psi air	80	1433/0	8	9	-3.8	8	Off
205	K <sub>13</sub> +H <sub>1.0</sub> +E <sub>5.0</sub> (40 psi)/Same as 204 with 40 psi air	=	•					
207	K <sub>13</sub> +H <sub>1.2.1</sub> +I <sub>1</sub> +E <sub>1.0</sub> (0 psi)/7.6" solid cap, no gap	=	=	=	•			1 89
208	FE1.0	=		=	=	•	•	<b>.</b>
210	K <sub>13</sub> +H <sub>1.15.1</sub> +I <sub>1</sub> +E <sub>1.0</sub> (0 psi)/Repeat of 189	=	•	-	=	•	-	
211	K <sub>13</sub> +H <sub>1.14.1</sub> +I <sub>1</sub> +E <sub>1.0</sub> (0 psi)/Like 189 and 210 except cap is oper	•			-			
								ent.
31 81 35						# 15 kg	7 2 4	
							6	
							iai U	

TABLE 3

INDEX TO RAKE POSITIONS

RUN NUMBER	TEST POINT	WATER LINE	MODEL STATION	BUTT	LOCATION
111	20 21 22 24 26 28 30 32 34 36	53.5	103.1 105.0 107.0 109.0 111.0 112.9 114.9 116.9 118.9	-7.25	1
112	2 4 6 8 10 12	48.9 50.8 52.7 54.5 56.2 57.2	107.3	-7.25	1 V
113	2 4 6 8 10 11	51.7 52.3 52.8 53.3 53.9 53.3	103.3	-3.25	1
114	2 4 6 8 10	44.5 46.4 48.2 50.0 51.9	103.0	-3.25	1
115	3 4 6 9 10 12 14 16 18 20	52.9 52.0 50.0 48.0 46.0 44.1 42.1 53.0 54.0 55.0	124.7	-3.25	1

TABLE 3 (CONTINUED)

INDEX TO RAKE POSITIONS

RUN NUMBER	TEST POINT	WATER LINE	MODEL STATION	BUTT	LOCATION FIGURE
116	7	36.9	100.5	-17.5	1
117	2 4 6 8 10	37.6 37.3	100.5	-16.0 -14.0 -12.0 -10.0 - 8.0	1
118	2	37.6	100.5	- 6.0	1
119	2 5 8 9 14 16 20 25	37.3 "" "" 51.5 52.3	99.6 "" 102.5 101.7	+ 6.0 8 10 14 16 17.5 -17.5	1
121	3 4 6 8 10	62.9 53.5 50.1 46.0 42.1	129.0	+ 5.7	2
13́5	2 4 6 8 10 12 14	56.9 54.5 52.5 50.5 48.5 46.5 44.5	106.3	- 5.7 " "	3
136	2 4 6 8 10 12 14 17 18 19	56.5 54.5 52.5 50.6 48.5 46.5 44.5 37.1 39.0 41.0	104.0	- 8.0 " " "	4

# TABLE 3 (CONTINUED) INDEX TO RAKE POSITIONS

RUN NUMBER	TEST POINT	WATER LINE	MODEL STATION	BUTT	LOCATION FIGURE
137	3 5 7 9 11 13 15 17	38.7 39.9 42.0 44.0 46.0 48.0 50.0 52.0 54.0	98.4 100.5 103.6	- 8: :: :: :: :: :: :: :: :: :: :: :: ::	5
138-41, 143	2 3 4 5 6 7 8 9	38.8 40.0 42.0 44.0 46.0 48.0 50.0 52.0 54.0	98.4 100.5 103.6	- 8.0	5
142	7 8 9 10 11 12 13 14 15 16 17	37.8 40.2 42.0 44.0 46.0 48.0 50.0 52.0 54.0 56.8	98.4 " 100.5 103.6	- 8.0 "" ""	5

TABLE 3 (CONTINUED)

INDEX TO RAKE POSITIONS

RUN NUMBER	TEST POINT	WATER LINE	MODEL STATION	BUTT LINE	LOCATION FIGURE
149-151	2 3 4 5 6 7 8 9	38.8 40.0 42.0 44.0 46.0 48.0 50.0 52.0 54.0	98.5 100.6 103.5	- 8.0 "" ""	5
152-6, 158 161-4, 166 167, 169-71 175, 177-9 180,182,184 186-8, 190 191,193,194 196,198,201 204,207,208 211	7 8	42.9 44.9 46.9 48.9 50.9 52.9 54.9 56.9	97.9 100.6 104.6	0.0	6
159	1 2 3 4 5	54.9 52.9 50.7 48.6 46.7	104.6	0.0	6
160,203	5 6 7 8 9 10	42.9 44.9 46.9 48.9 50.9 52.9 54.9	97.9 100.6 104.6	0.0	6
165	3 4 5 6 7 8	44.9 42.9 46.9 48.9 50.9 52.9	97.9 100.6 104.6	0.0	6

TABLE 3 (CONTINUED)

INDEX TO RAKE POSITIONS

RUN NUMBER	TEST POINT	WATER LINE	MODEL STATION	BUTT LINE	LOCATION FIGURE
168, 183	4 5 6 7 8 9	42.9 44.9 46.9 48.9 50.9 52.9 54.9	97.9 100.6 104.6	0.0	6
172	3 4 6 7 8 9 10	42.9 44.9 44.9 46.9 48.9 50.9 52.9 54.9	97.9 " 100.6 104.6	0.0 " " "	6
173,174,176 185,195,197 199,200,205 210	1 2 3 4 5 6 7	42.9 44.9 46.9 48.9 50.9 52.9 54.9	97.9 100.6 104.6	0.0	6
181	2 3 4 5 6 7 9 10 11 12 13	42.9 44.9 46.9 48.9 50.9 52.9 54.9	97.9 100.6 104.6 "	0.0	6

TABLE 3 (CONTINUED)

INDEX TO RAKE POSITIONS

RUN NUMBER	TEST POINT	WATER LINE	MODEL STATION	BUTT	LOCATION FIGURE
189	29 30 31 32 33 34 35 36 37 38 39	42.9 44.9 46.9 48.9 50.9 50.9 52.9 54.9	97.9 100.6 " 104.6 100.6 104.6	0.0	6
202	3 4 5 6 7	43.4 44.9 46.9 48.9 50.9	97.9 100.6 104.6	0.0	6
				26.35	

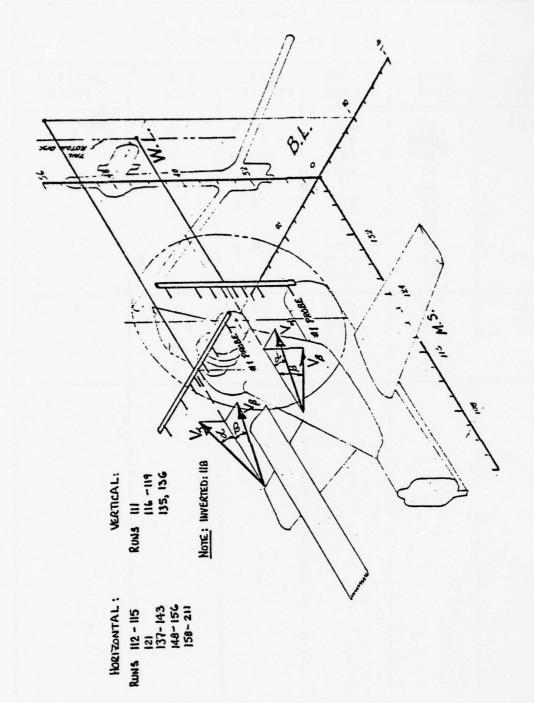


FIGURE 1 - RAKE ORIENTATION DIAGRAM



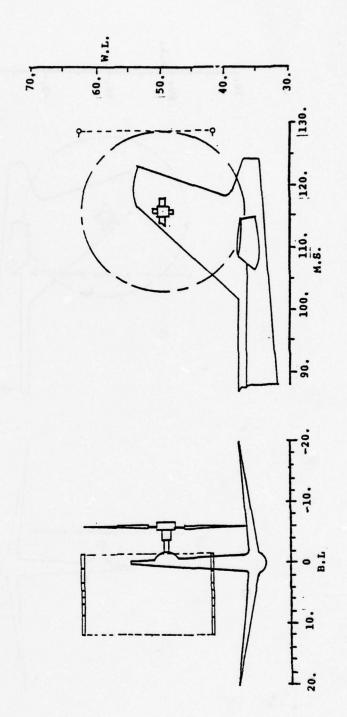


FIGURE 2 -HOT FILM RAKE LOCATIONS

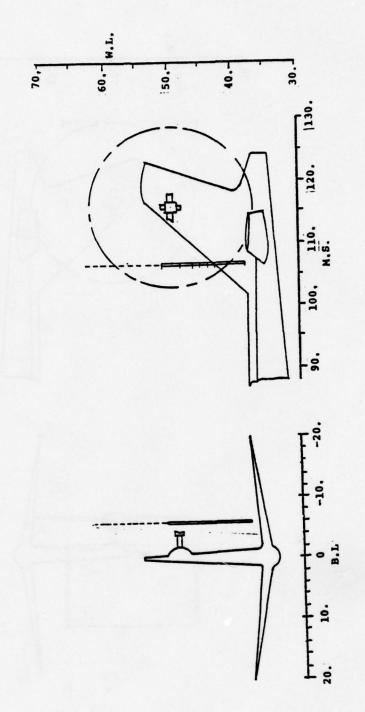


FIGURE 3 -HOT FILM RAKE LOCATIONS



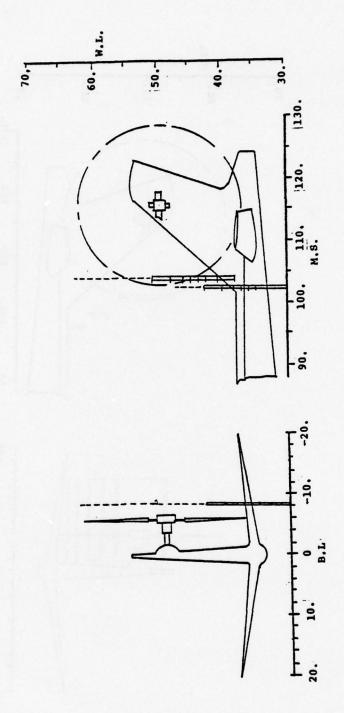


FIGURE 4 -HOT FILM RAKE LOCATIONS

RUN 137, 138, 139, 140, 141, 142, 143, 148, 149, 150, 151

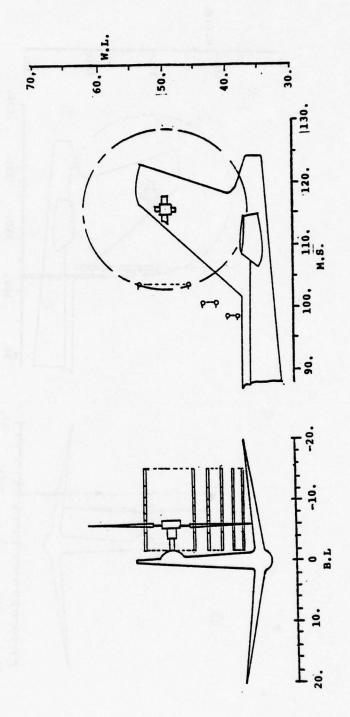


FIGURE 5 -HOT FILM RAKE LOCATIONS

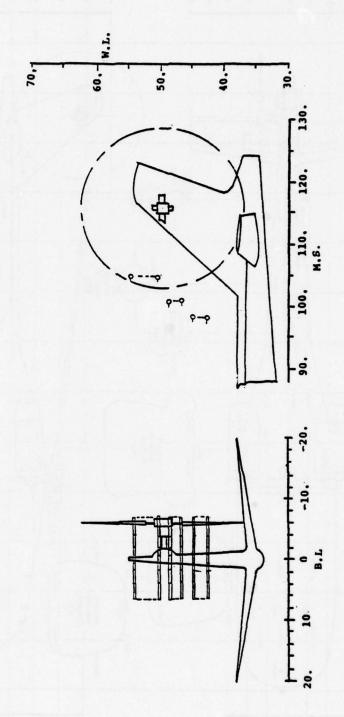


FIGURE 6 -HOT FILM RAKE LOCATIONS

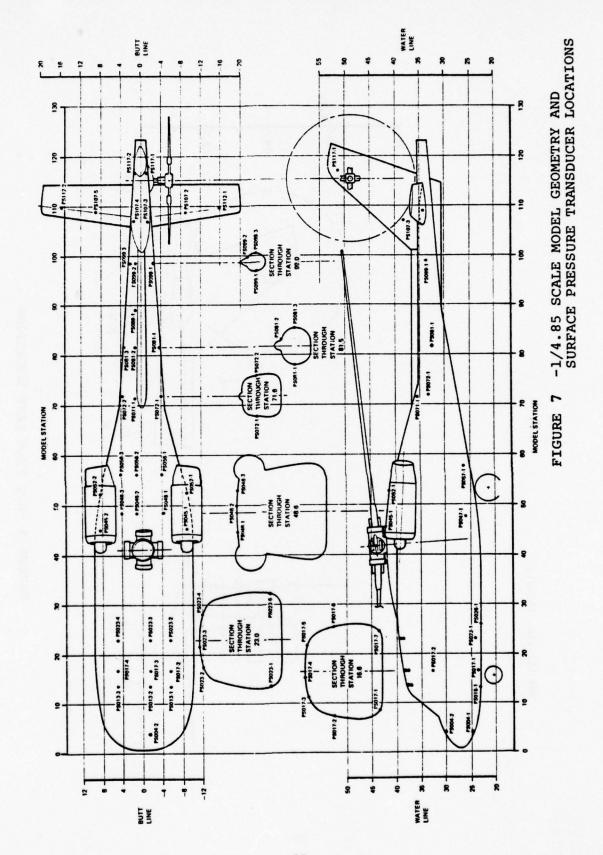
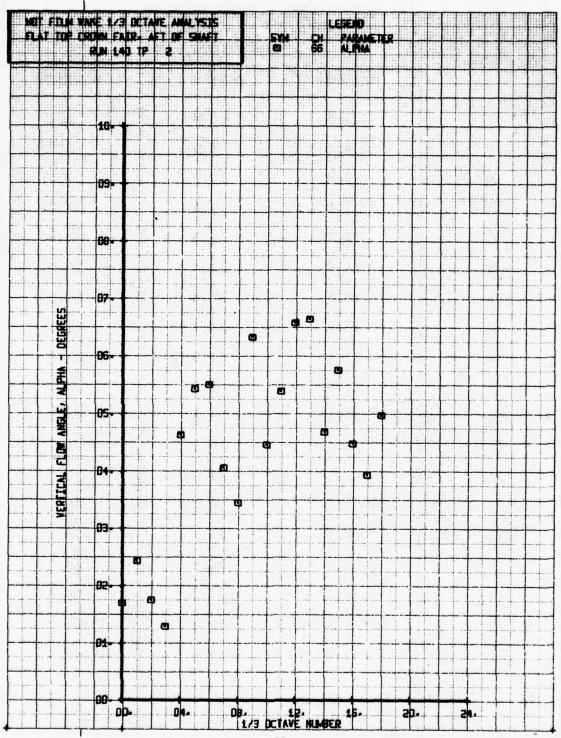
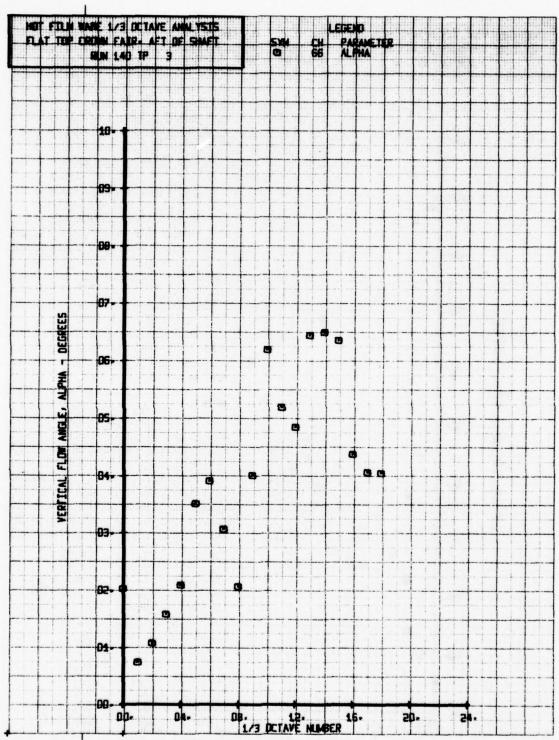
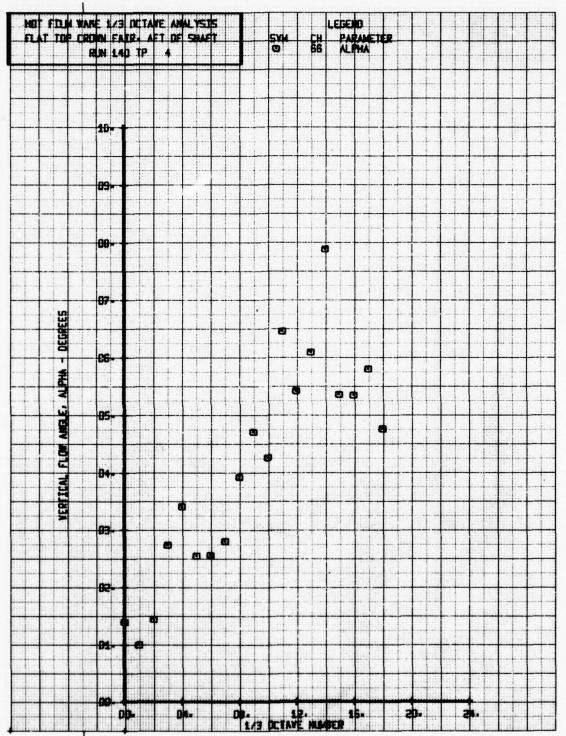


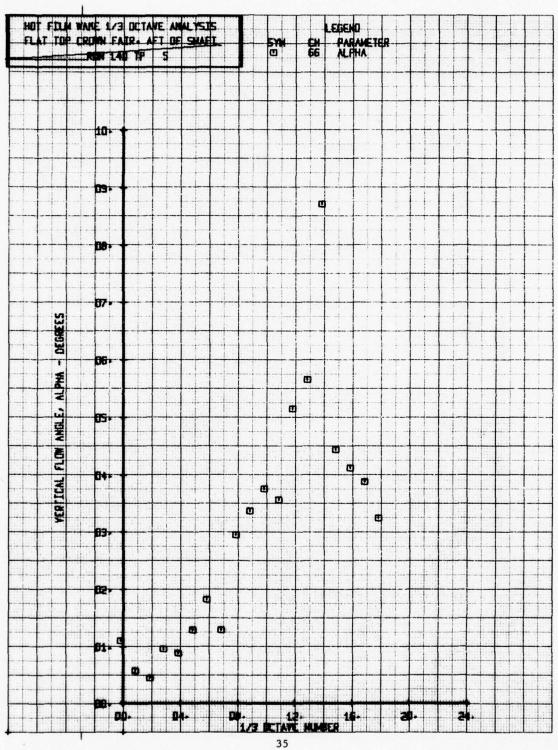
TABLE 4
1/3 OCTAVE BAND IDENTIFICATION

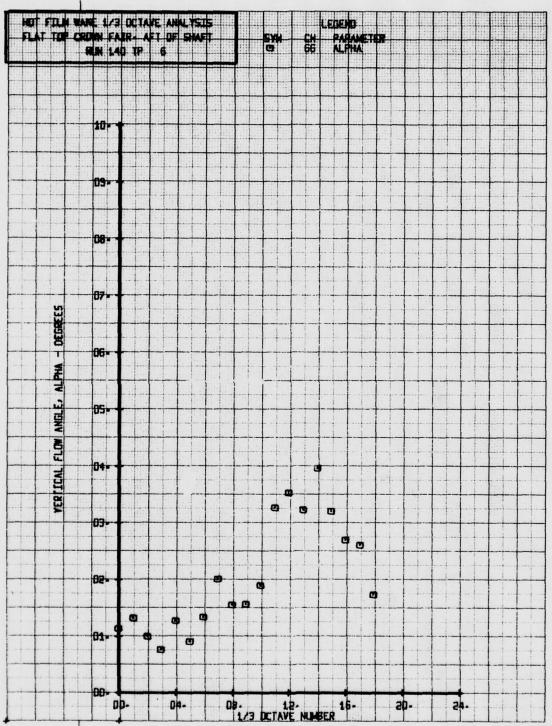
BAND NUMBER	BAND WIDTH - Hz						
BAND NUMBER	MINIMUM	CENTER	MAXIMUM				
0	3.5	3,4	4.4				
1	4.4	4.9	5.5				
2	5.5	6,2	7.0				
3	7.0	7.8	8.7				
4	8.7	9.8	11.0				
5	11.0	12,4	13.9				
6	13.4	15,6	17.5				
7	17.5	19.7	22.1				
8	22.1	24.8	27.8				
9	27.8	31.25	35,1				
10	35.1	39.4	44.2				
11	44.2	49.6	55.7				
12	55.7	62.5	70.2				
13	70.2	78.7	88.9				
14	88.9	99.2	111.4				
15	111.4	125.0	140.3				
16	140.3	157.5	176.8				
17	176.8	198.4	222.7				
18	222.7	250.0	280.6				

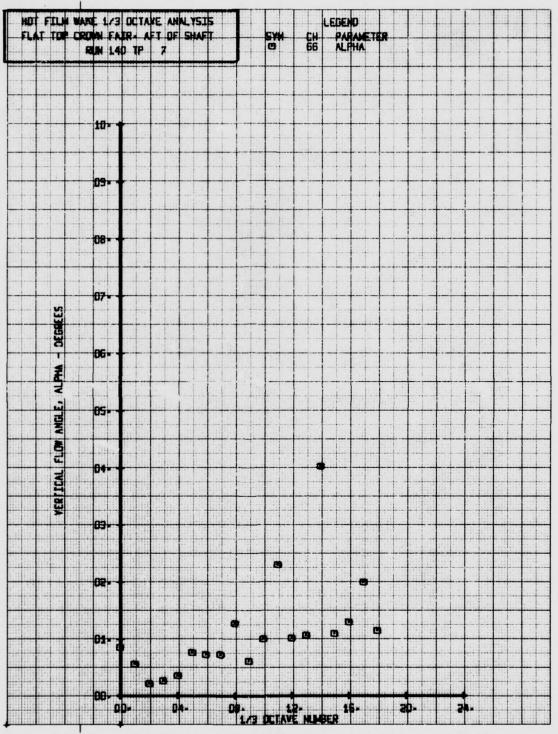


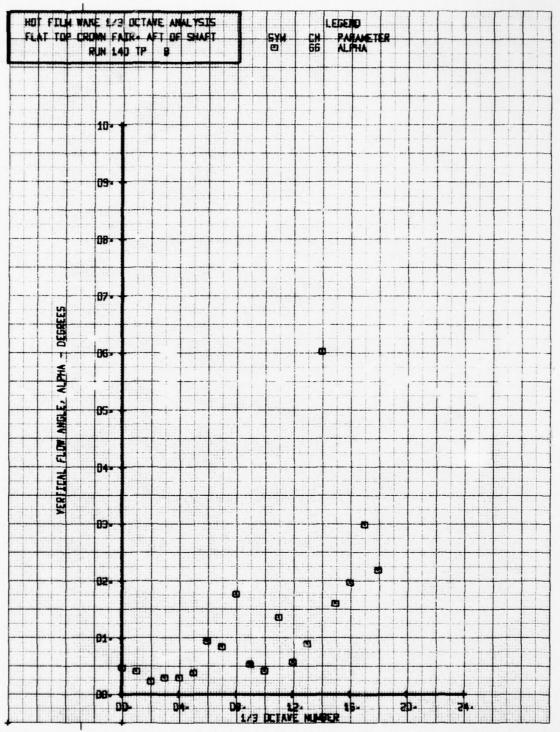


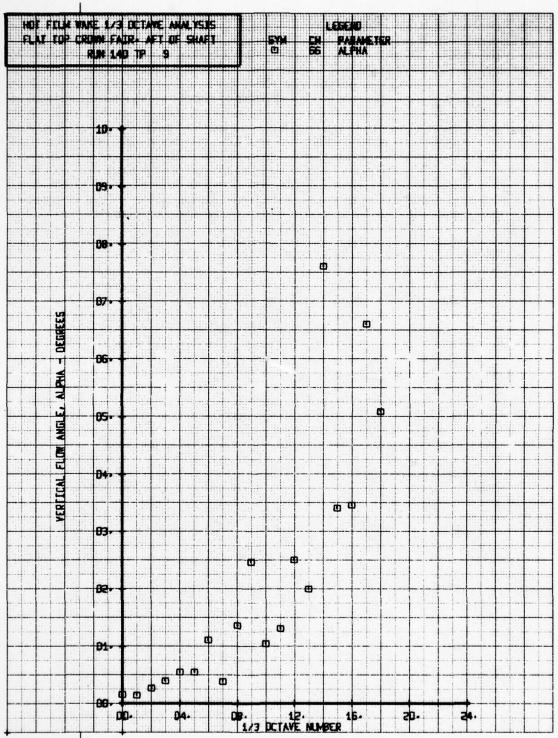


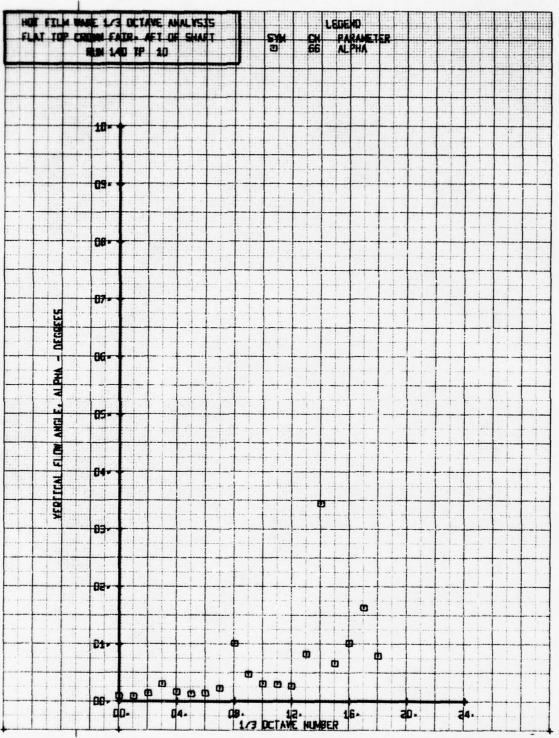


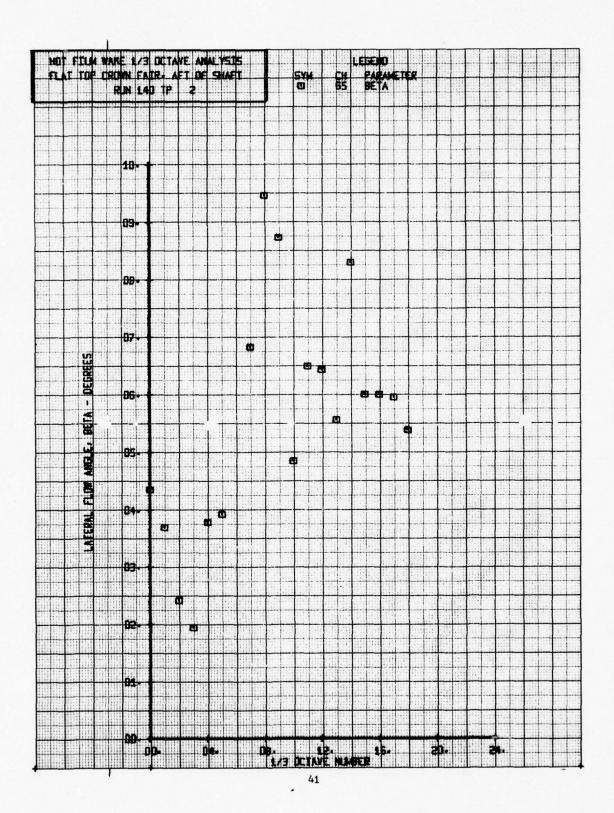


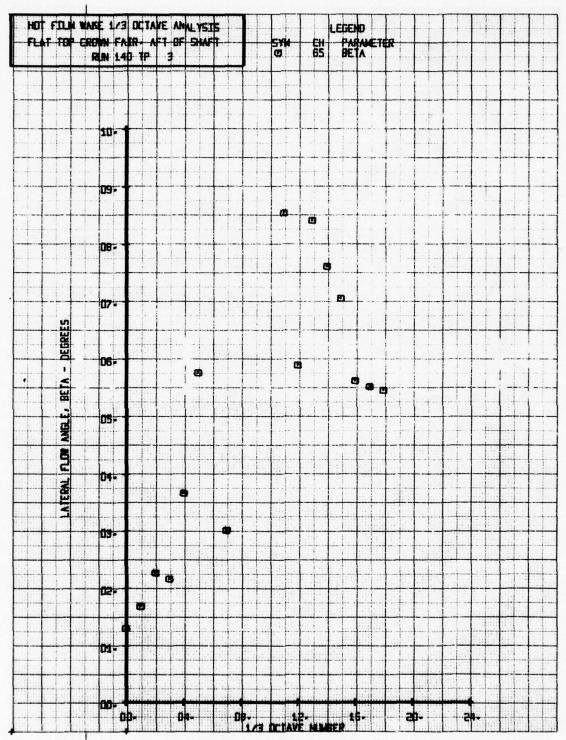


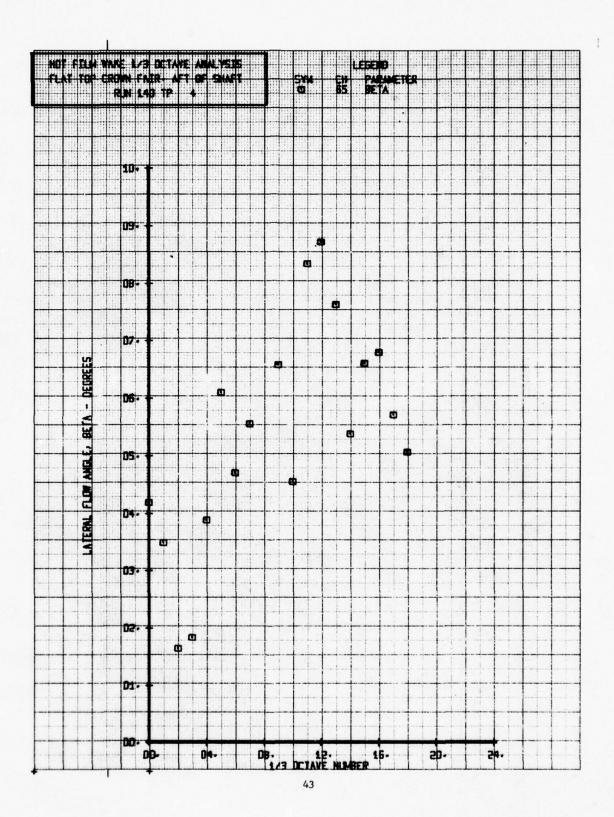


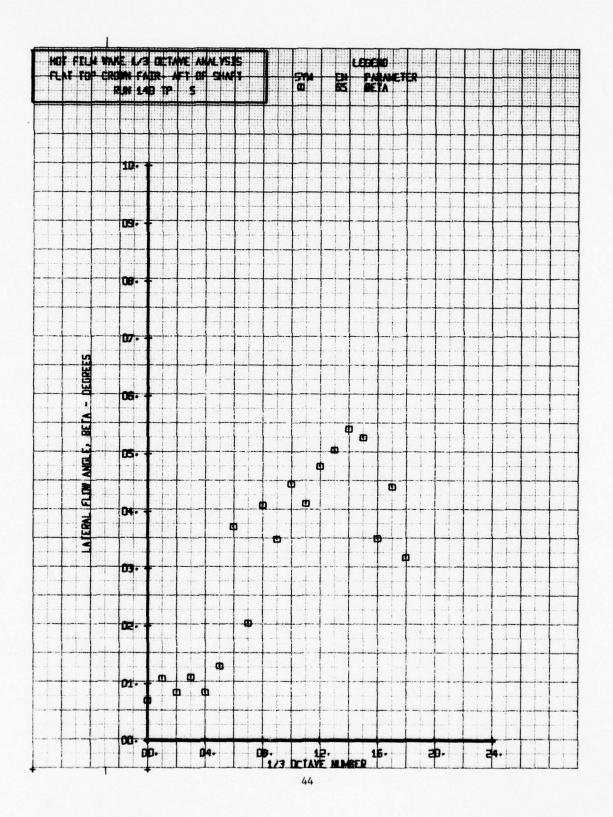


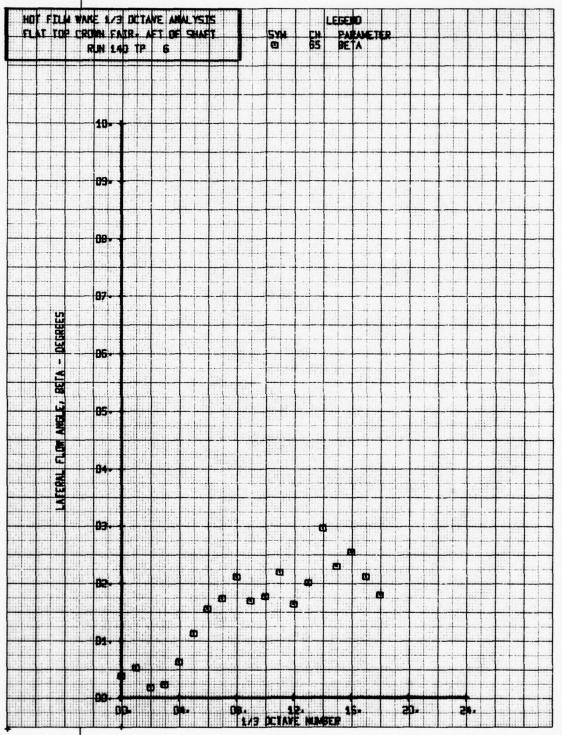


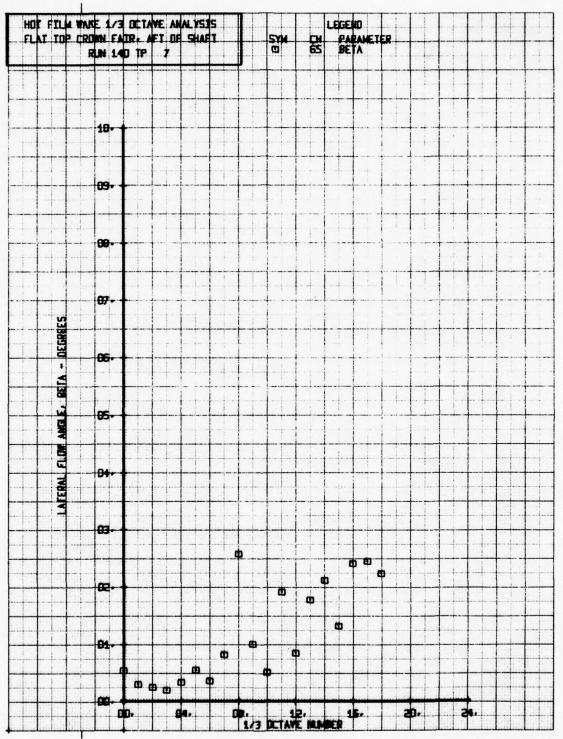


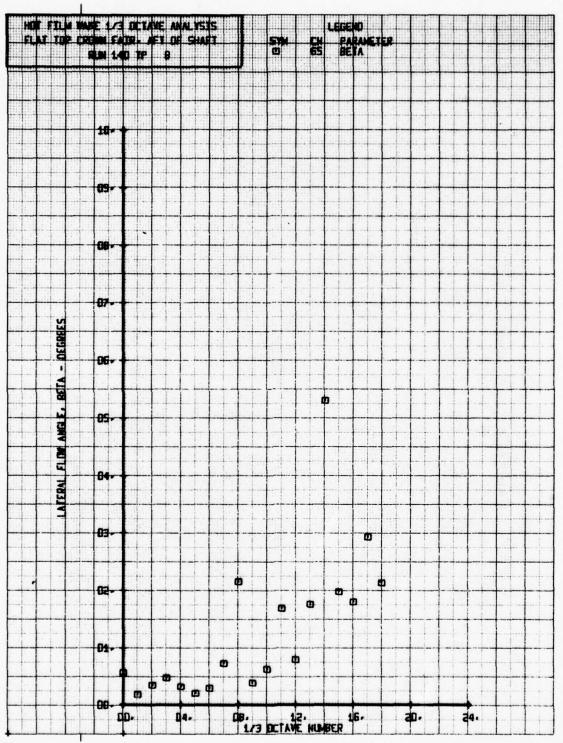


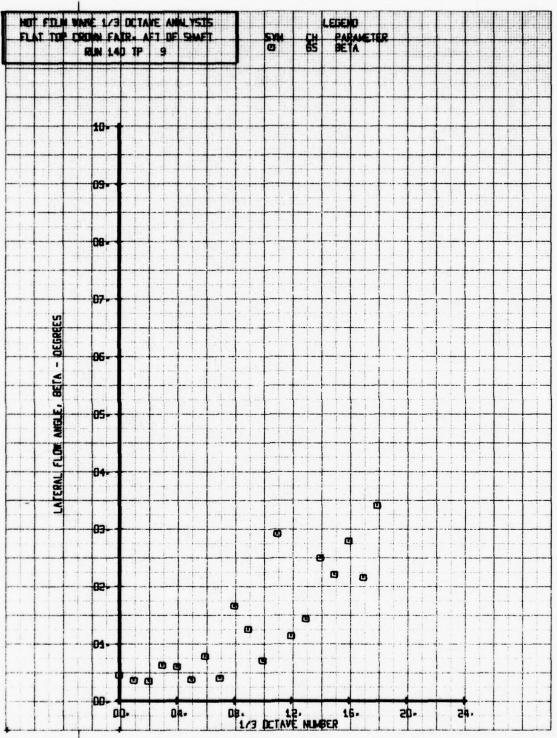


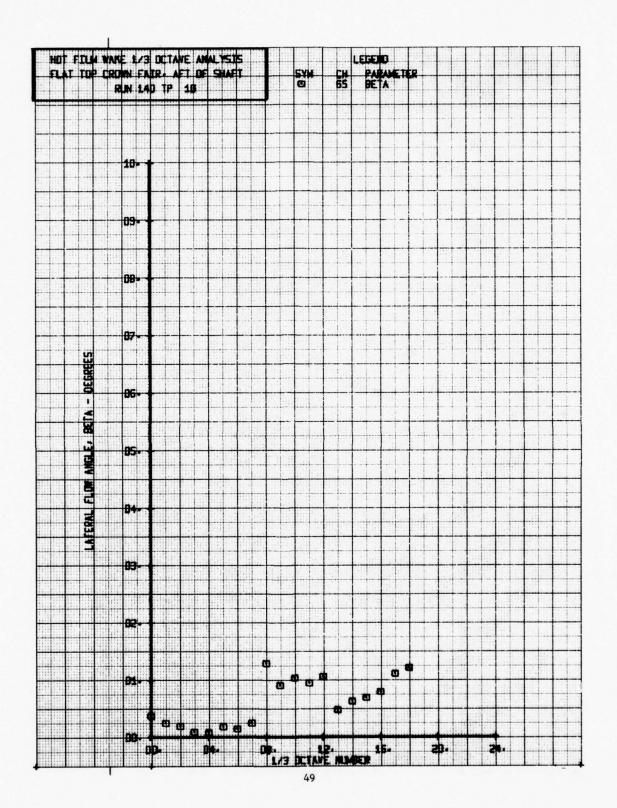


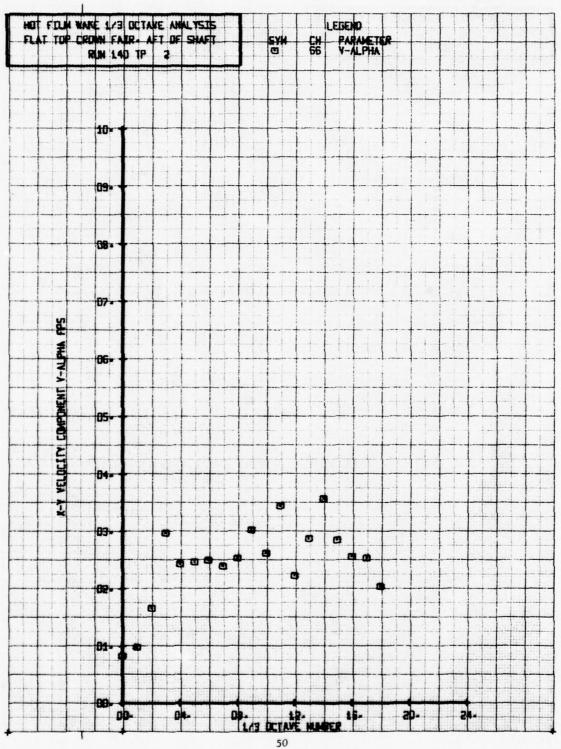


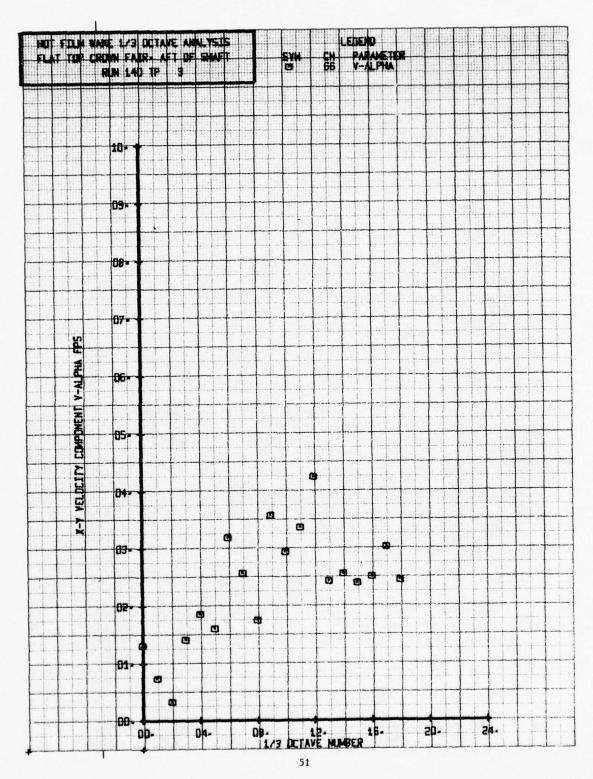




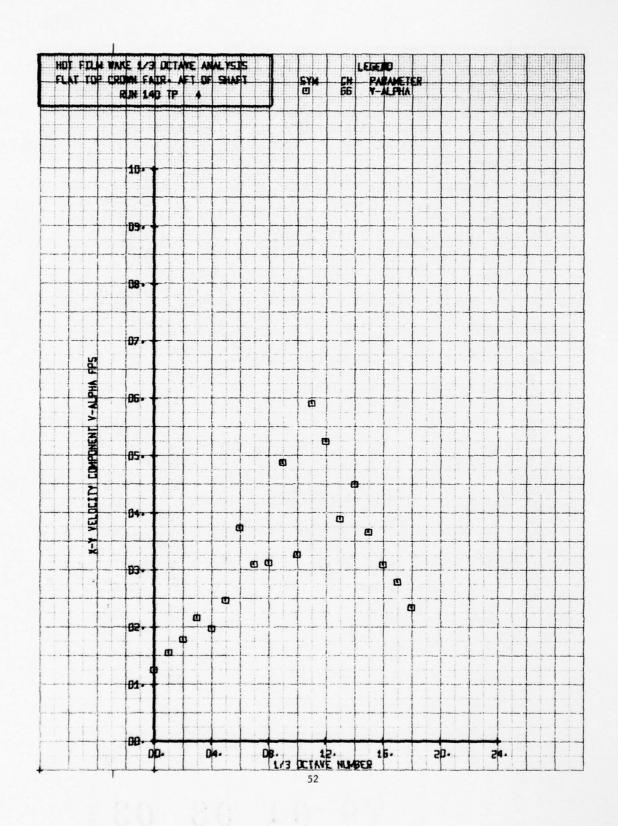


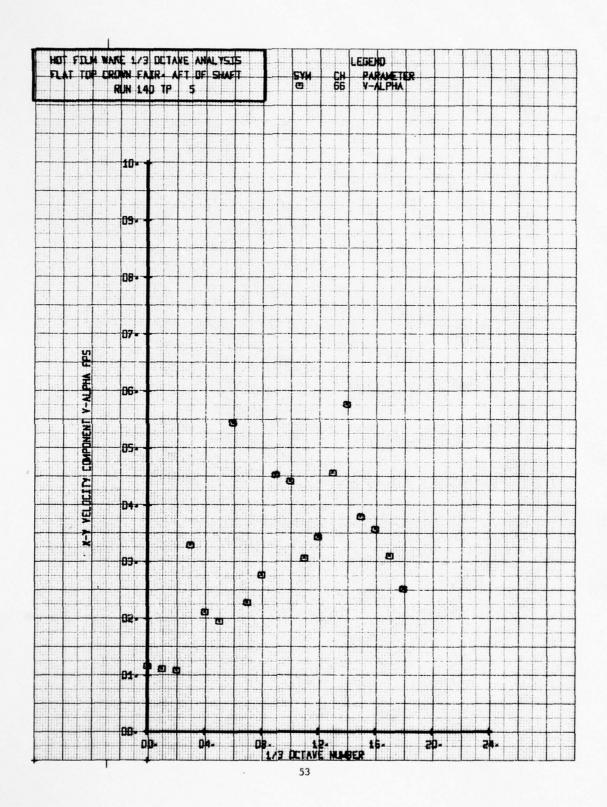


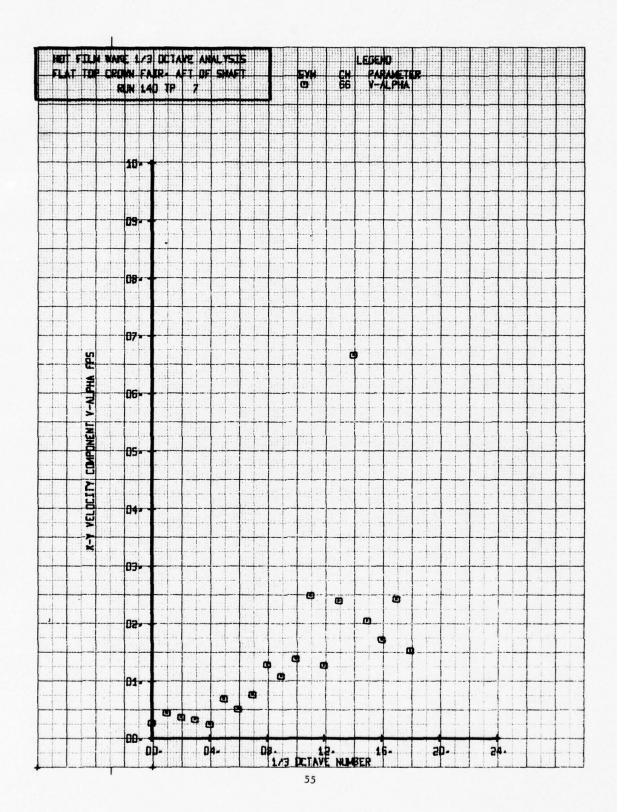


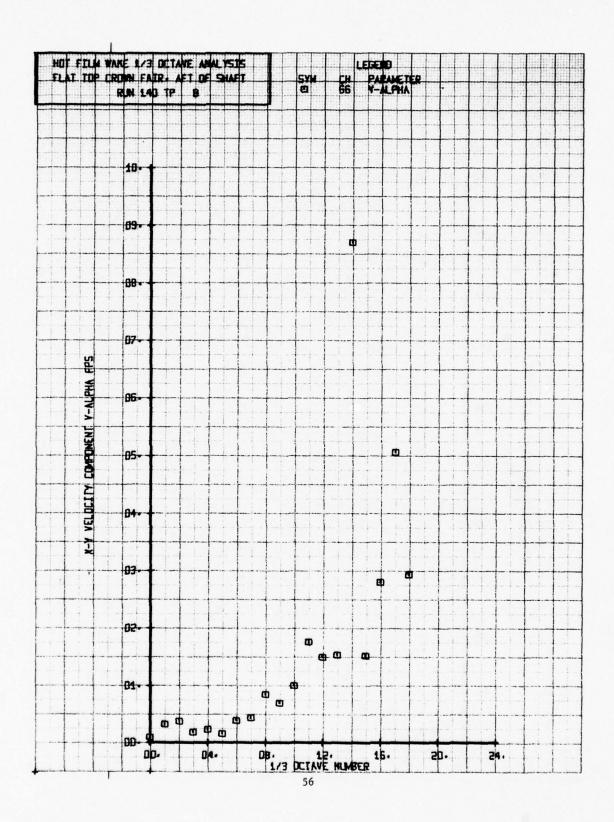


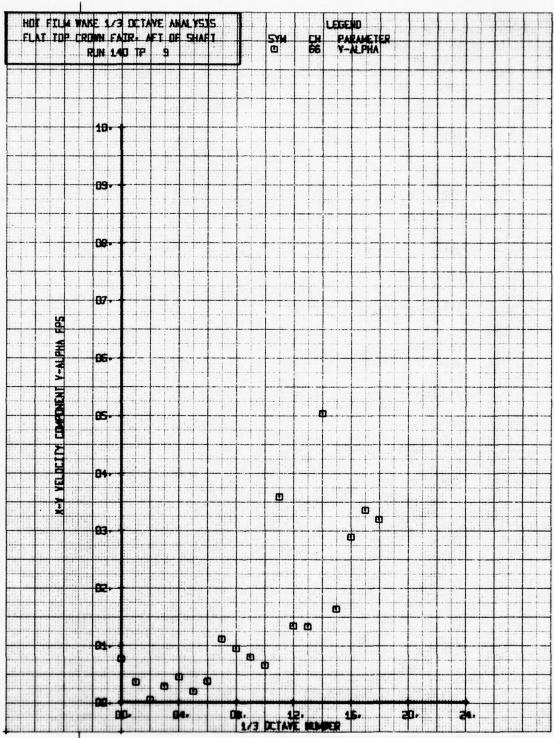
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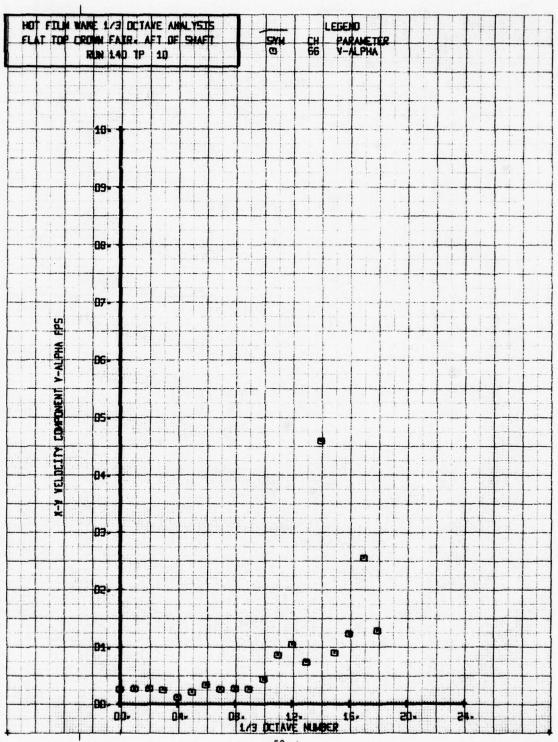


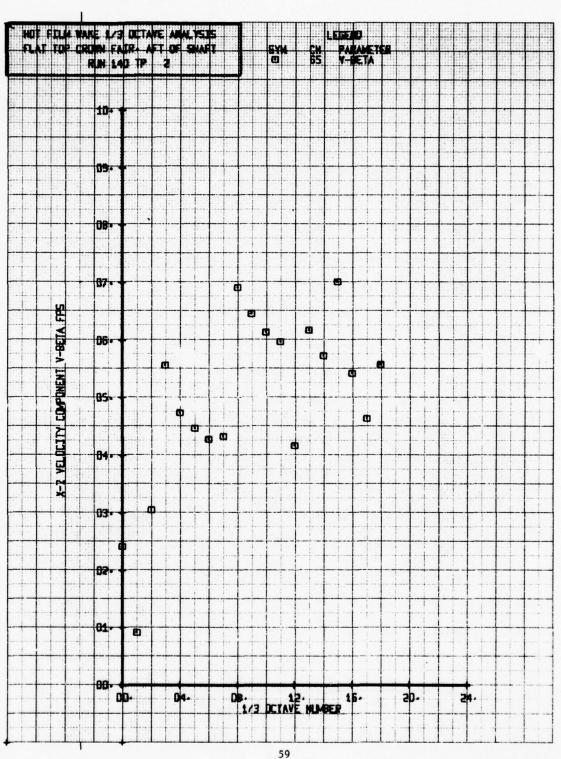


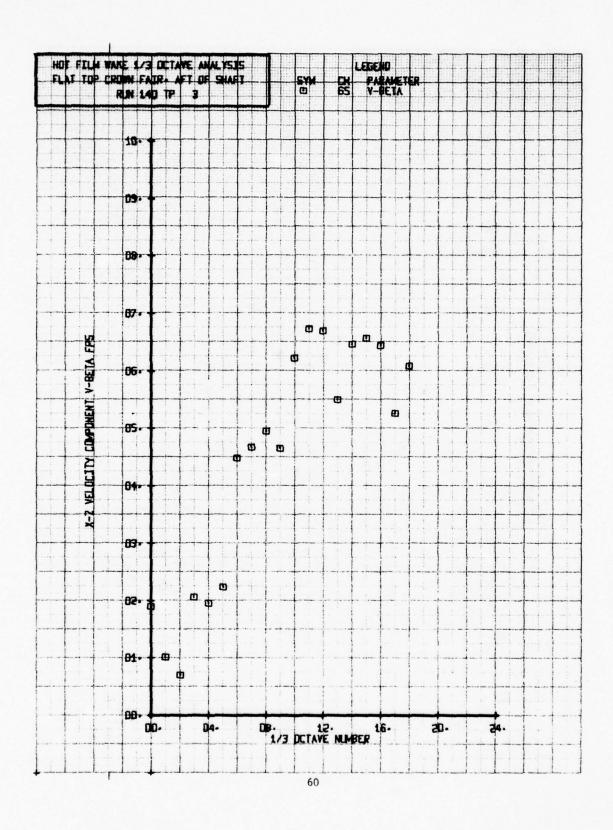


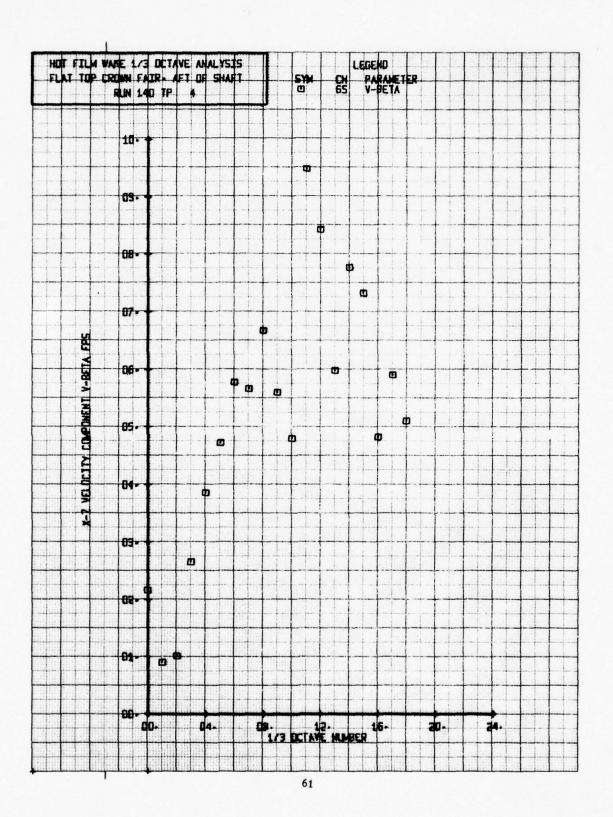


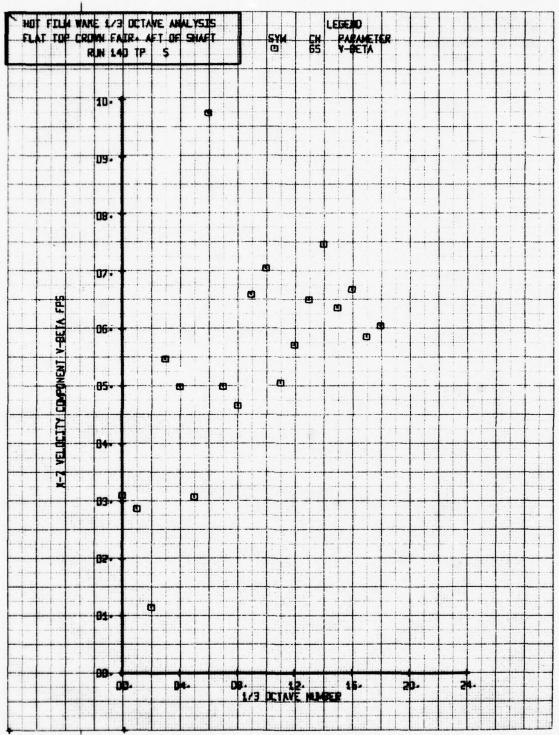


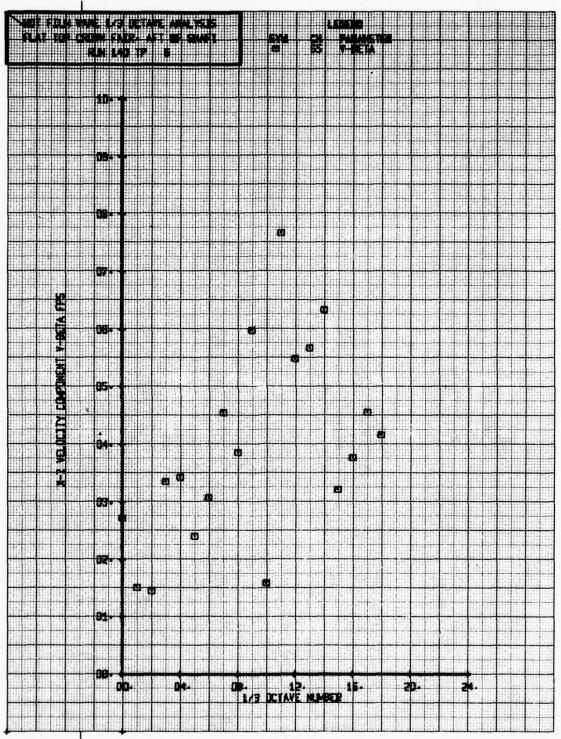


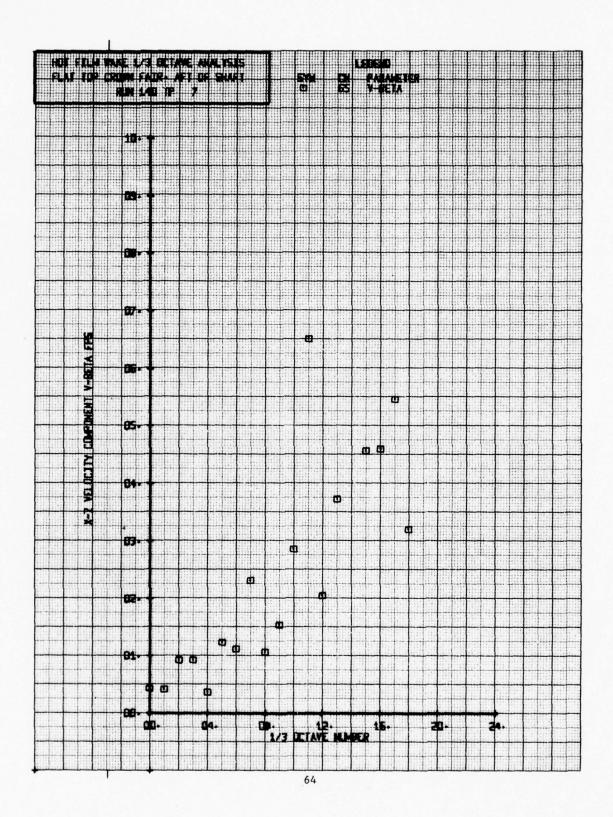


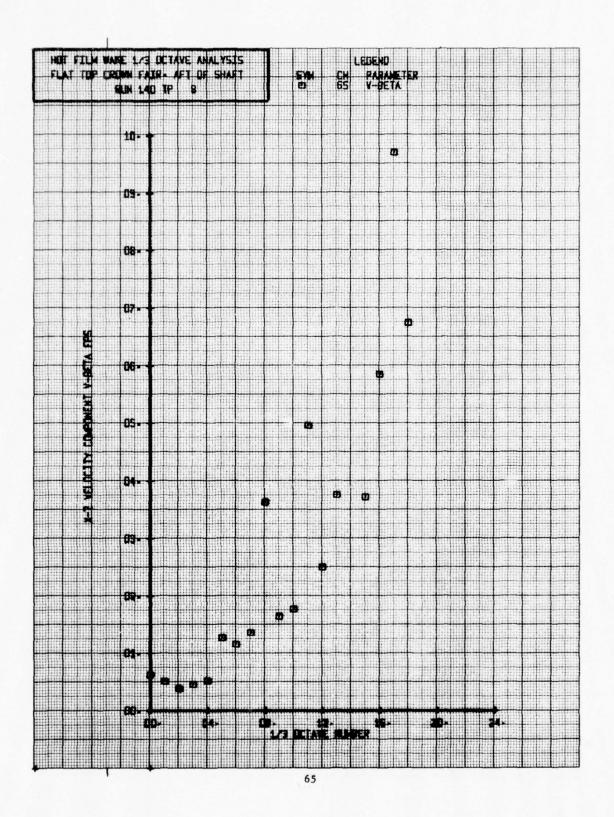


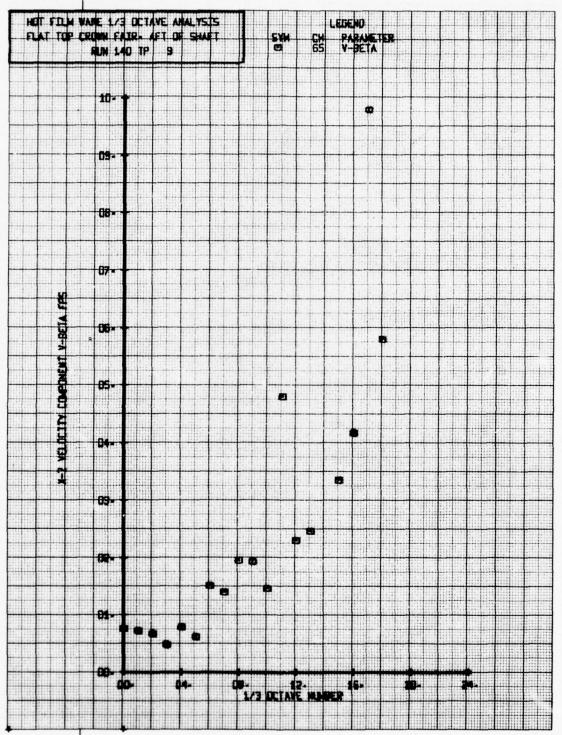


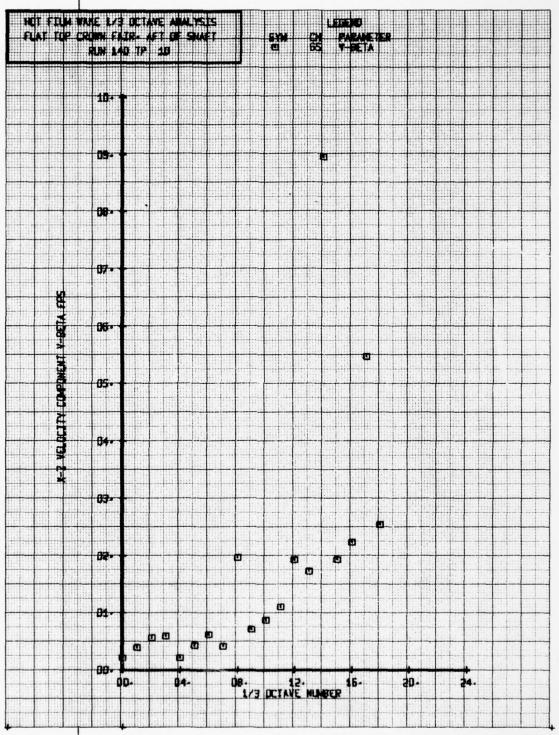


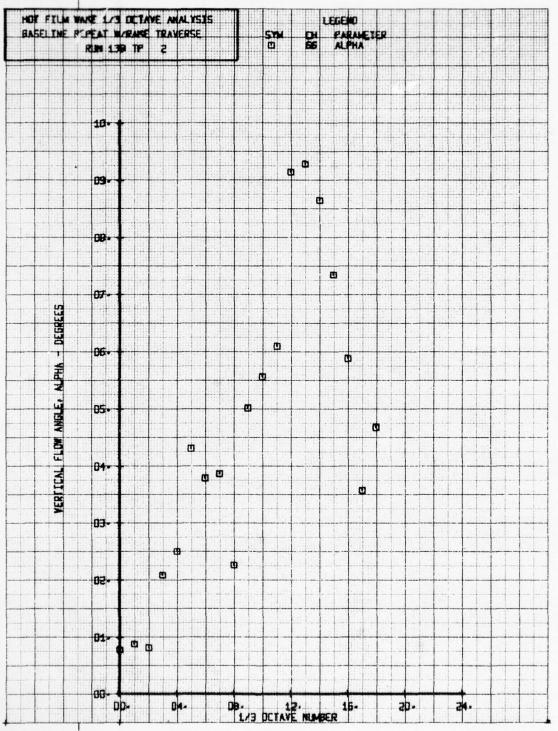


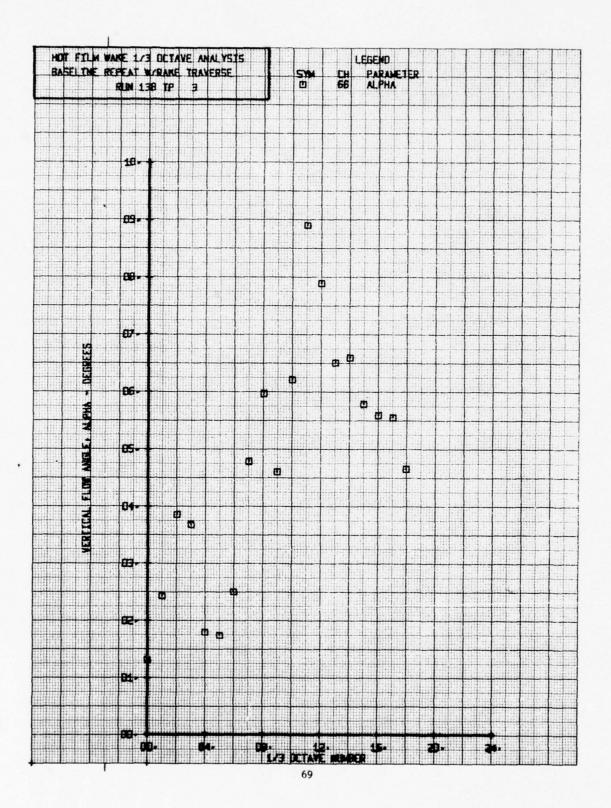


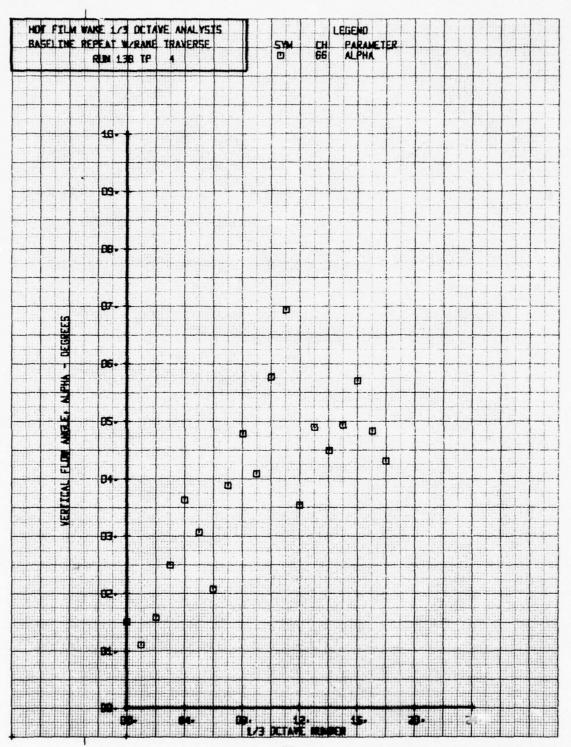


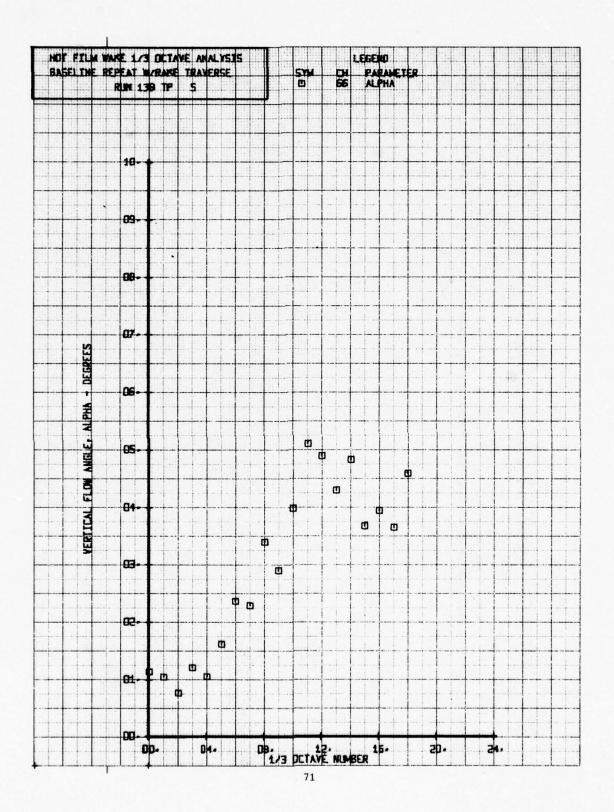


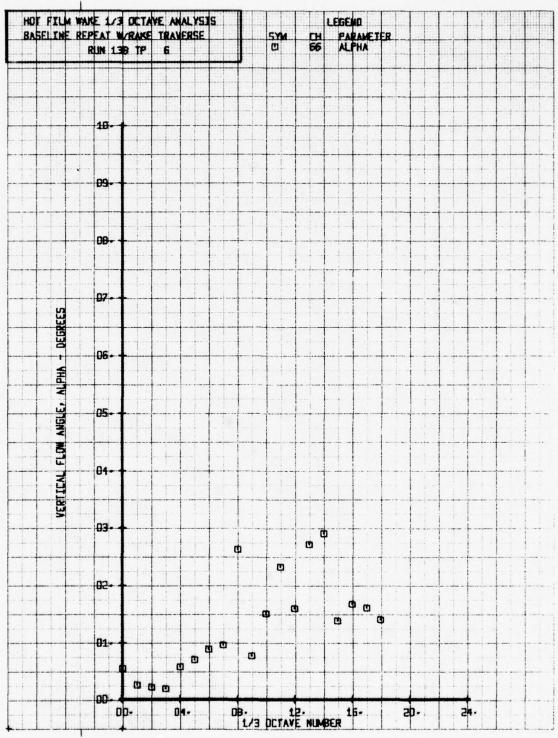


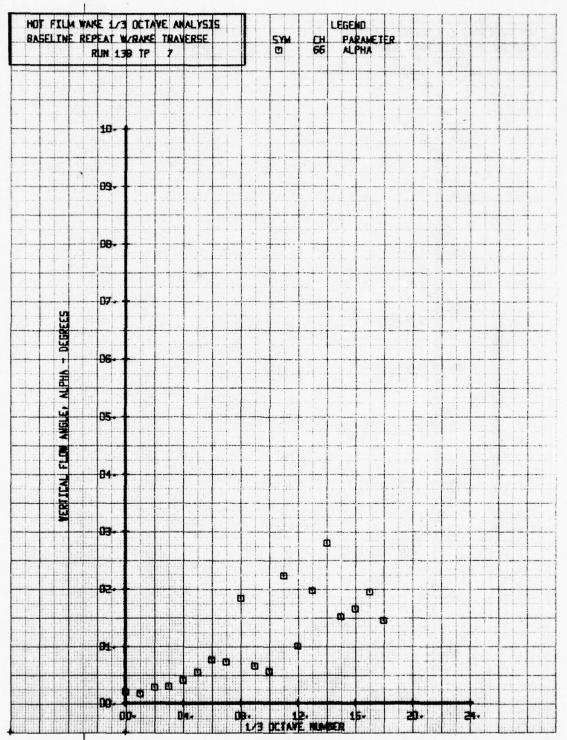


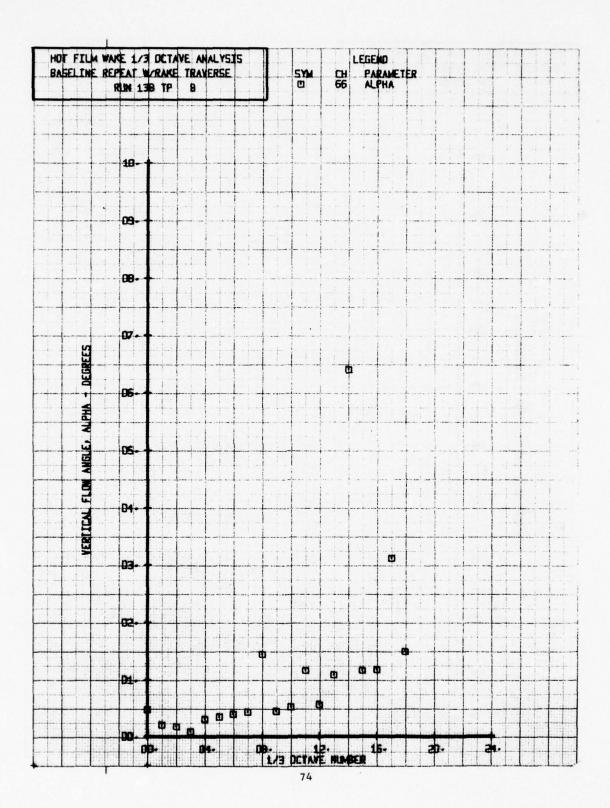


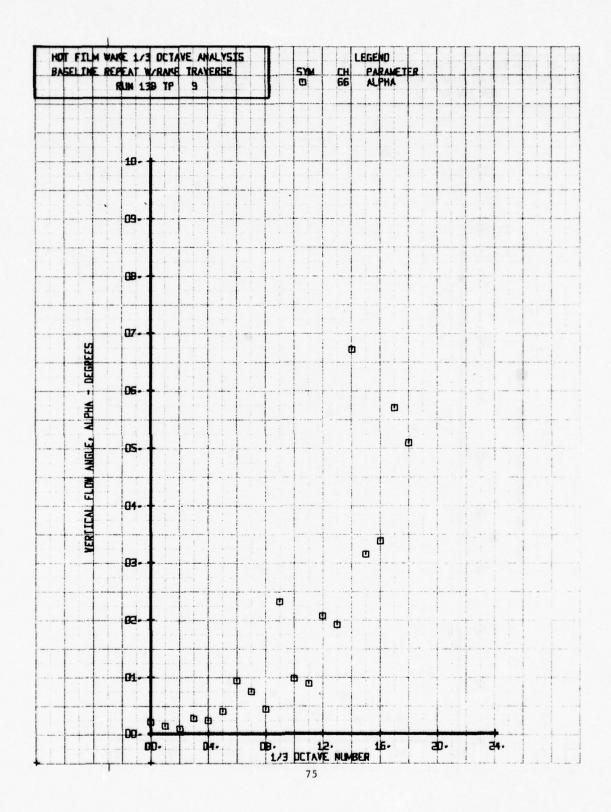


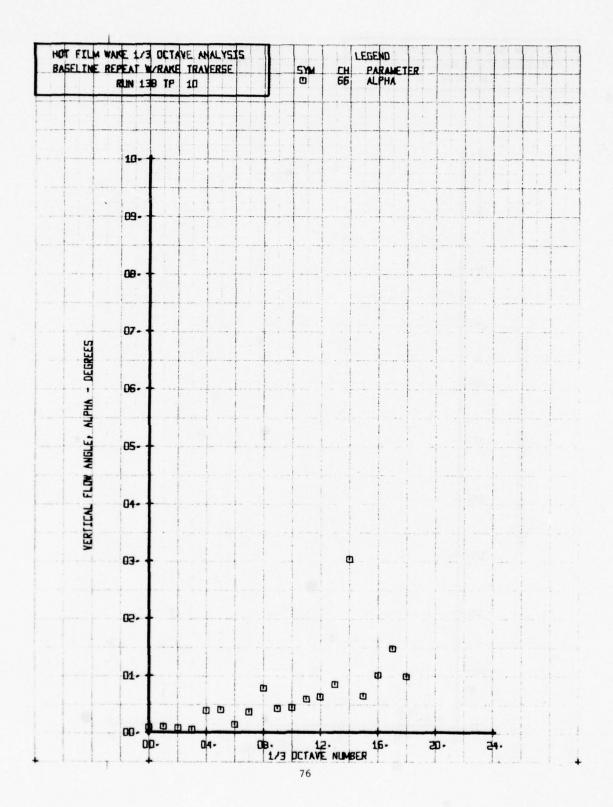


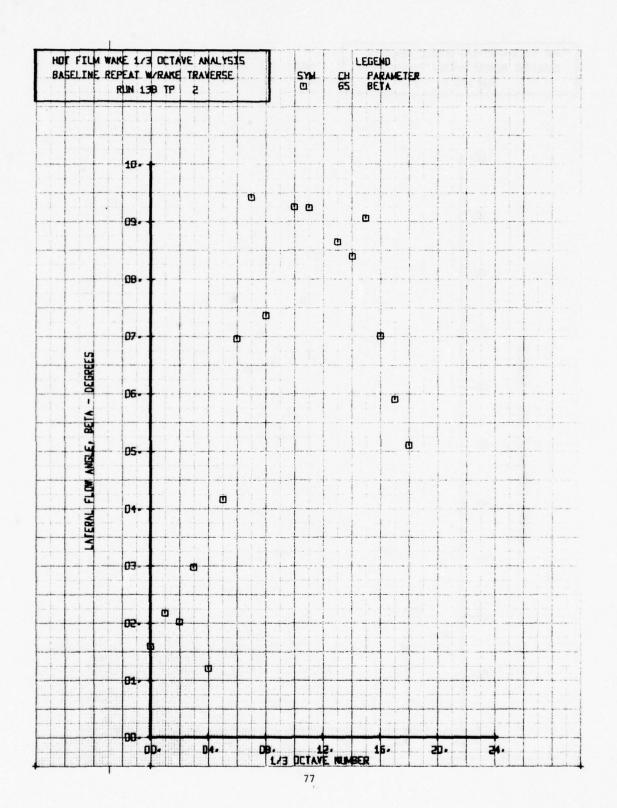


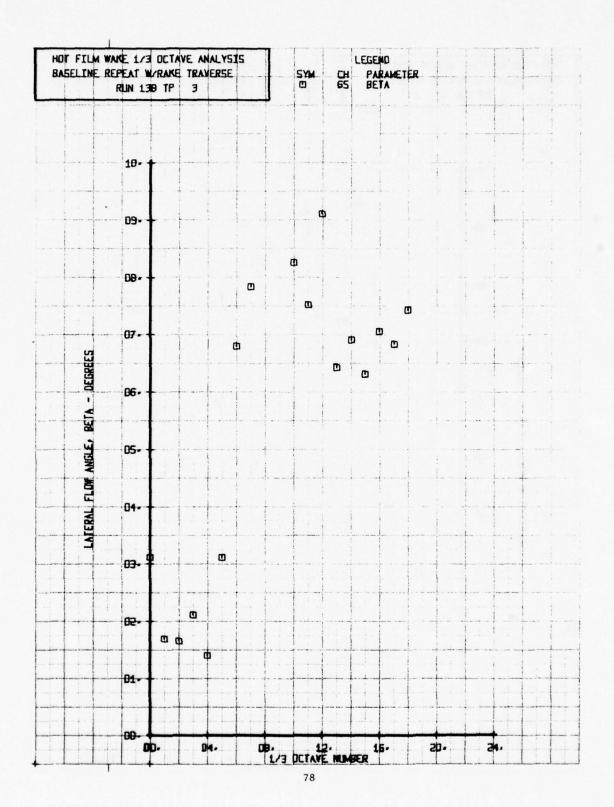


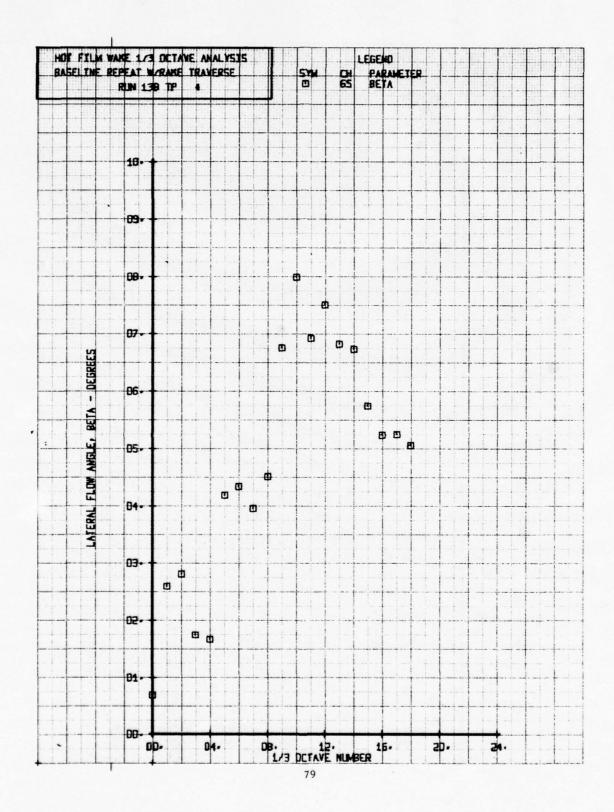


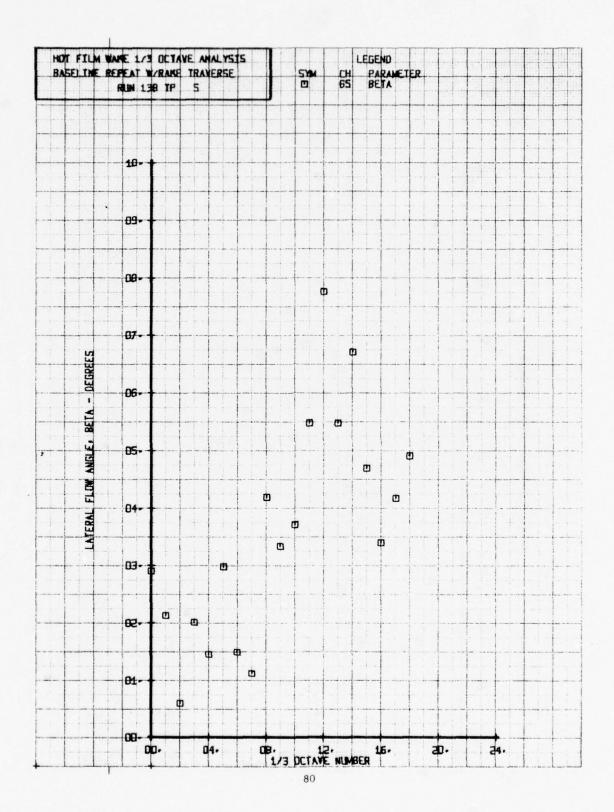


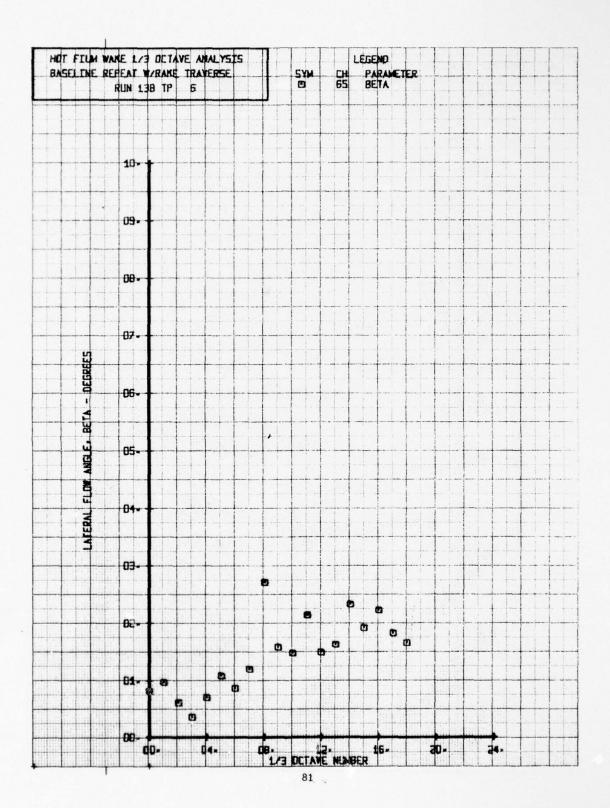


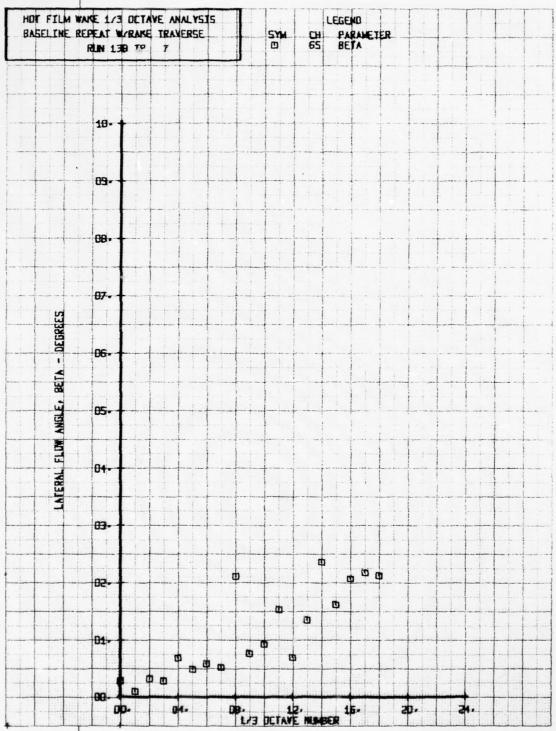


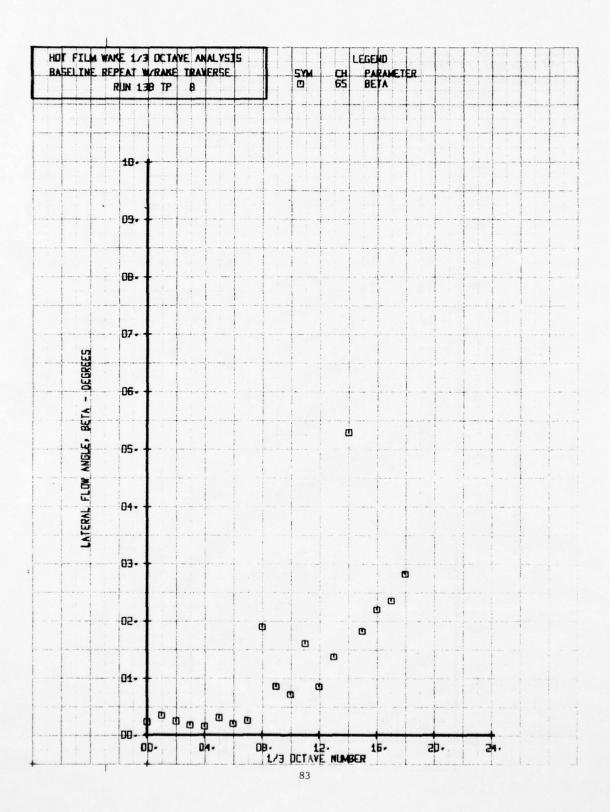


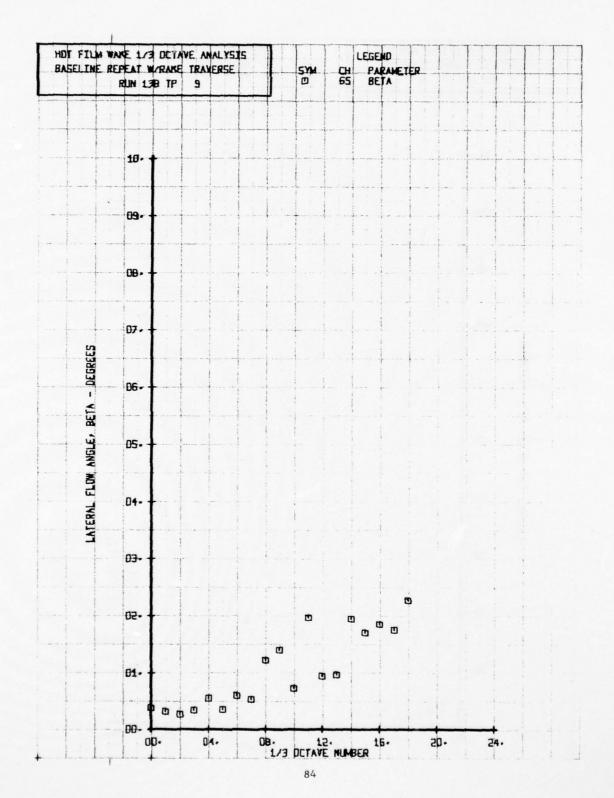


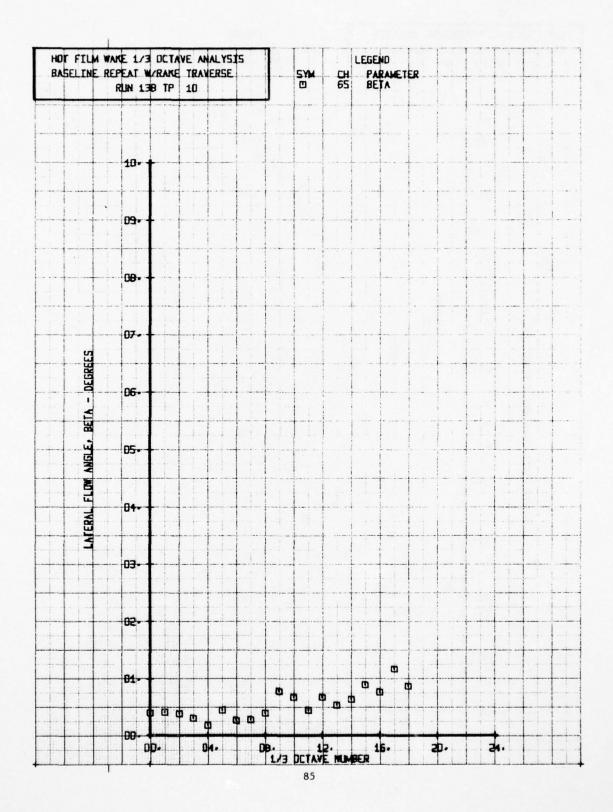


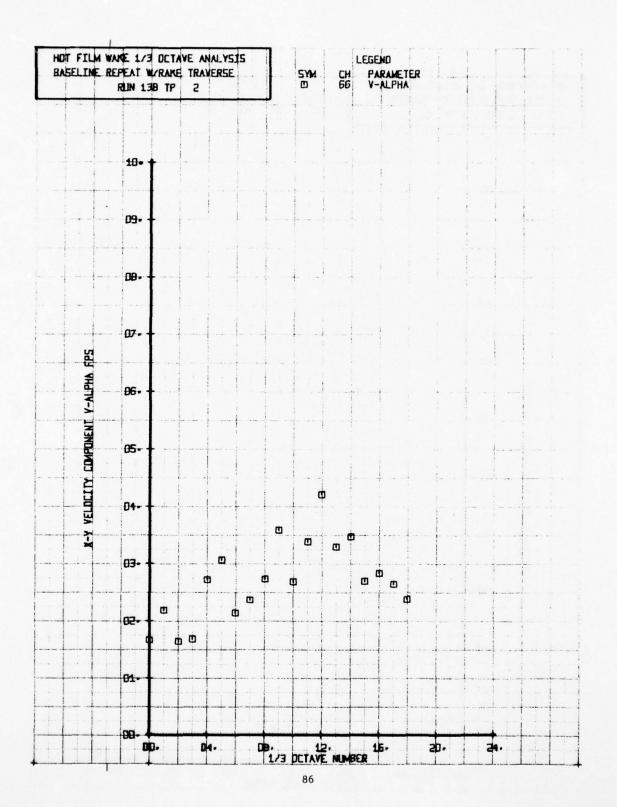


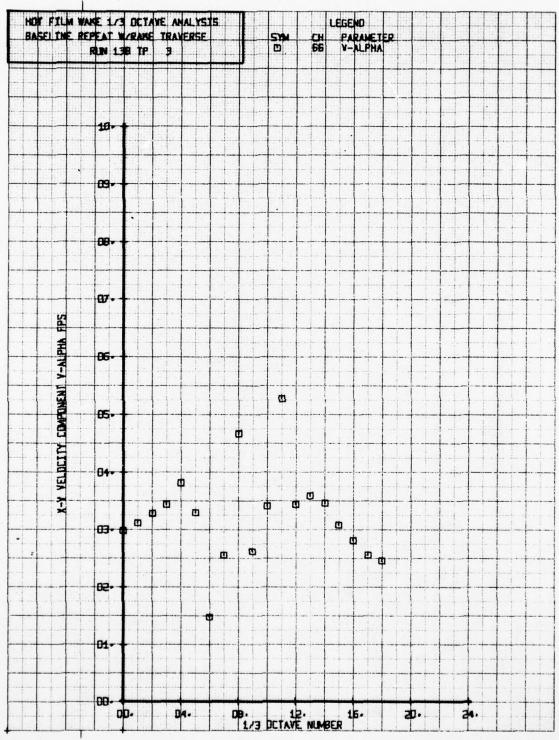


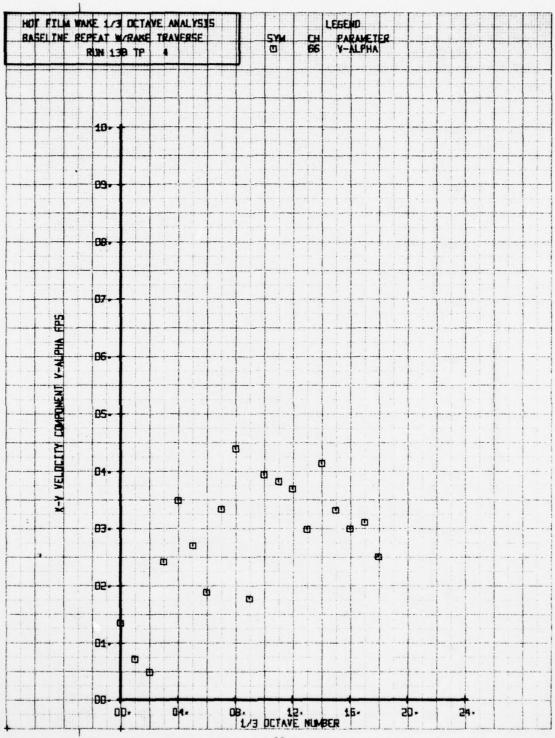


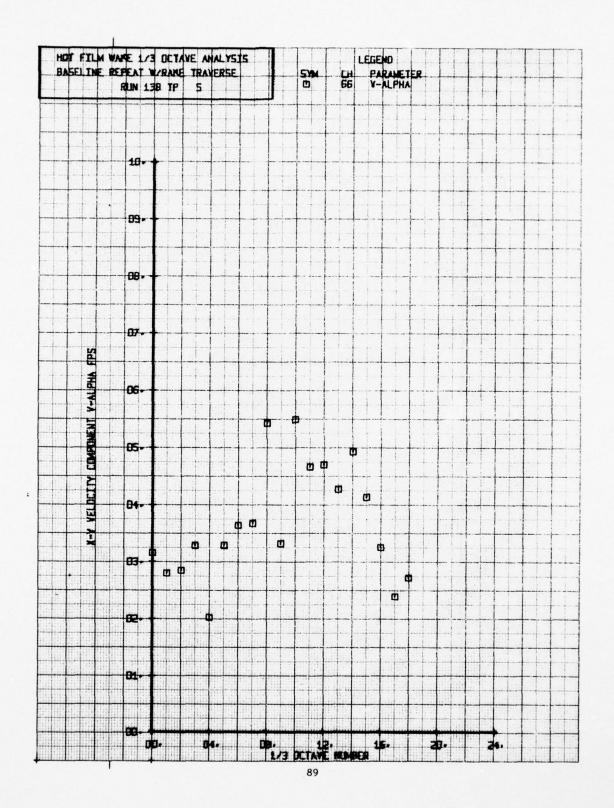


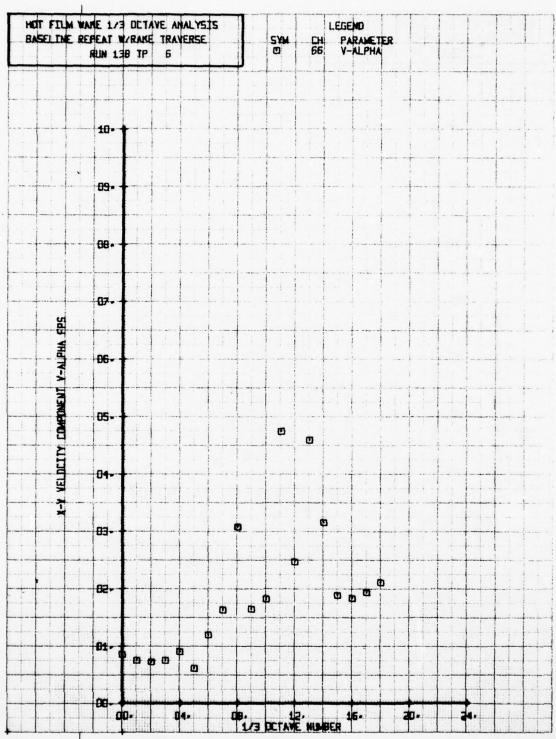


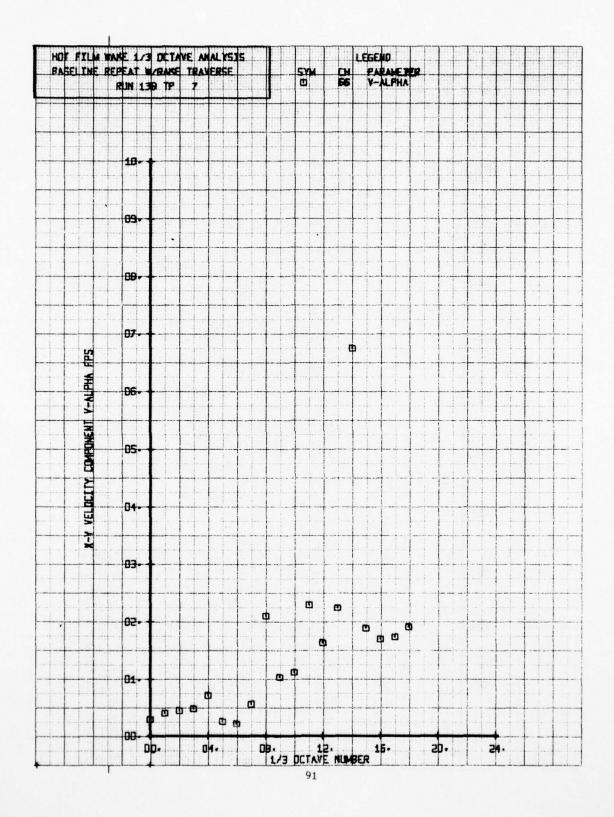


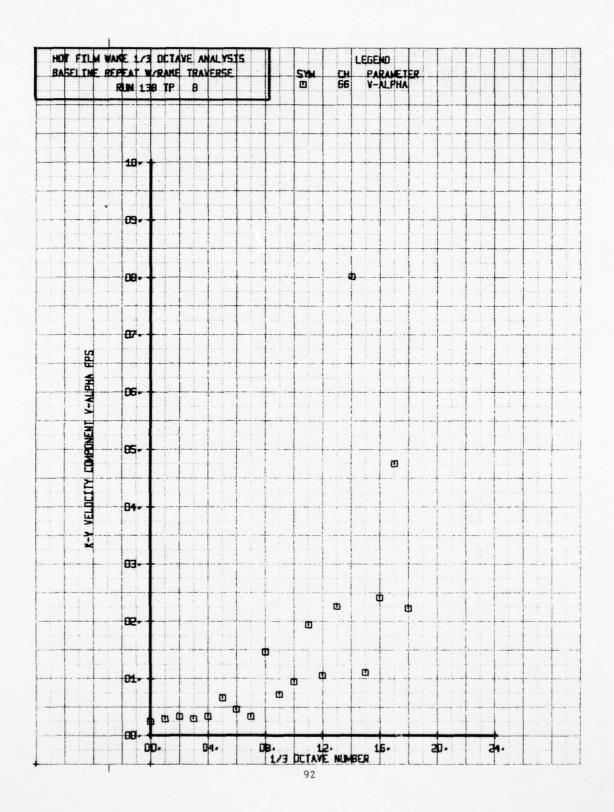


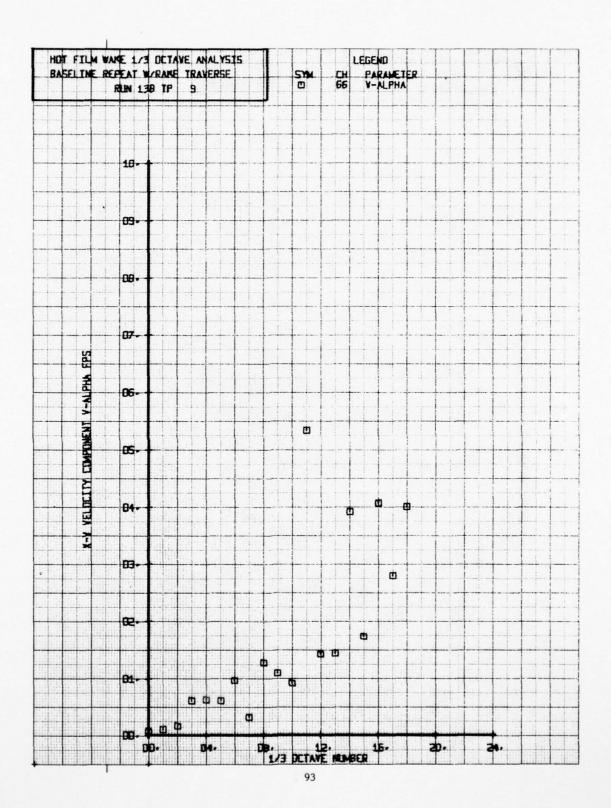


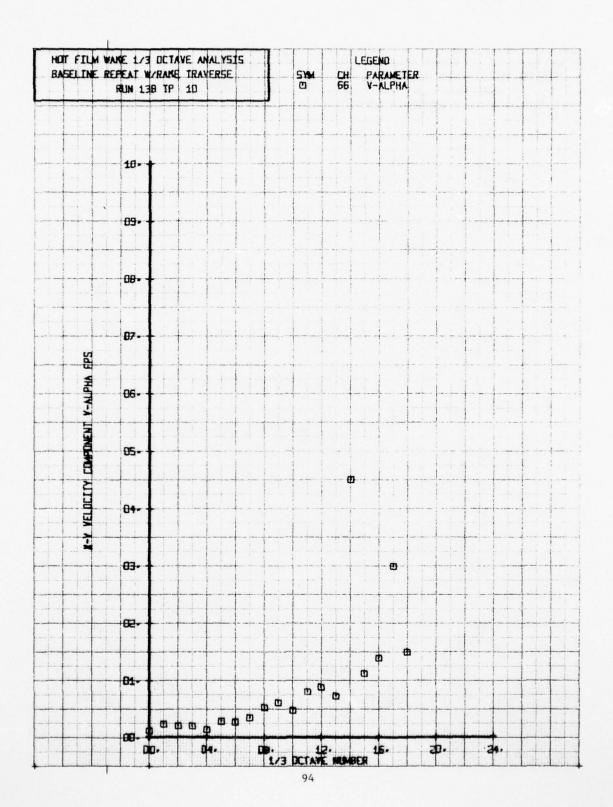


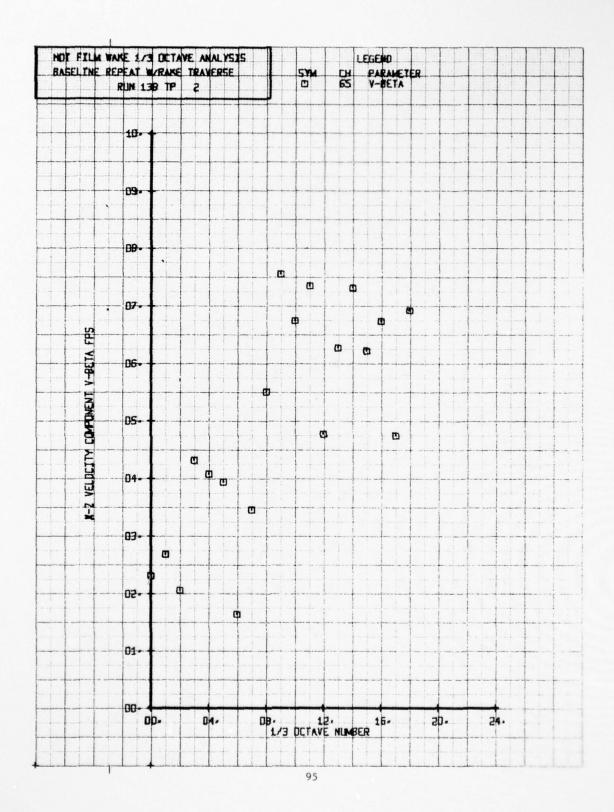


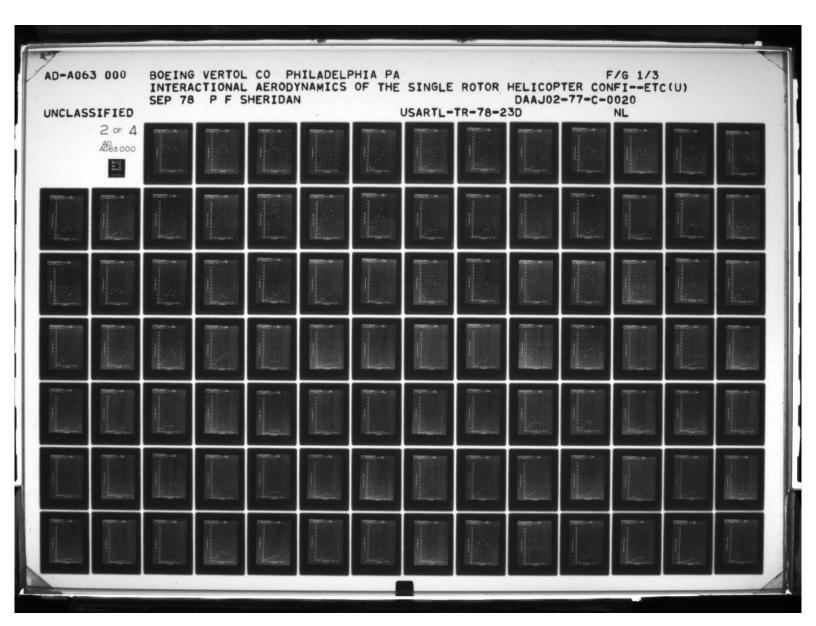


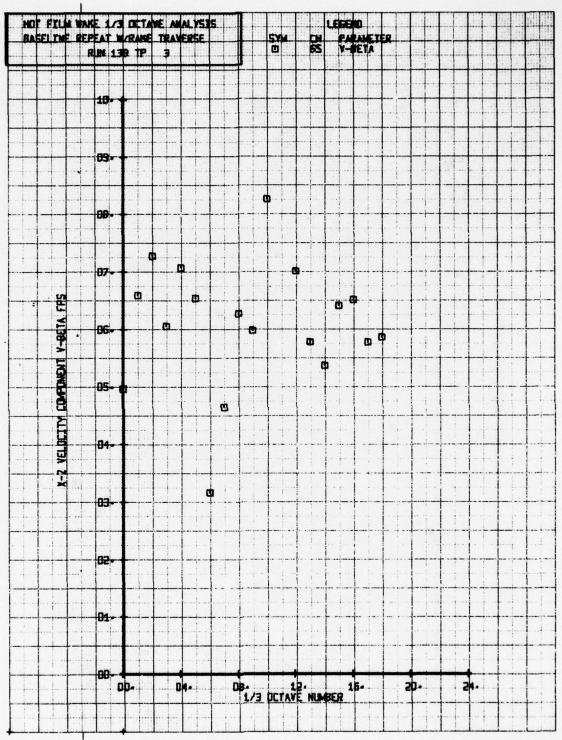


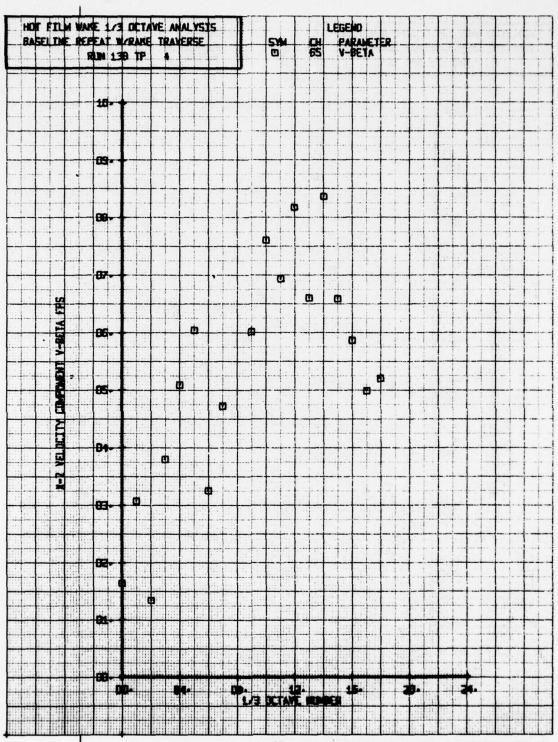


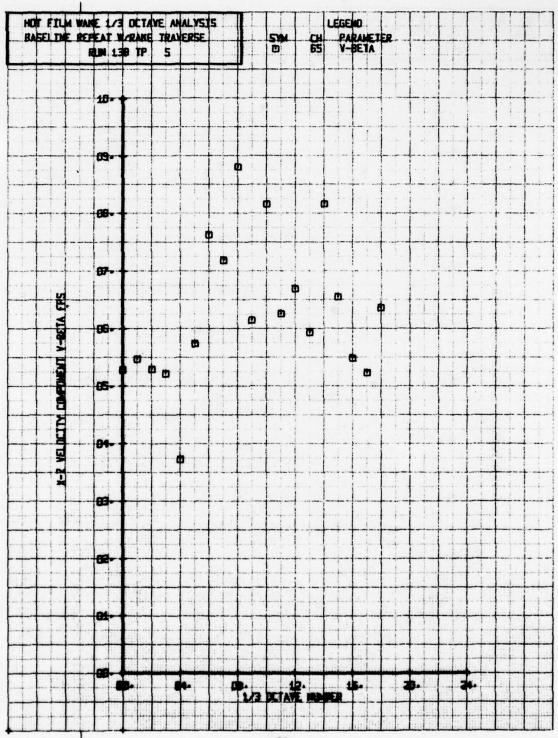


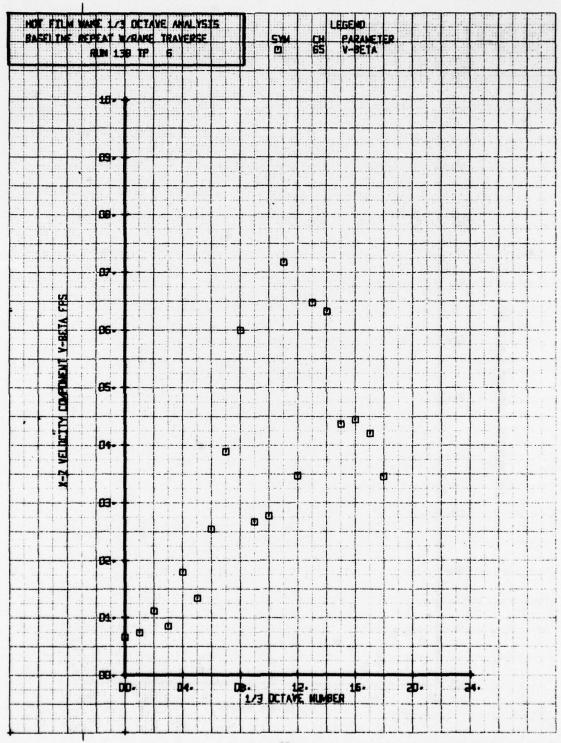


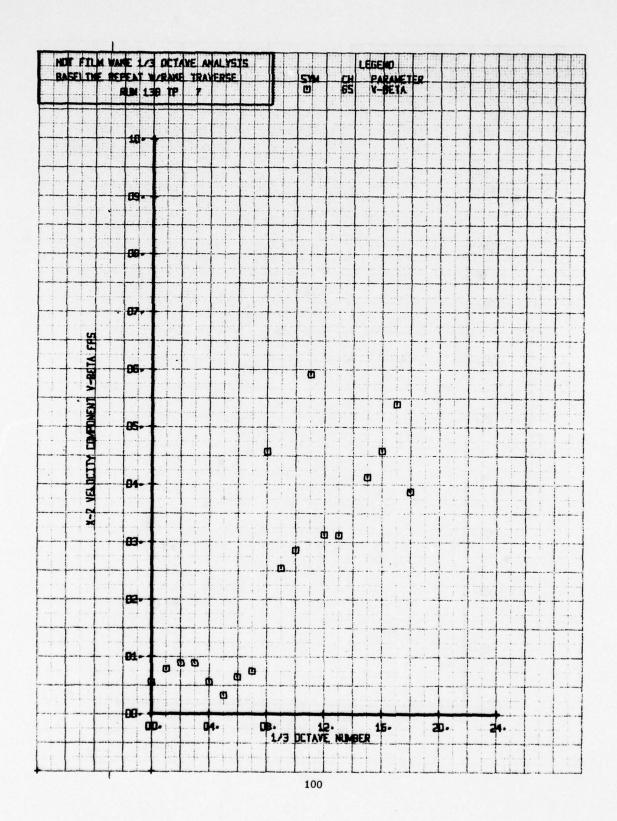


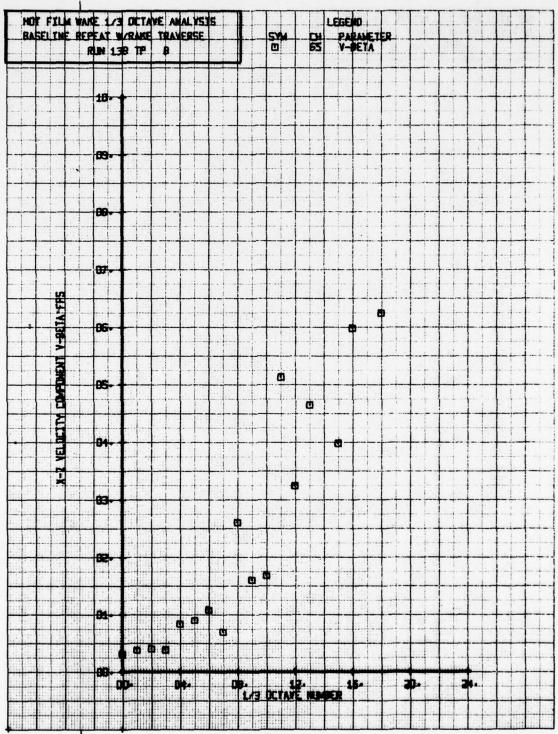


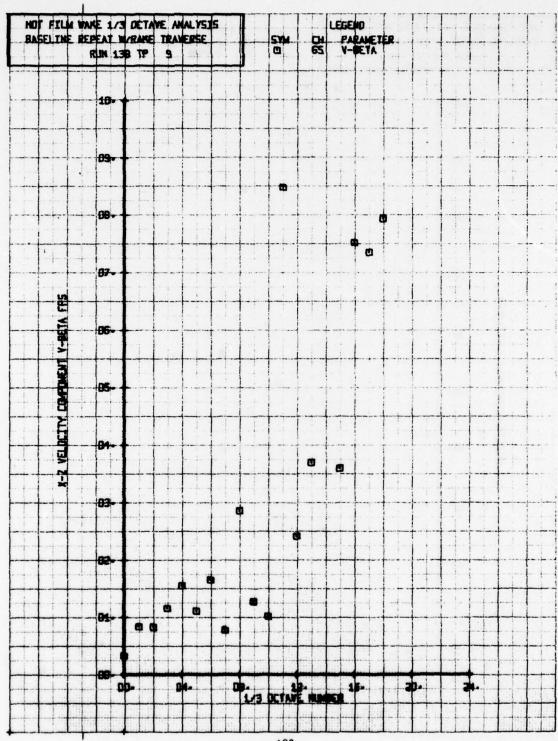


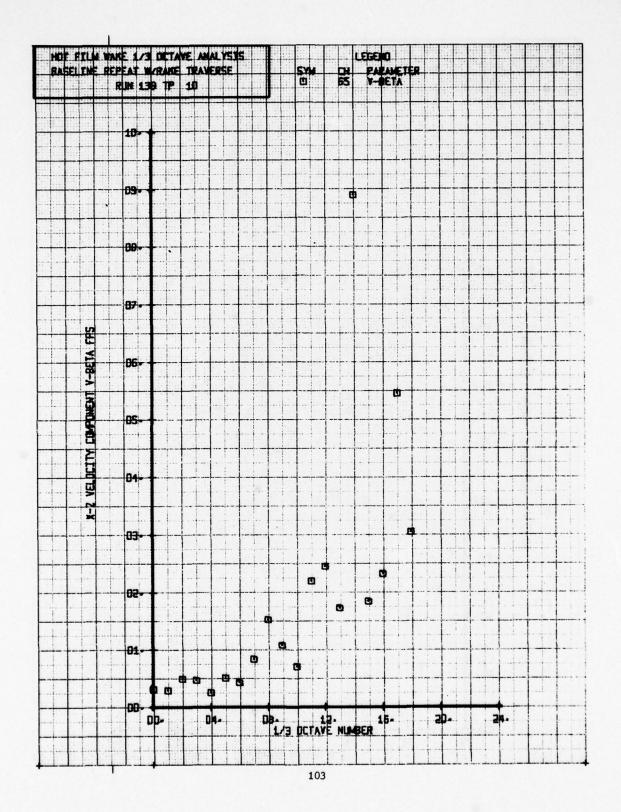


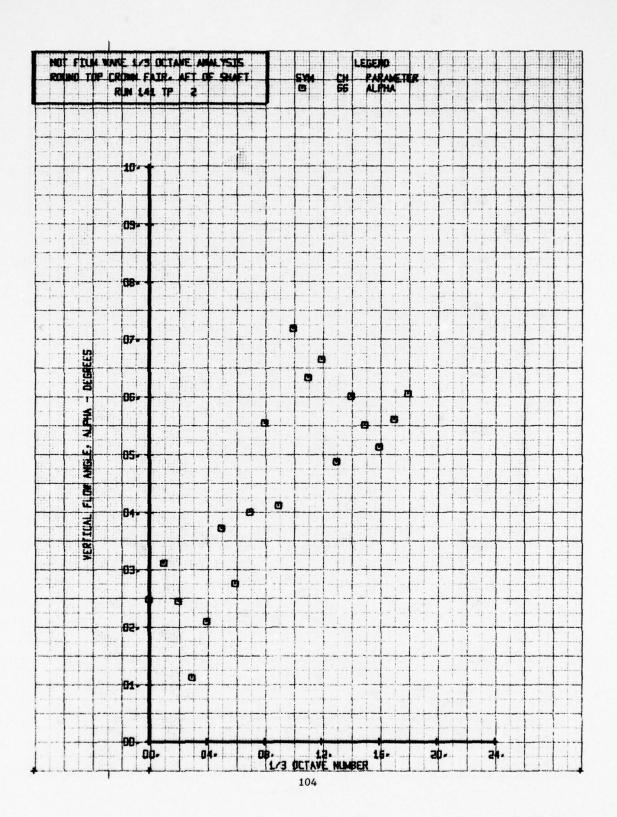


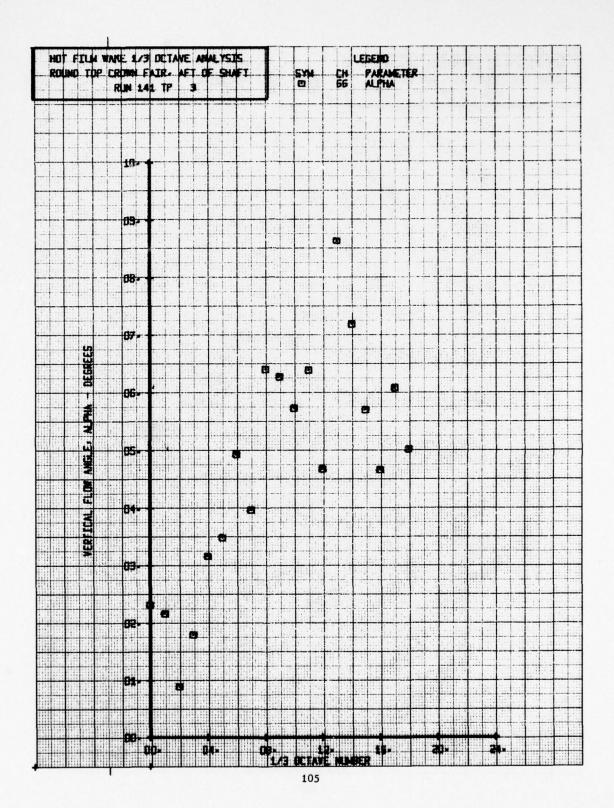


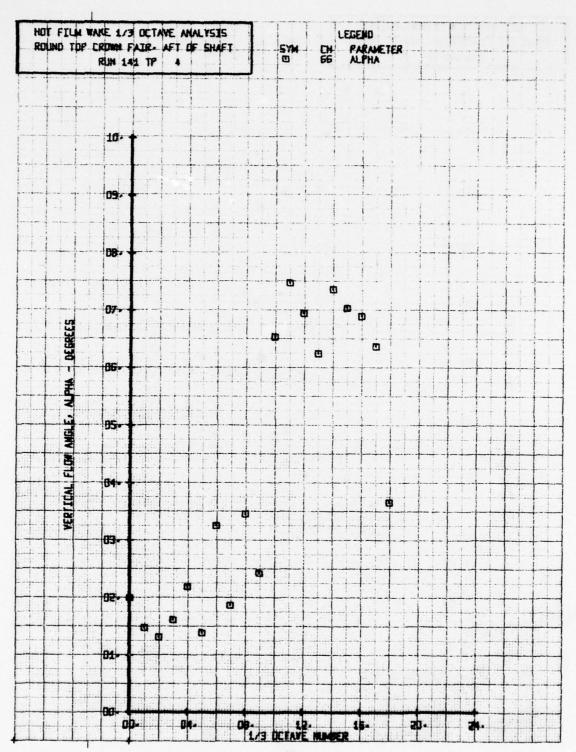


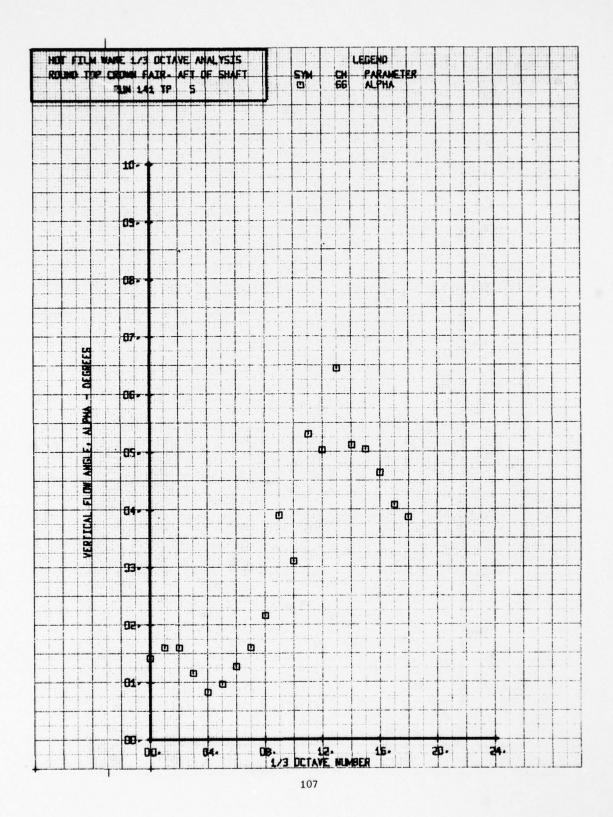


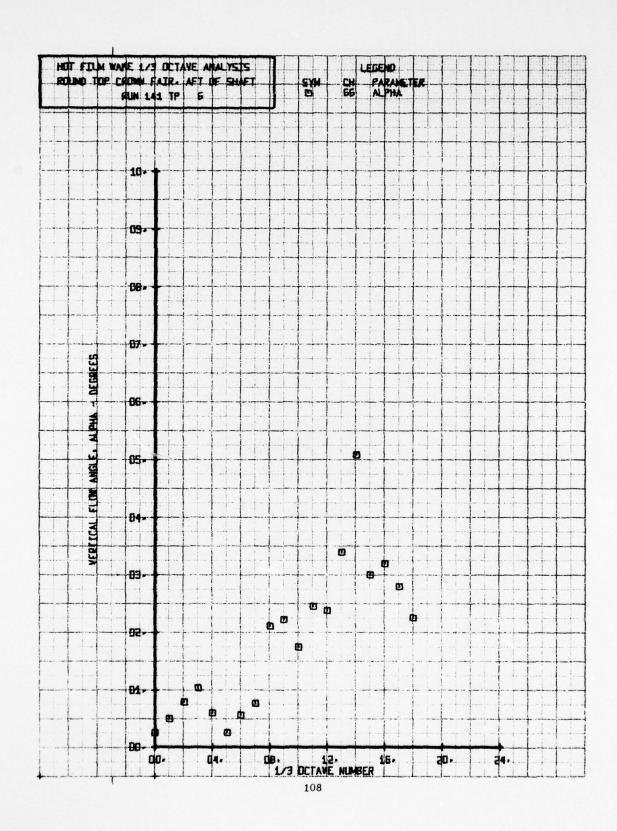


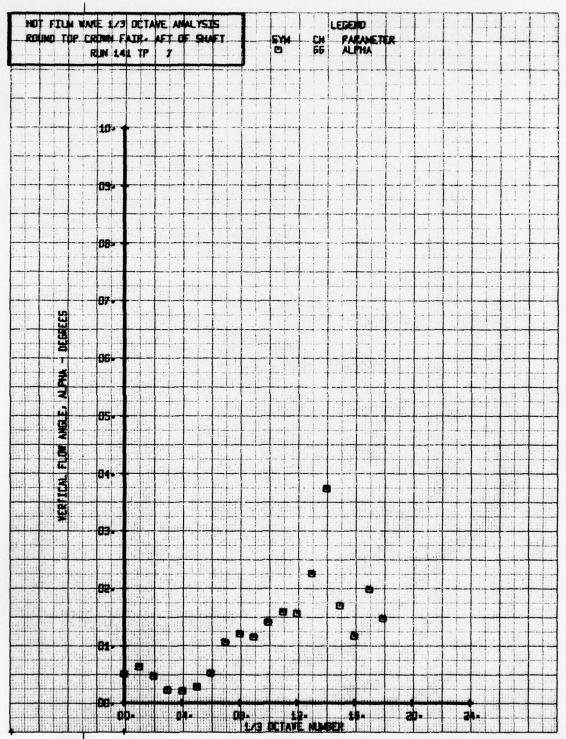


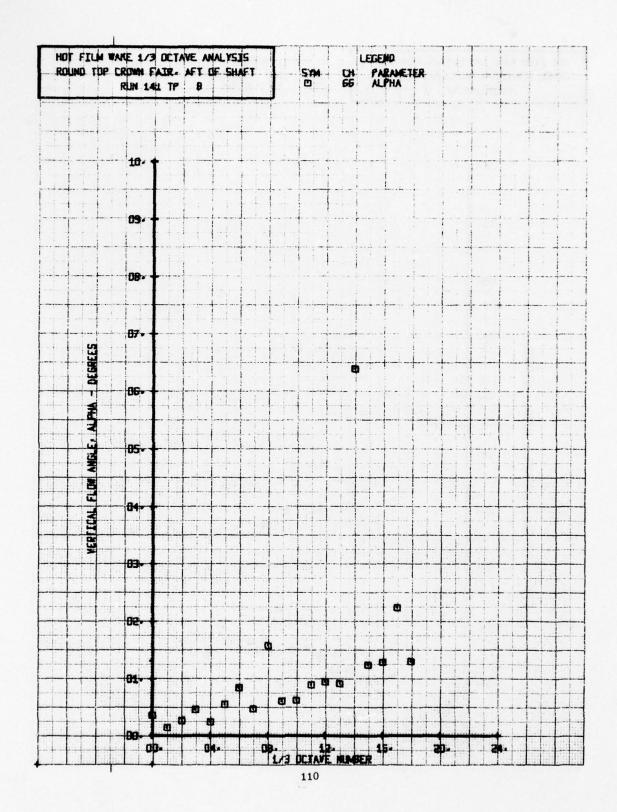


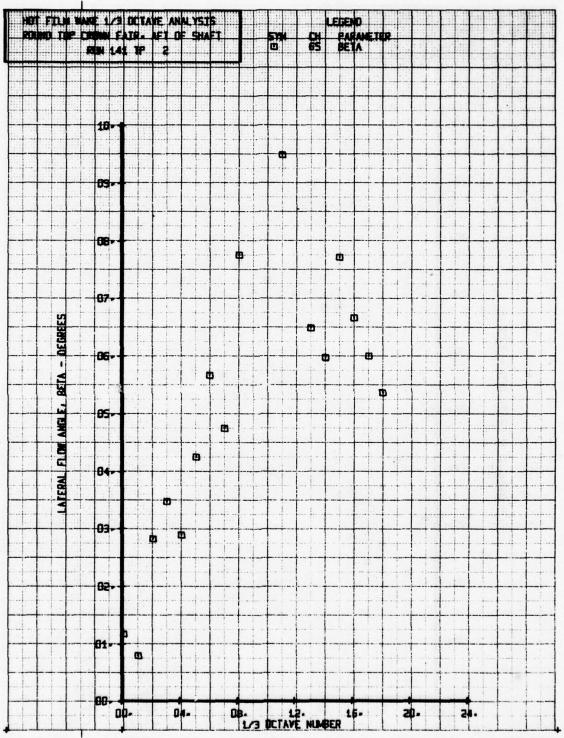


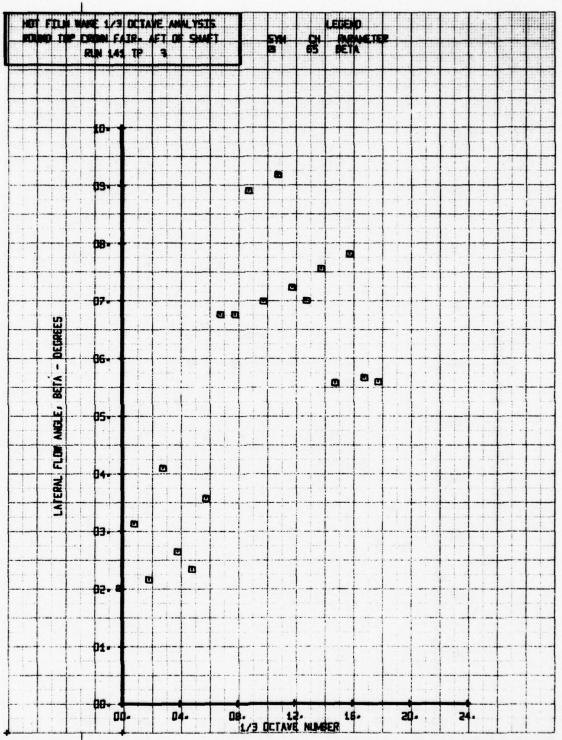


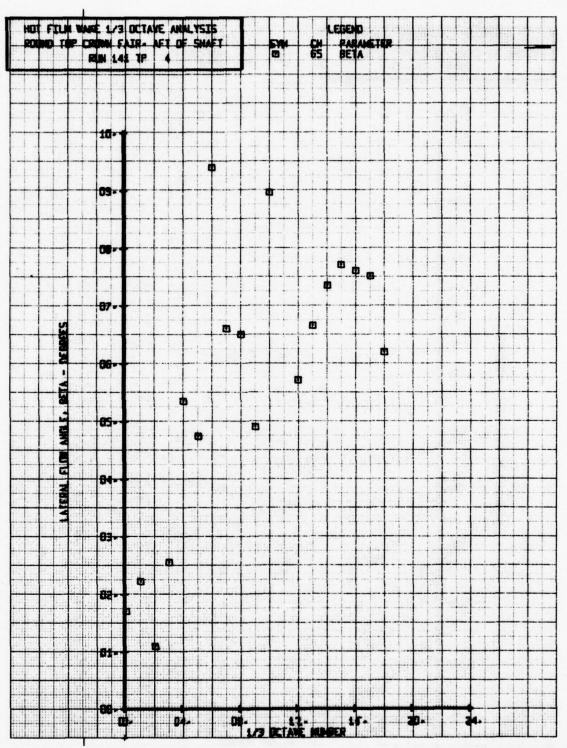


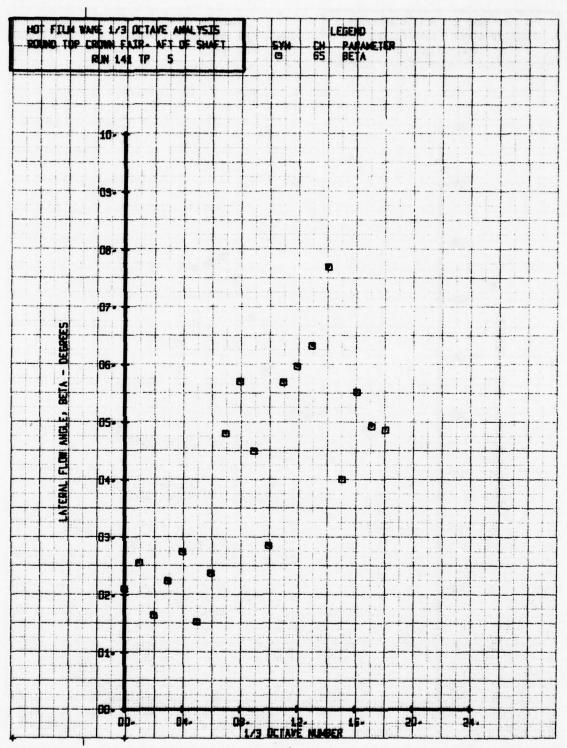


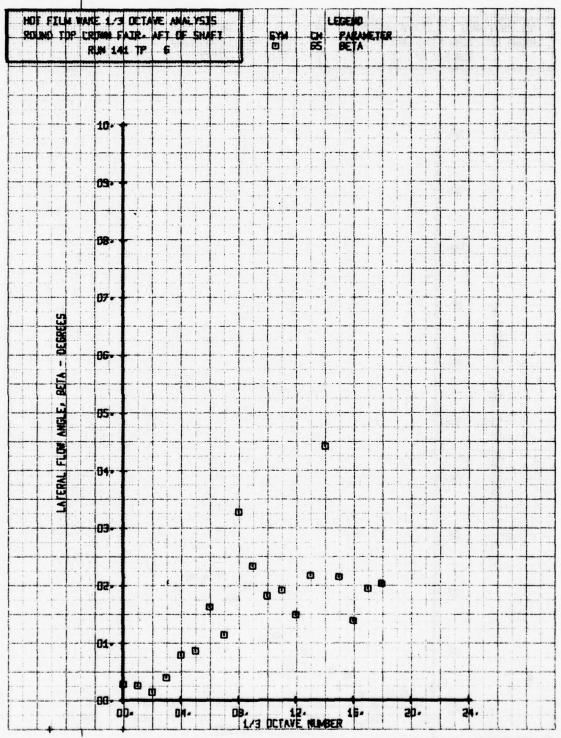


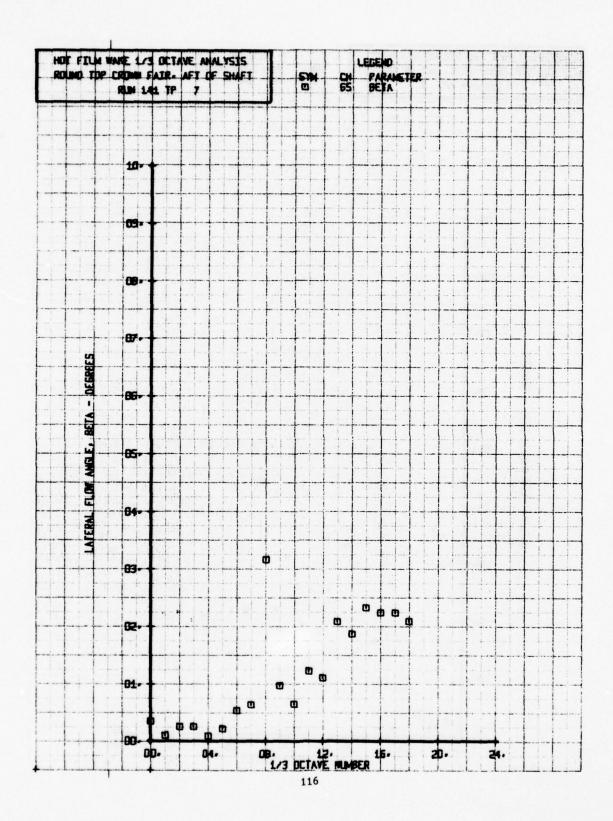


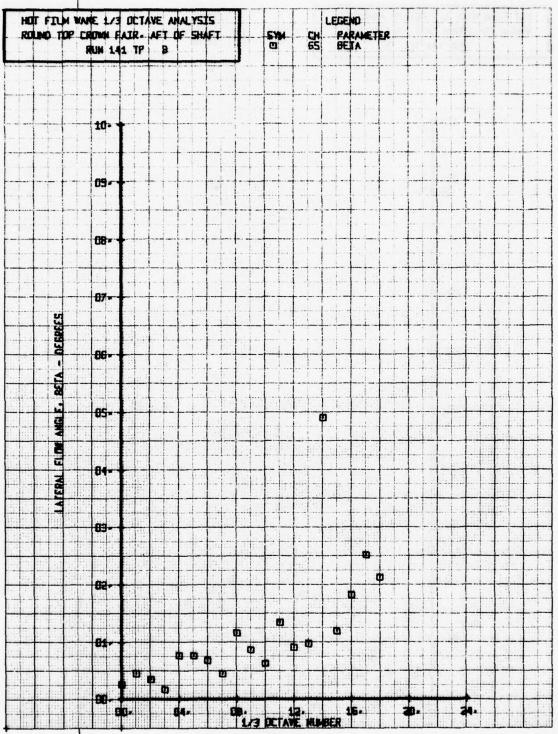


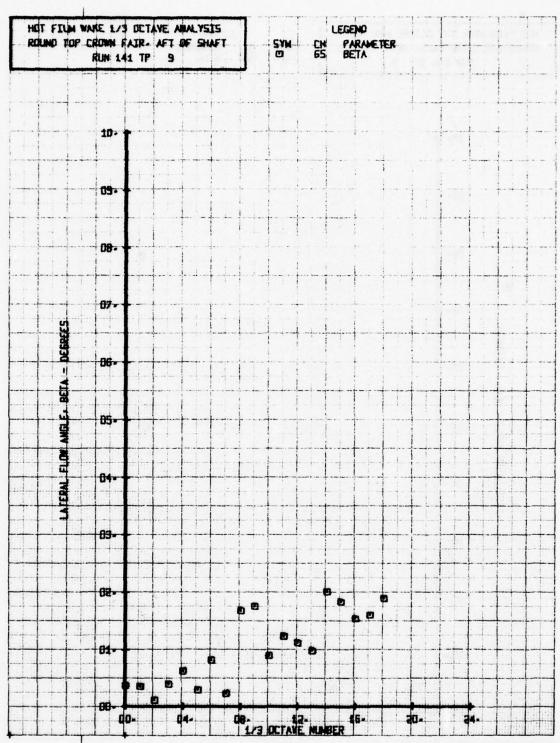


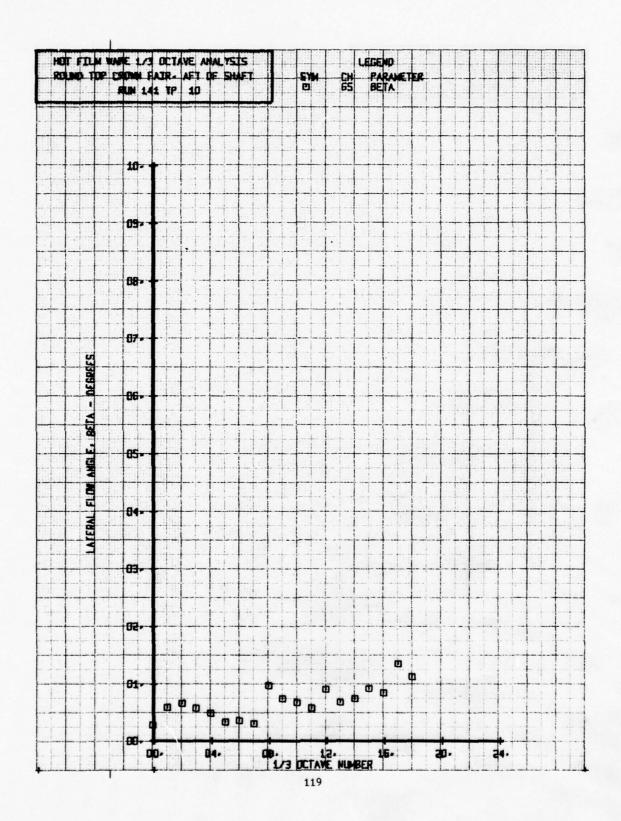


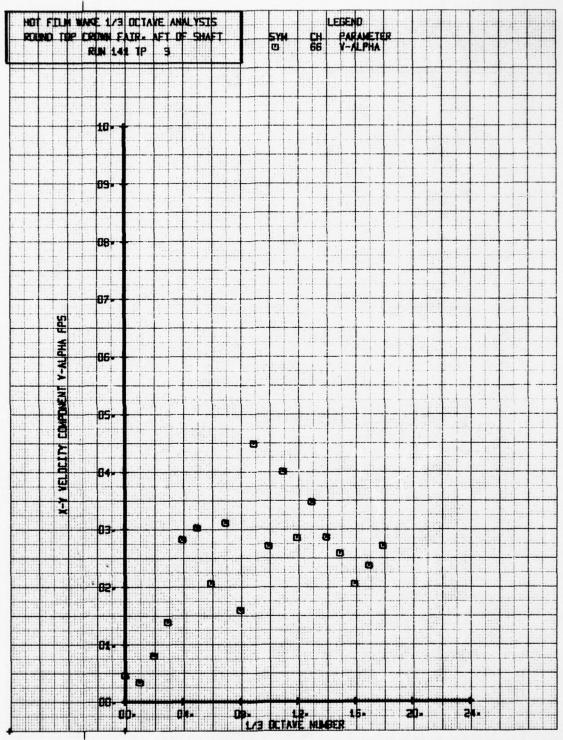


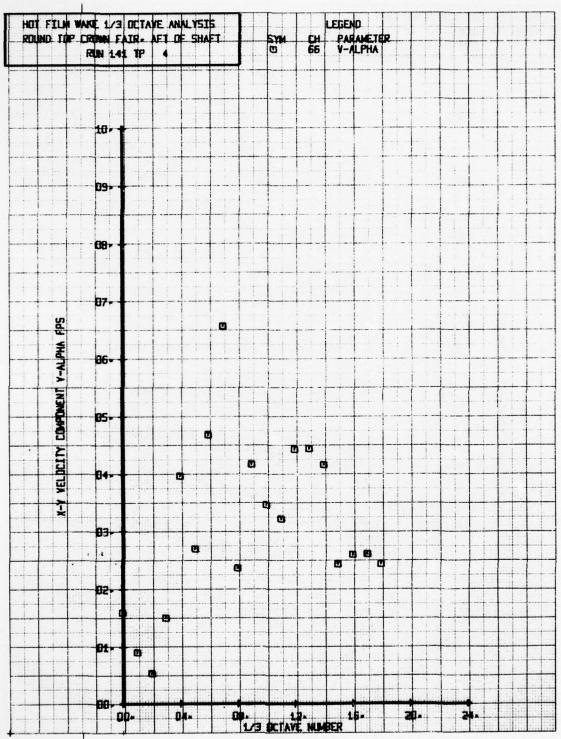


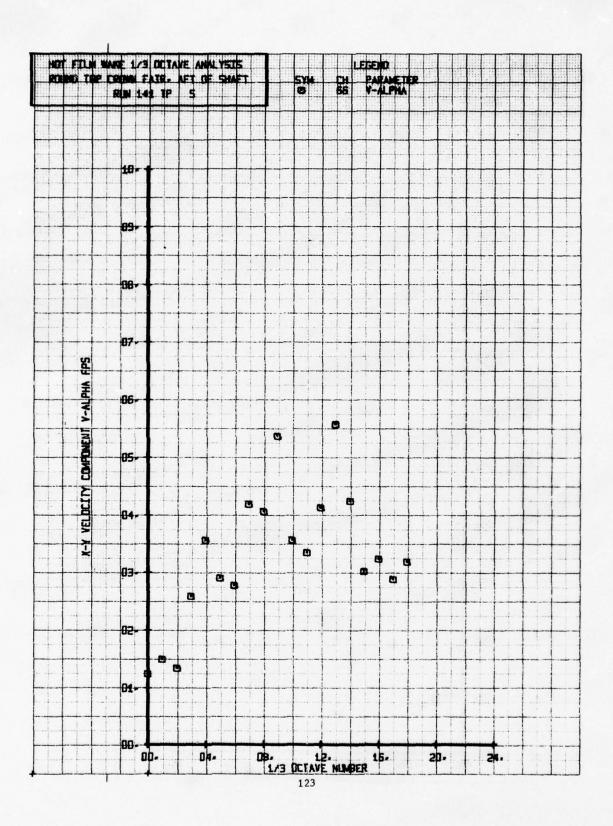


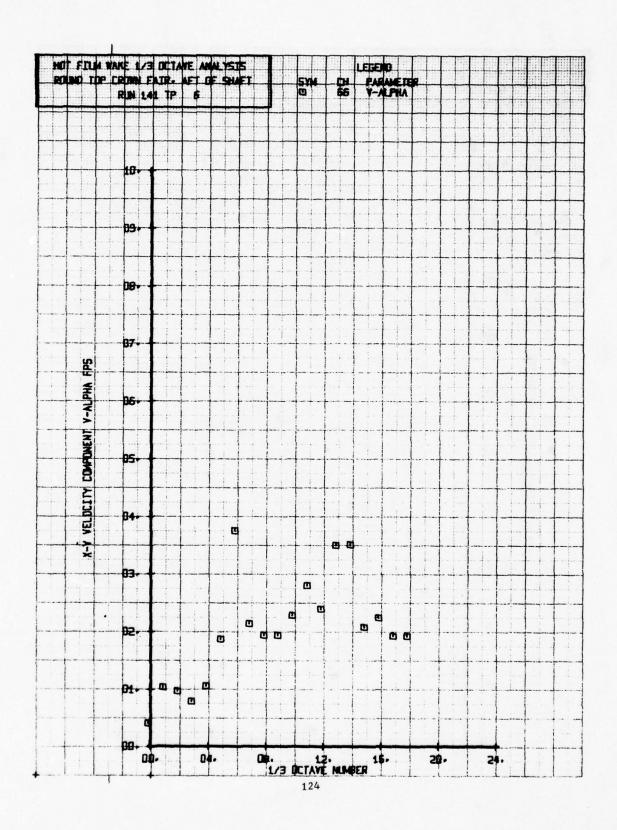


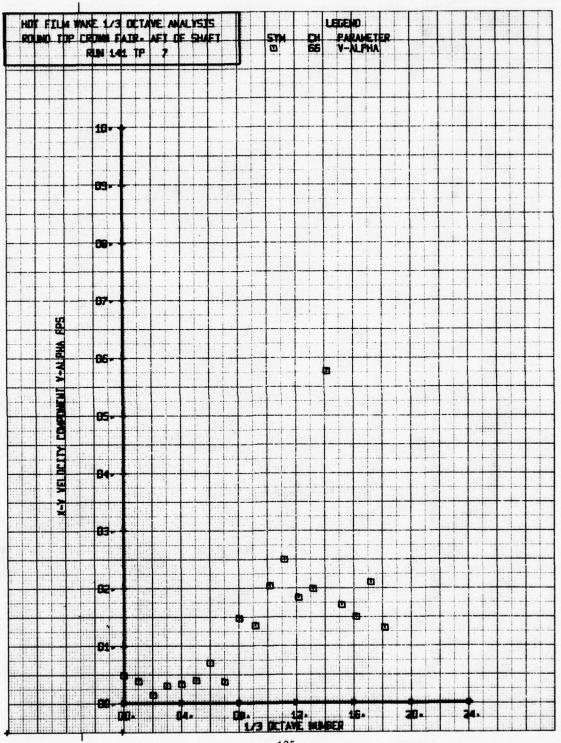


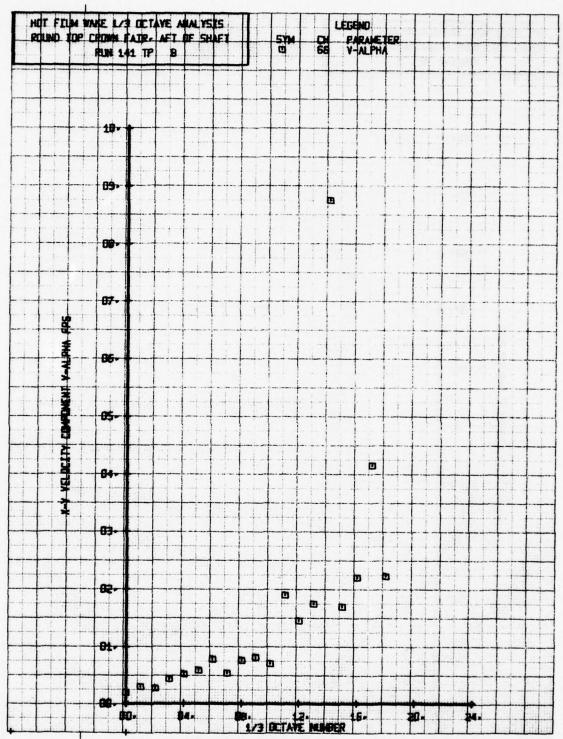


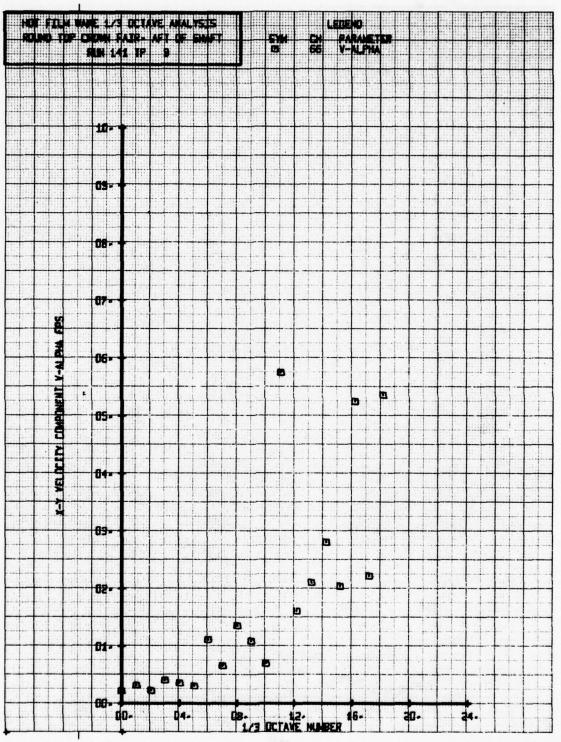


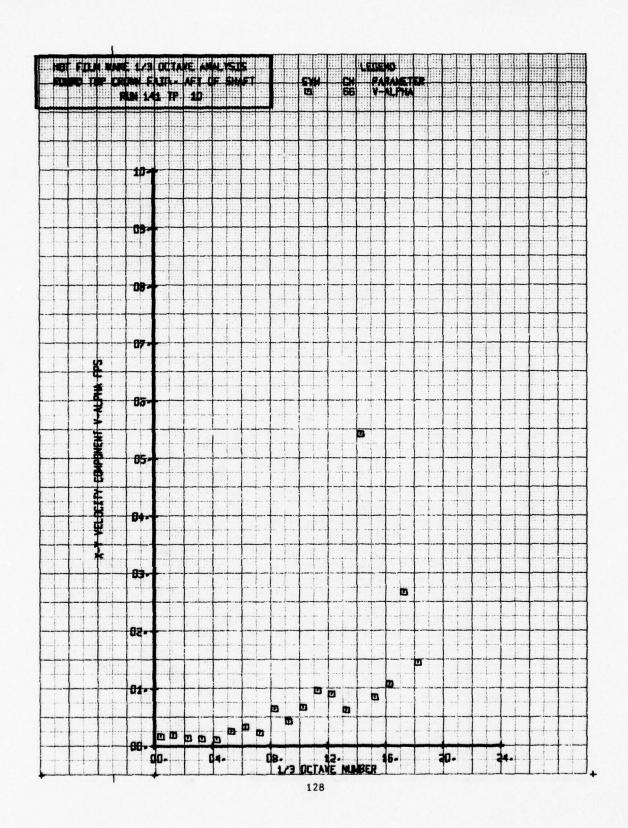


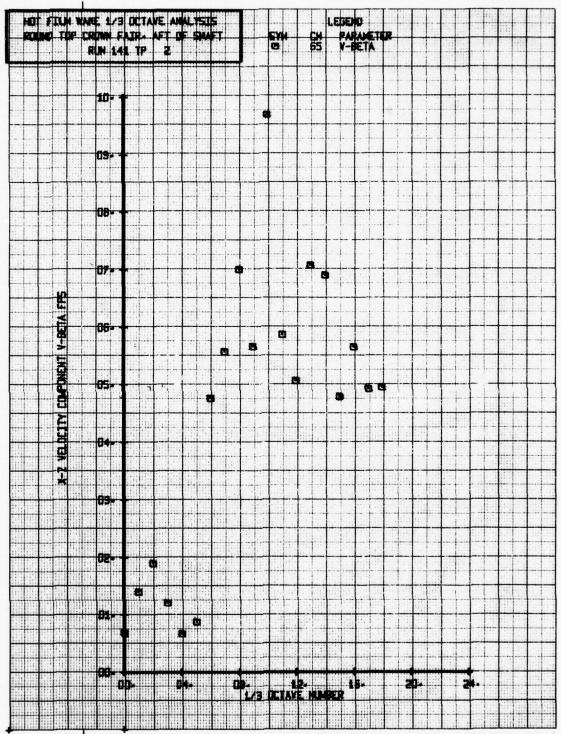










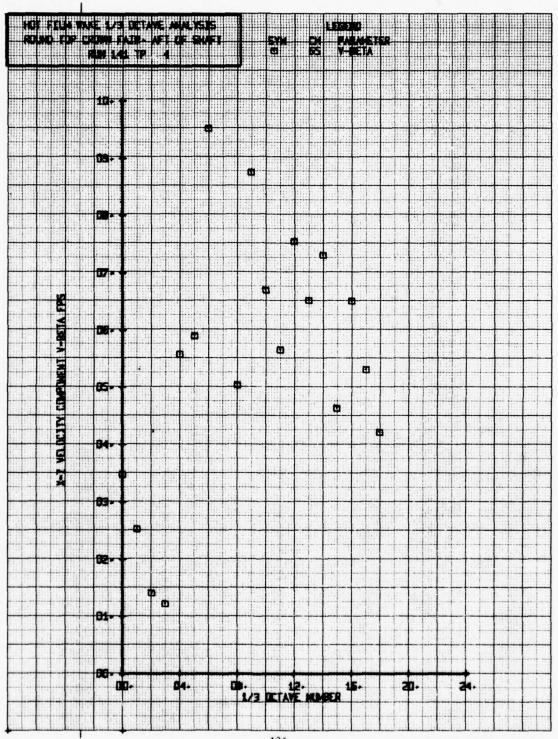


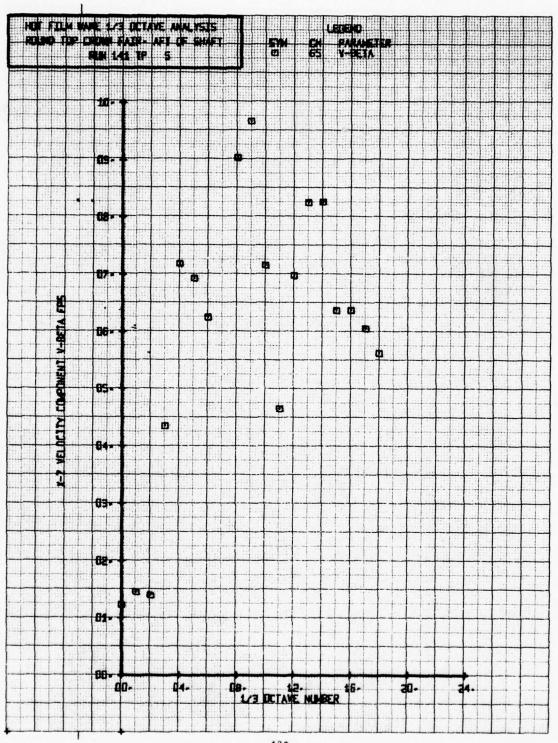
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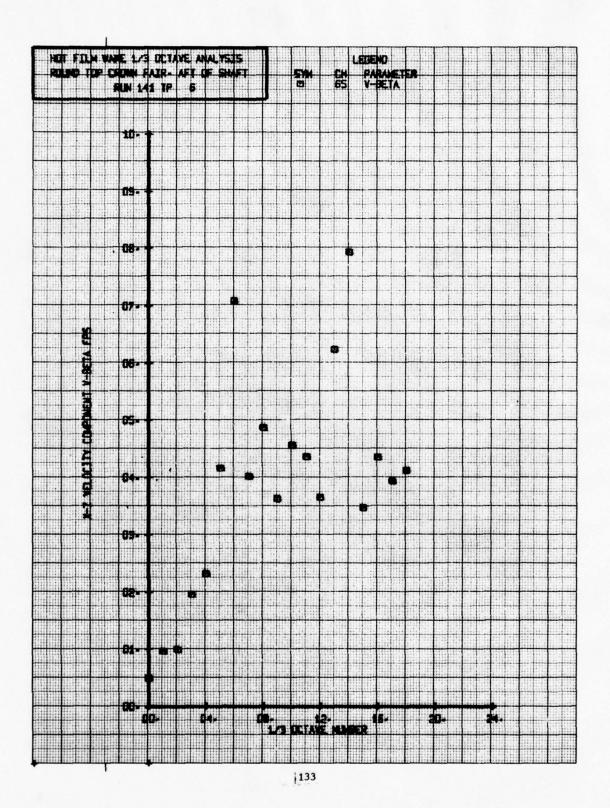
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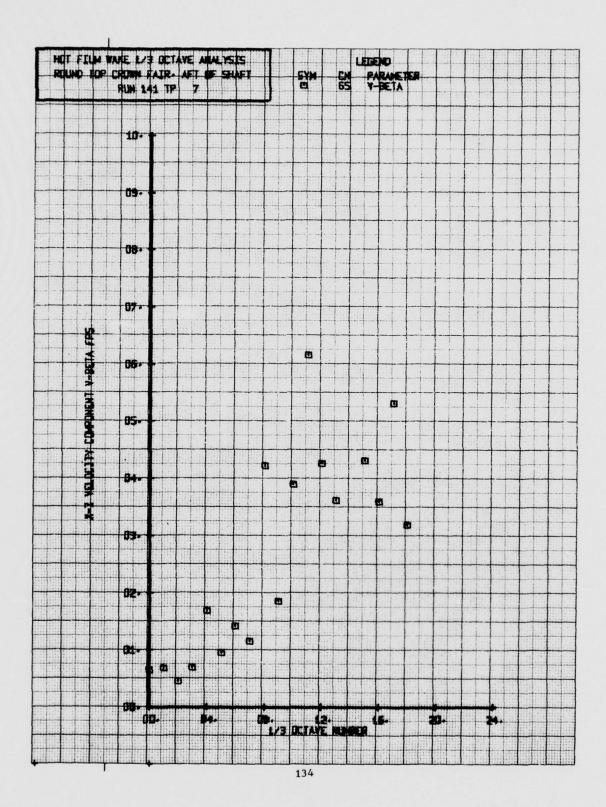
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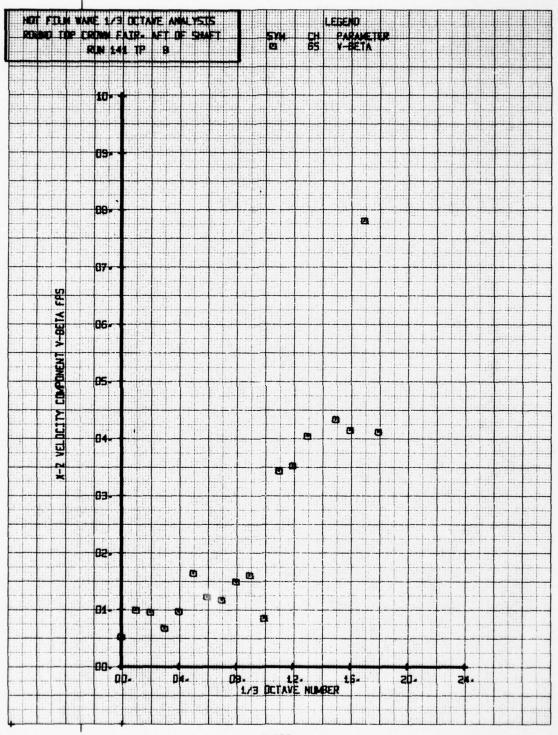
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ROUND FOR CROWN FAIR. AFT OF SHAFT
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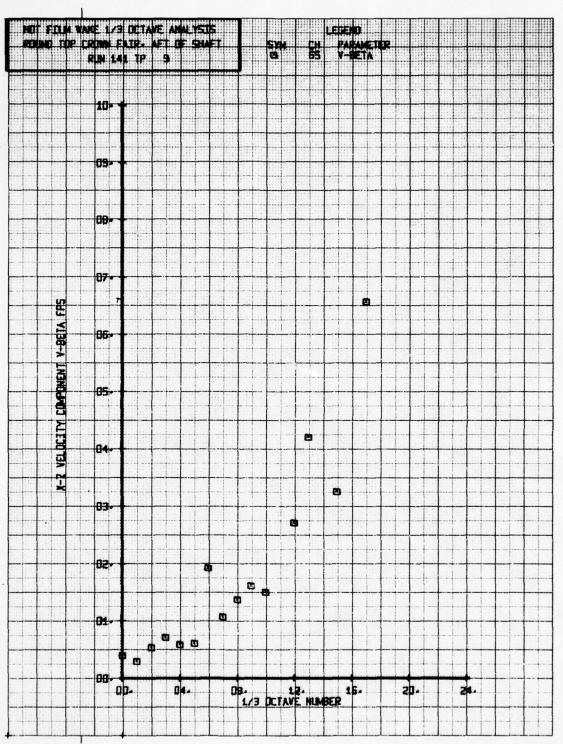


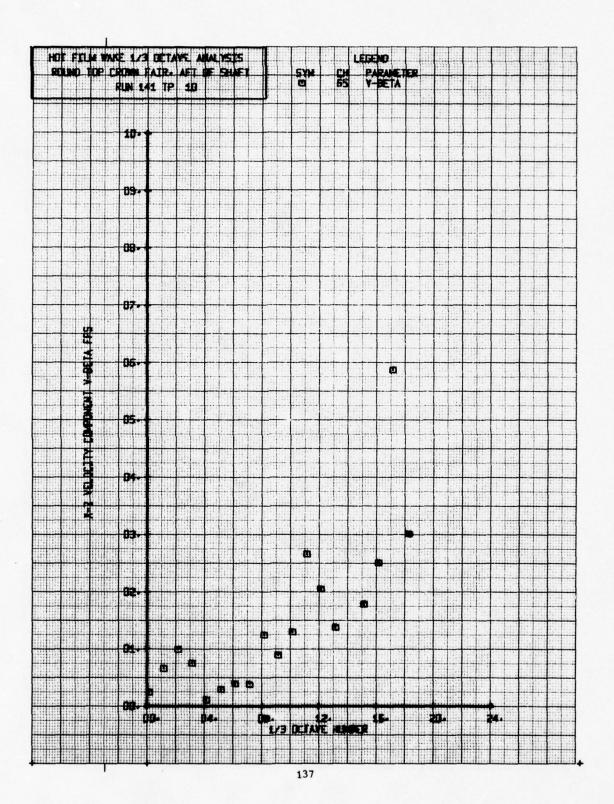


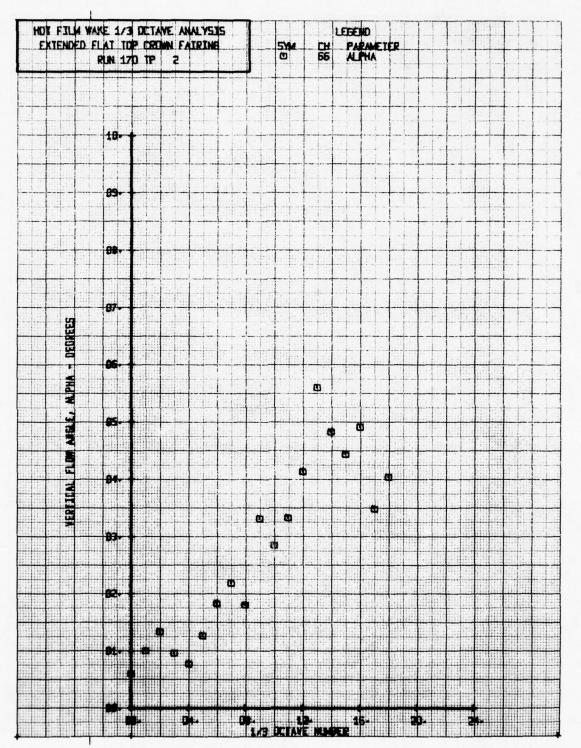


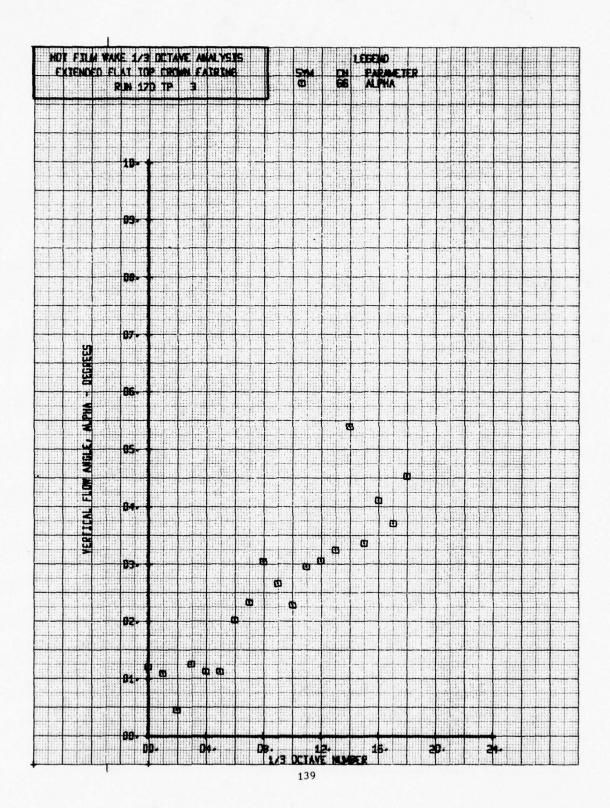


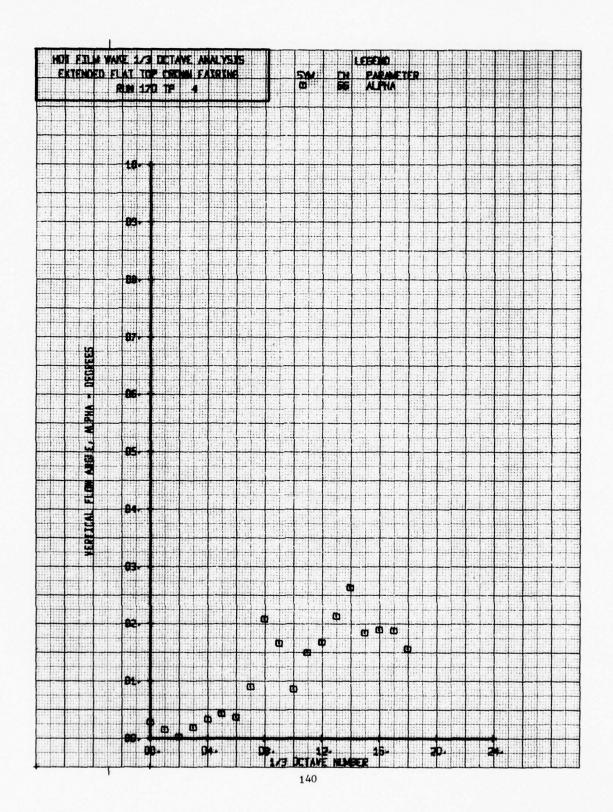


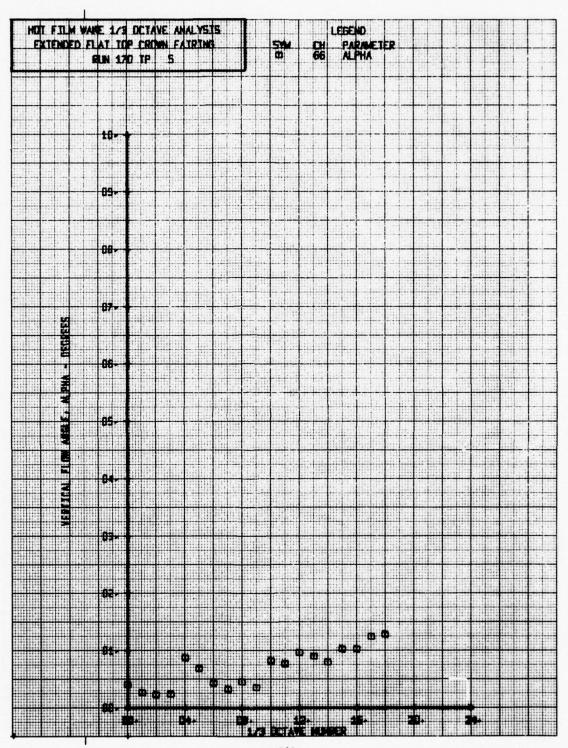


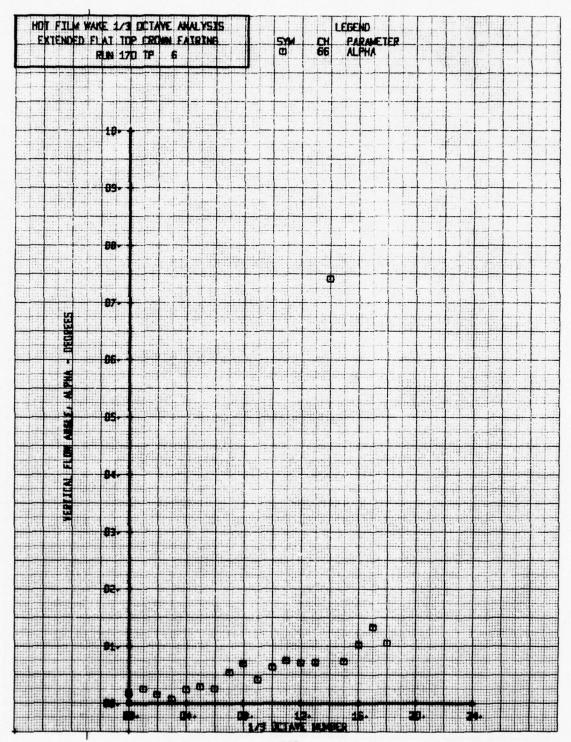


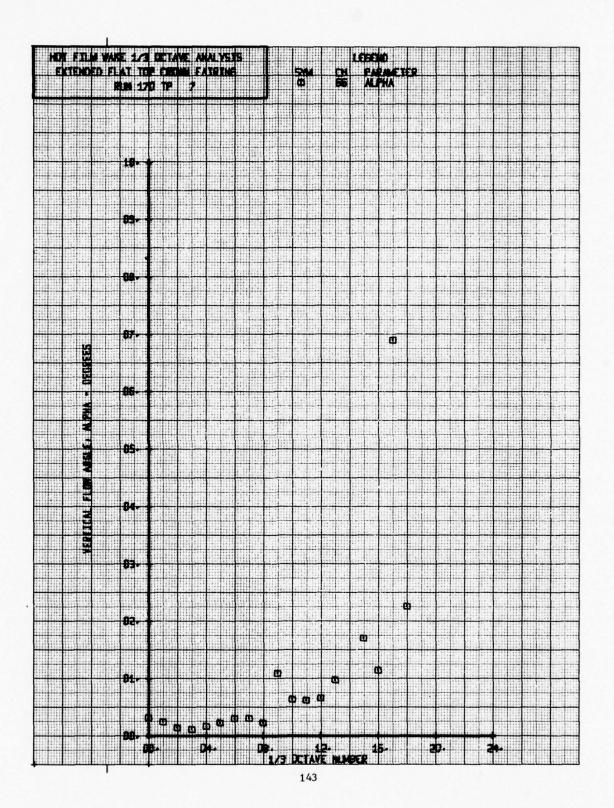


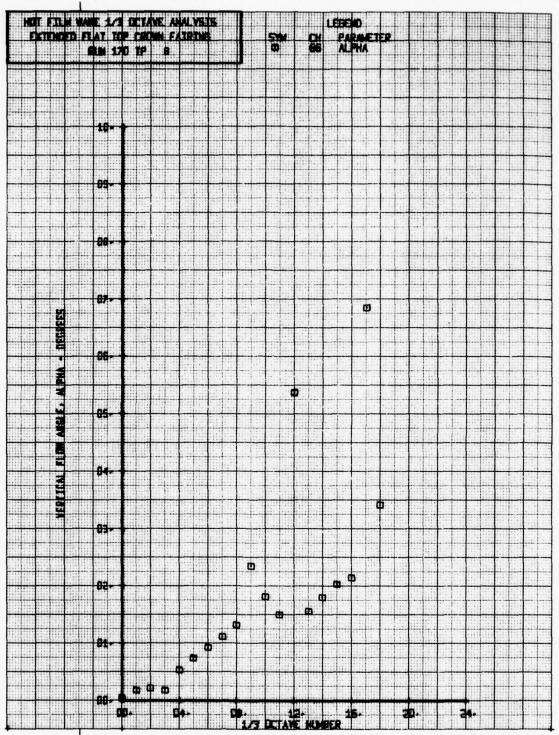


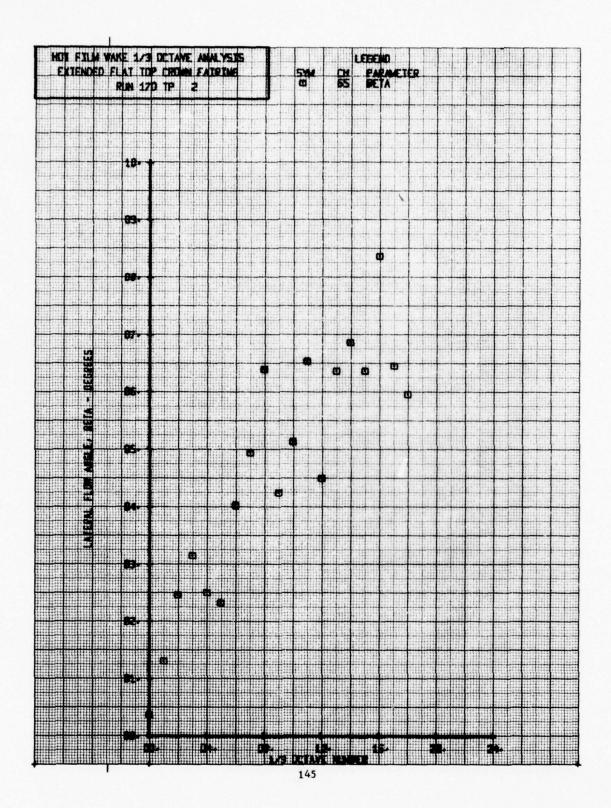


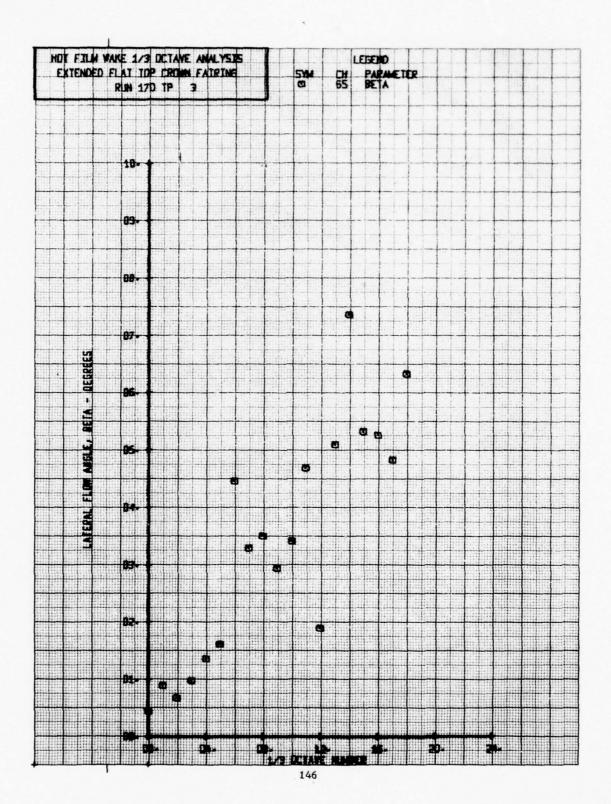


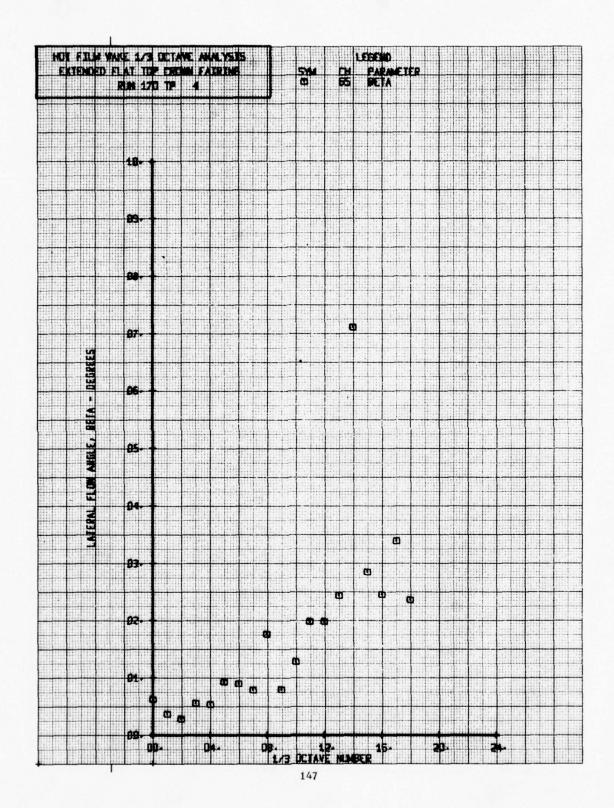


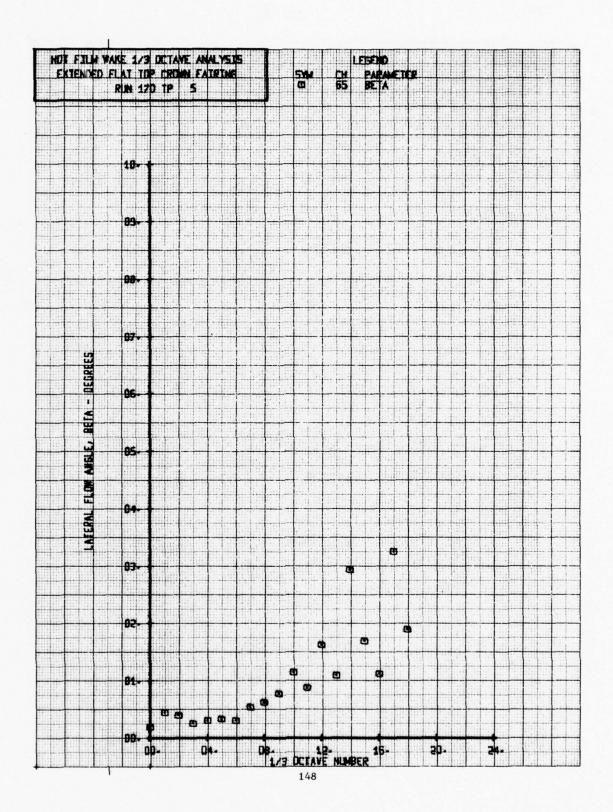


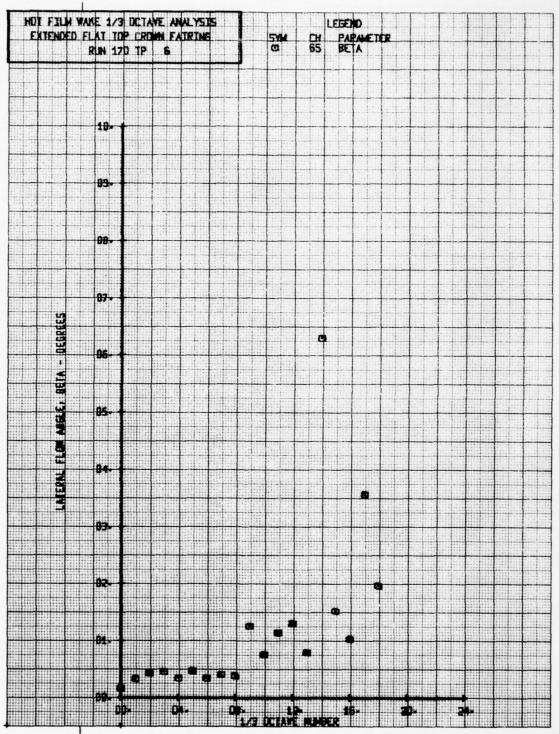


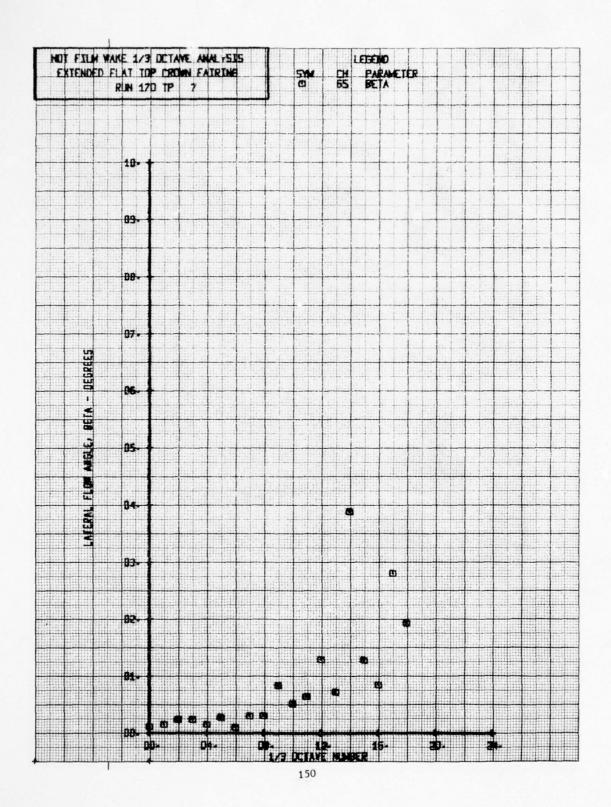


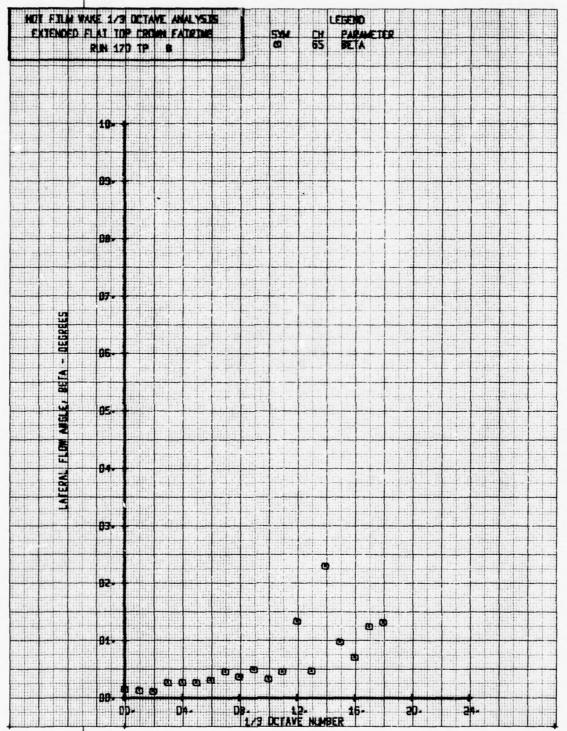


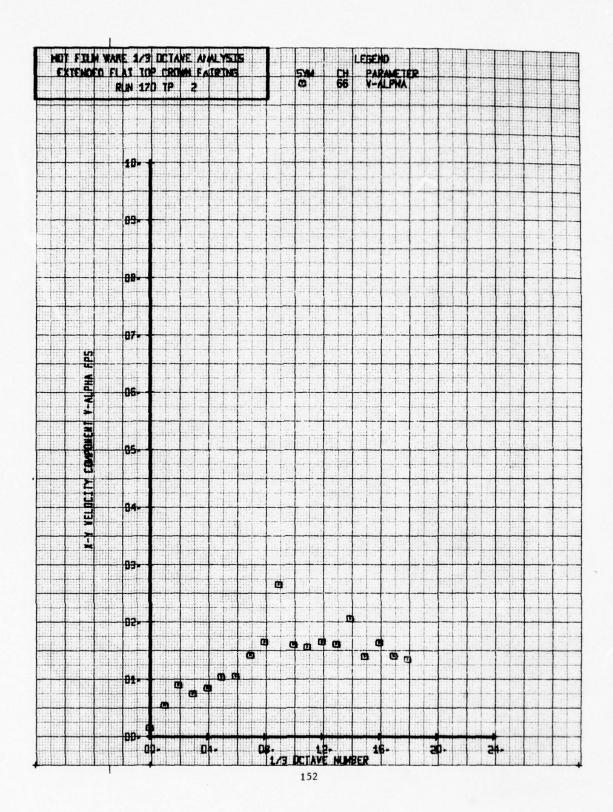


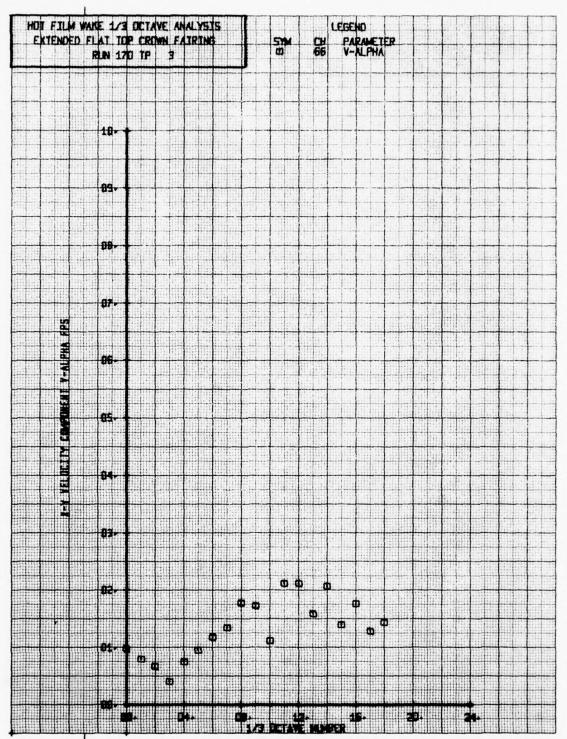


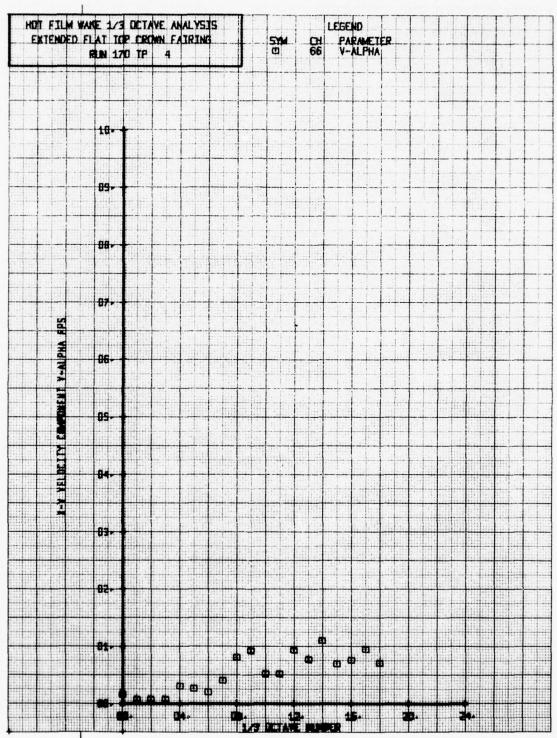


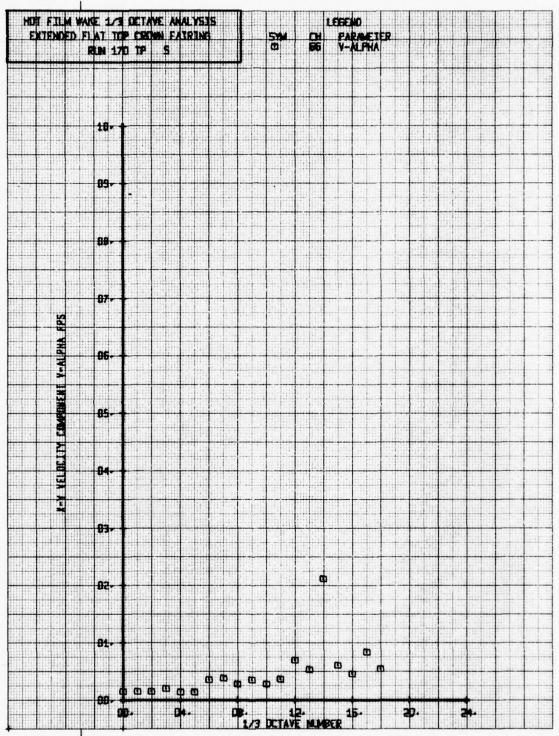


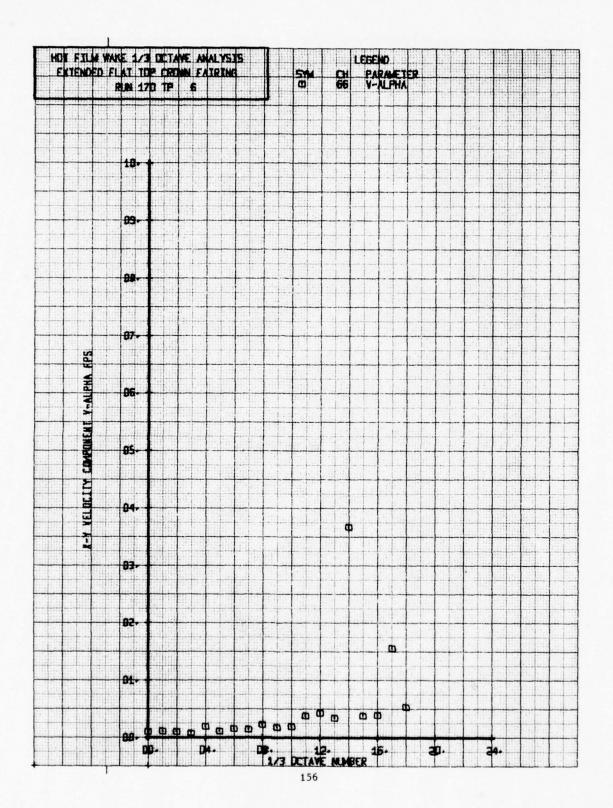


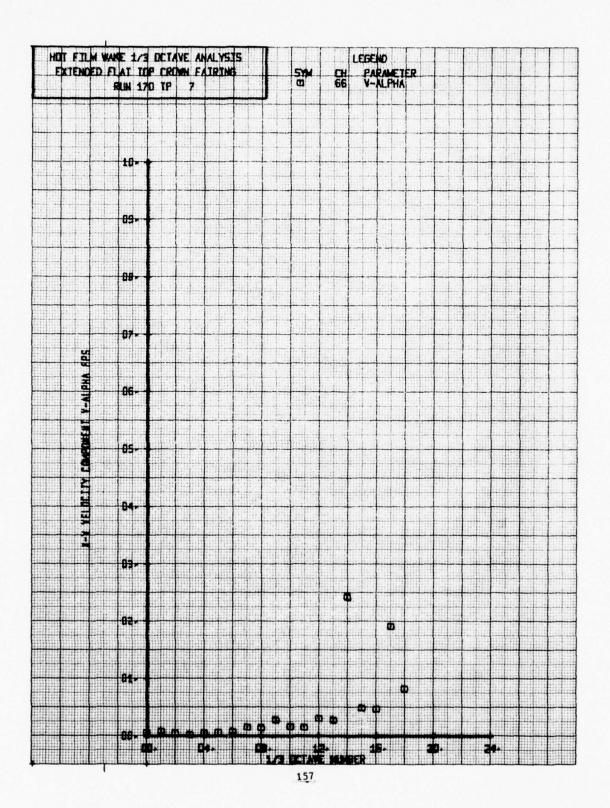


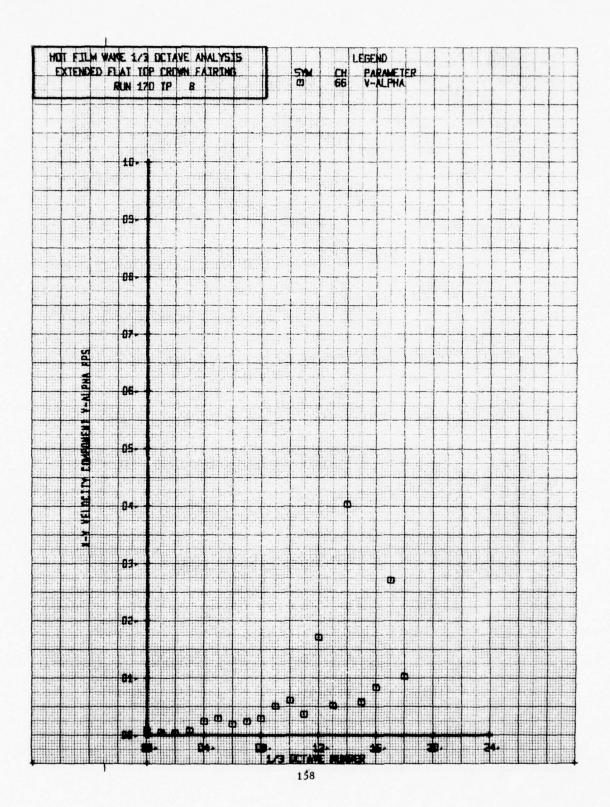


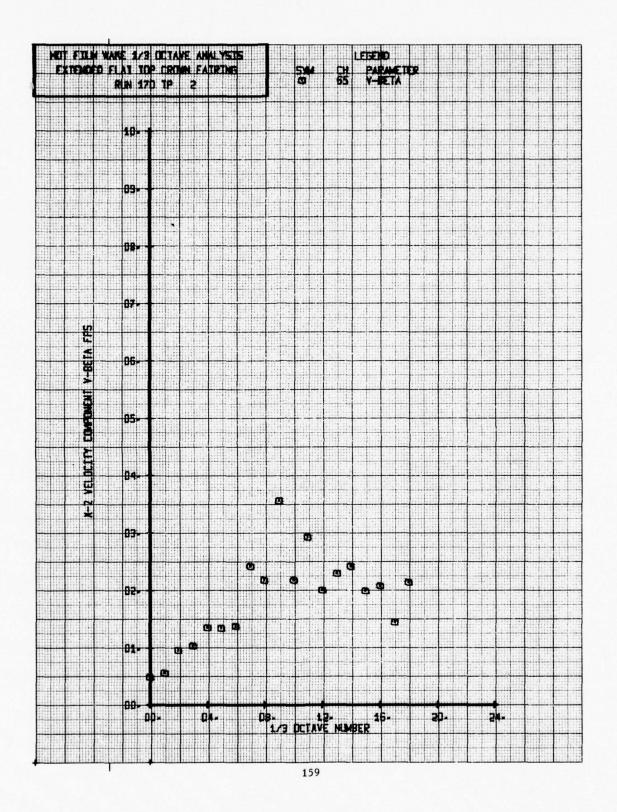


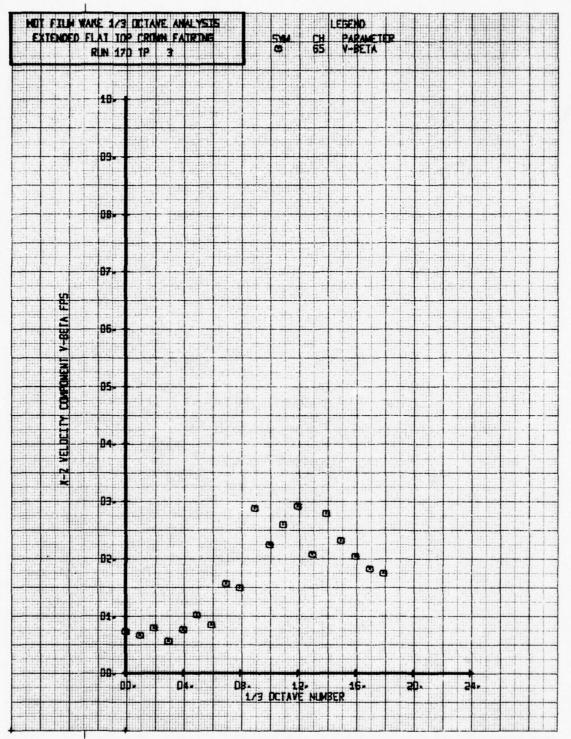


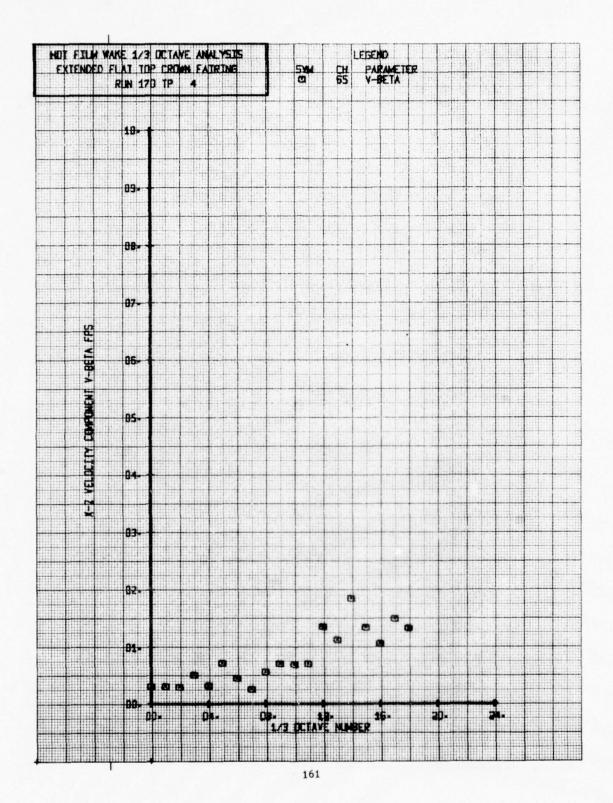


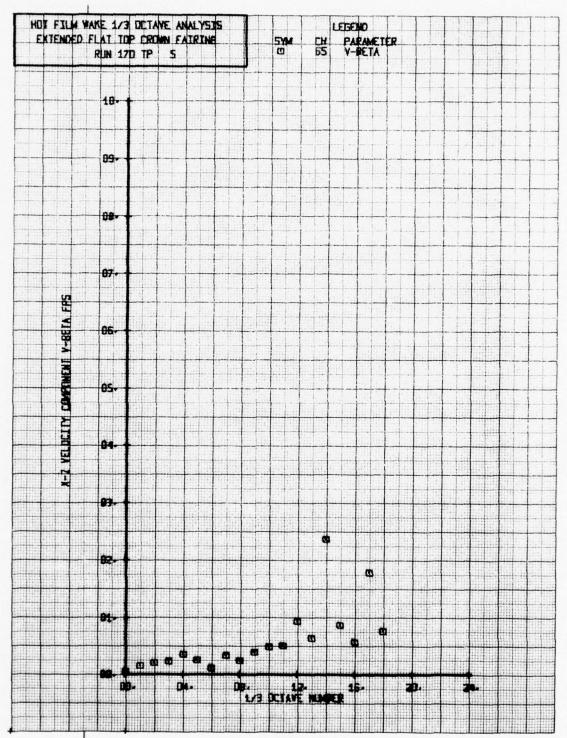


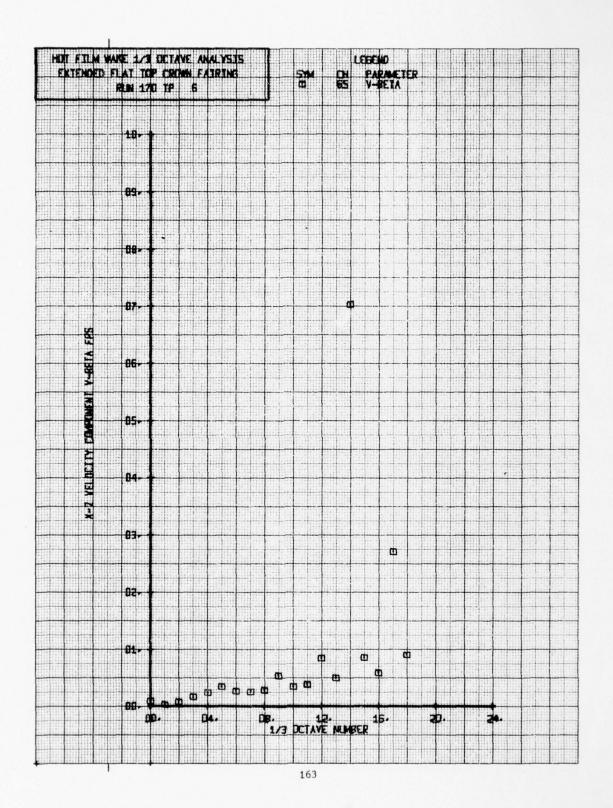


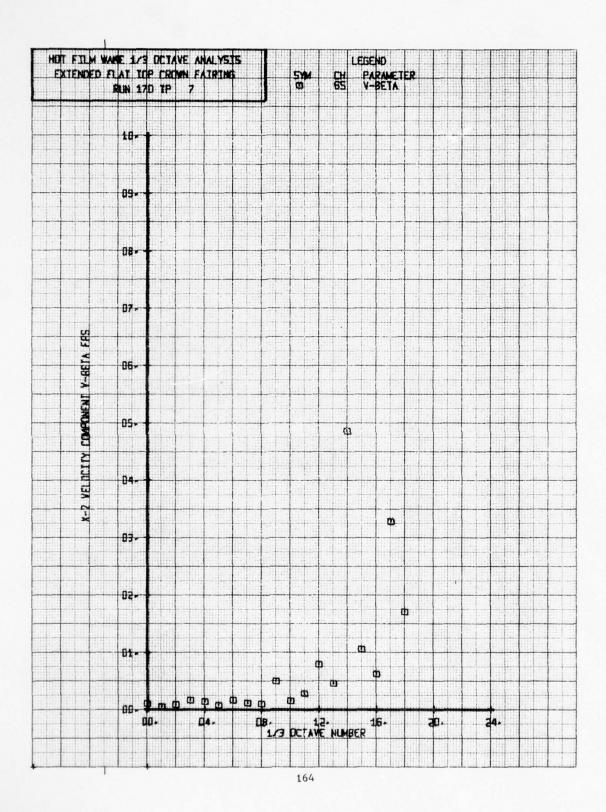


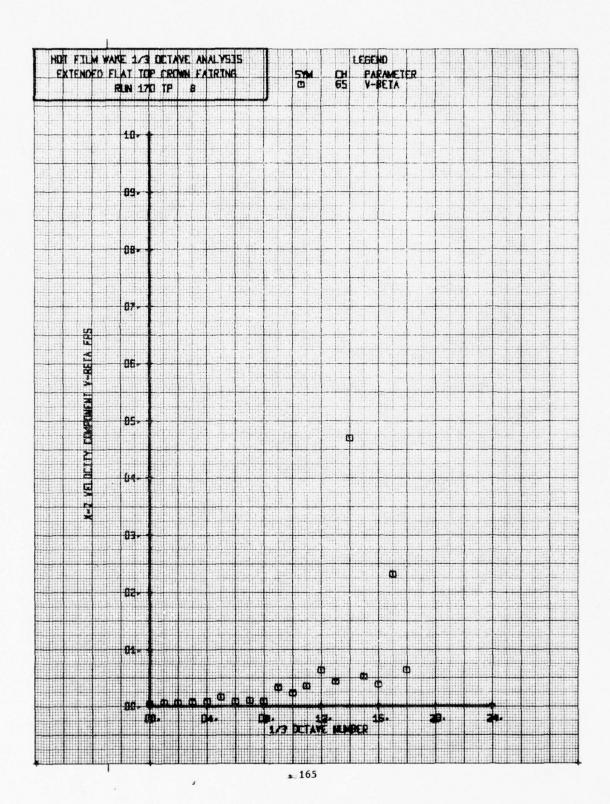


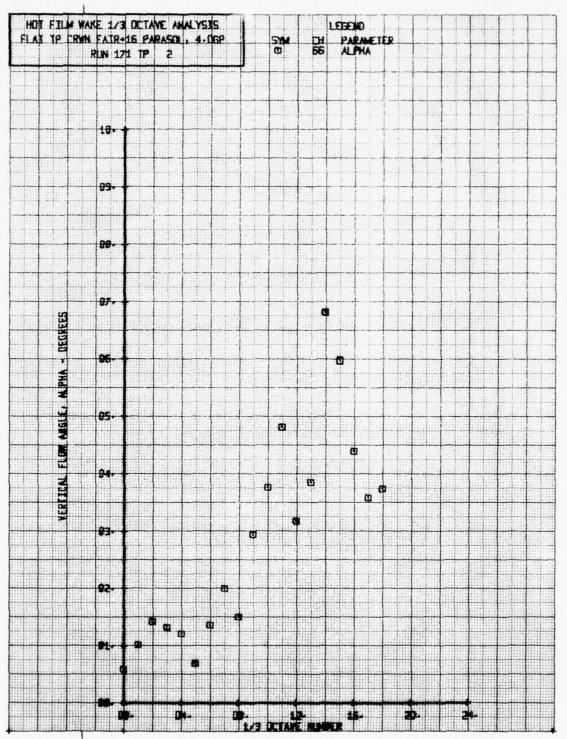


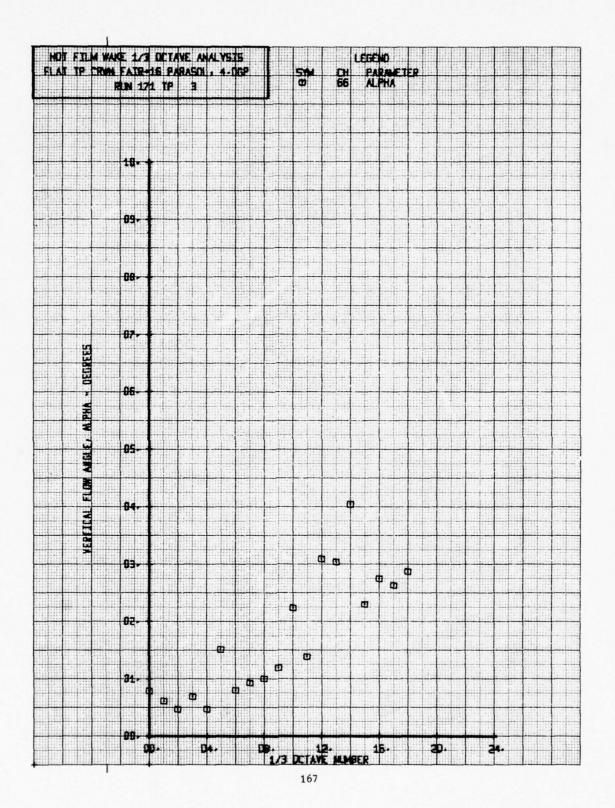


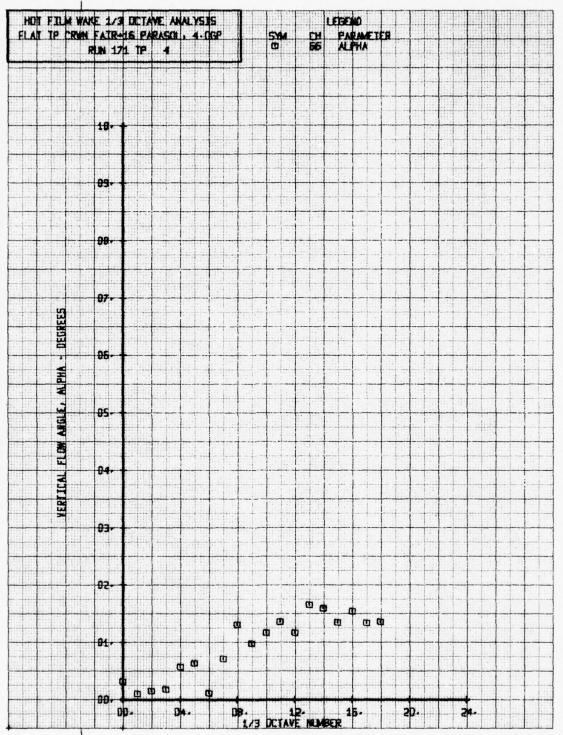


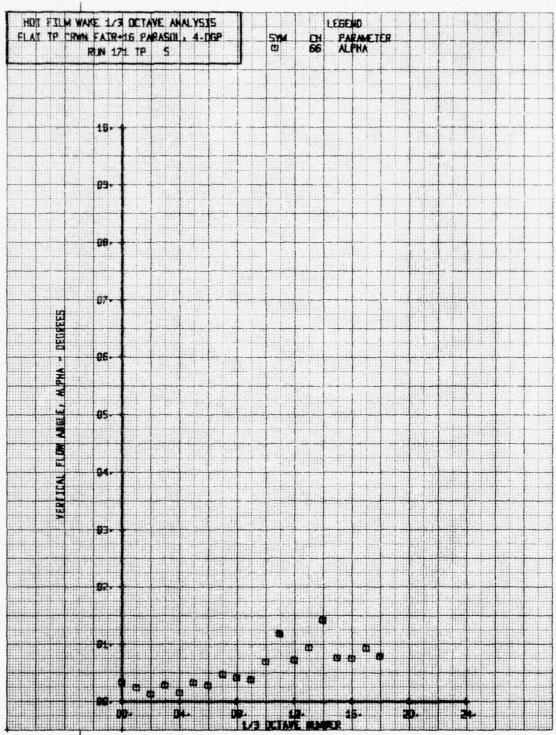


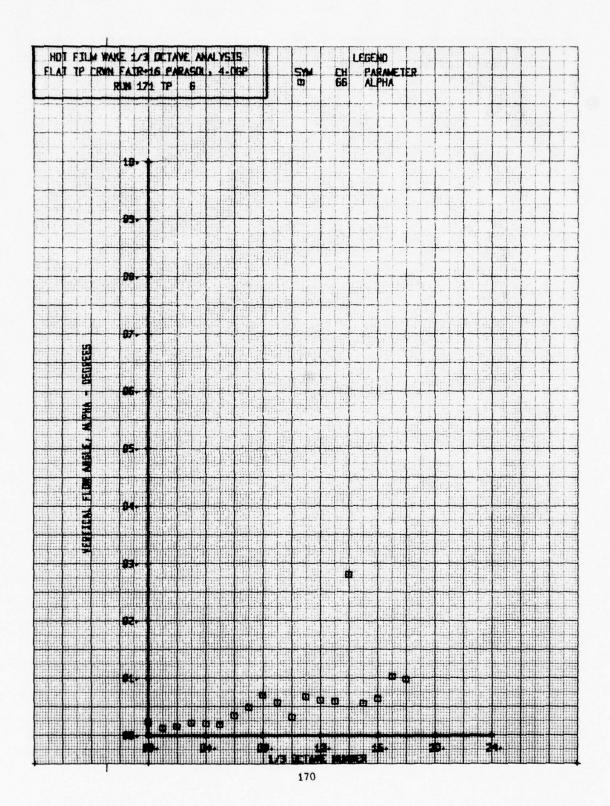


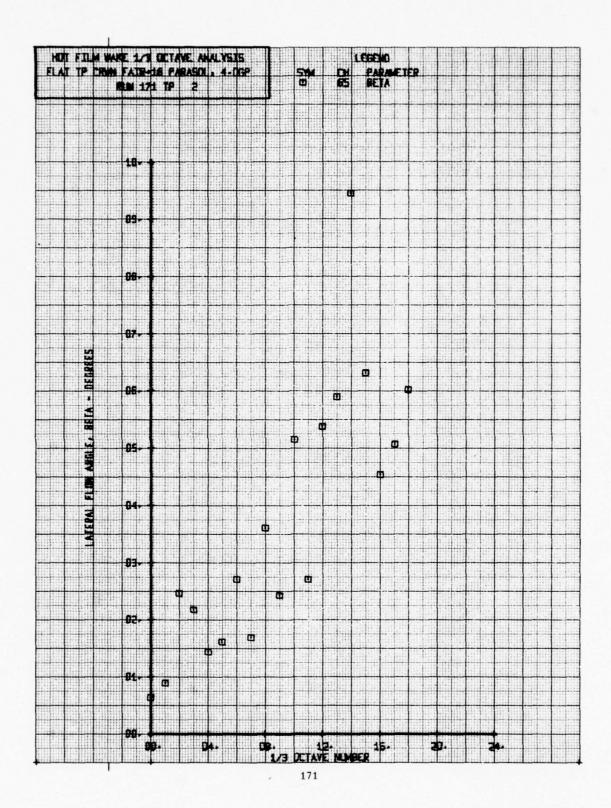


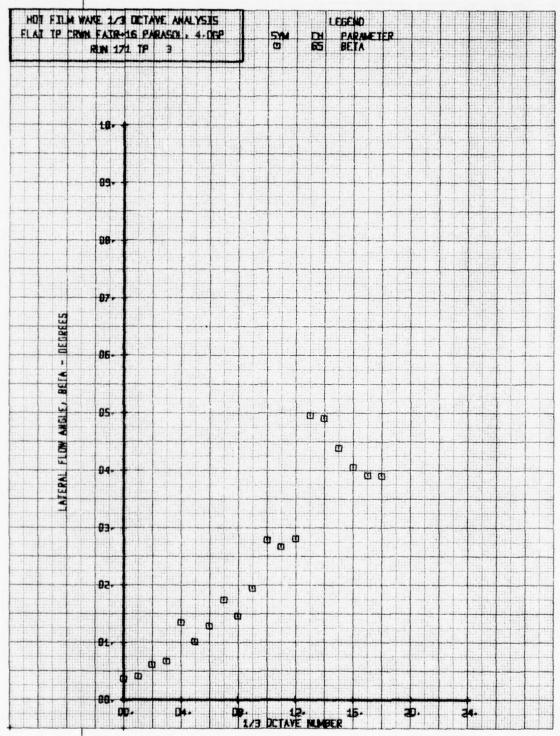


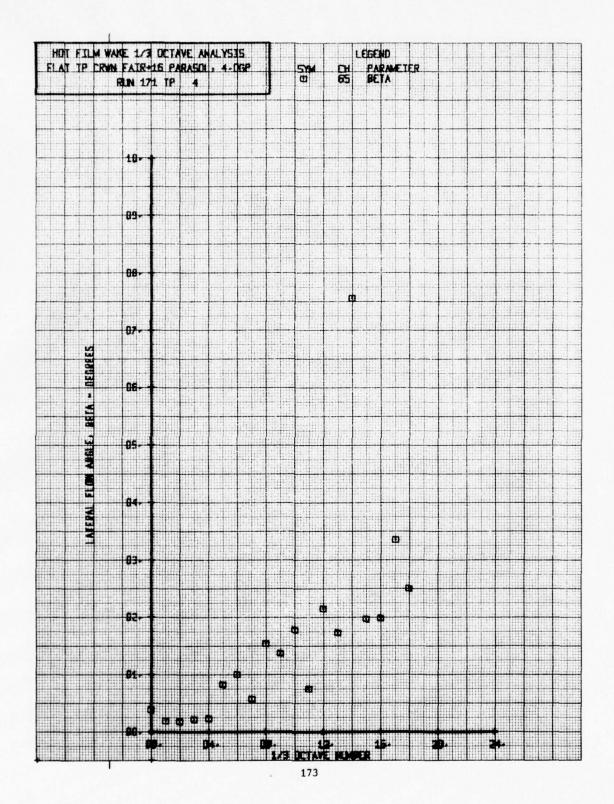


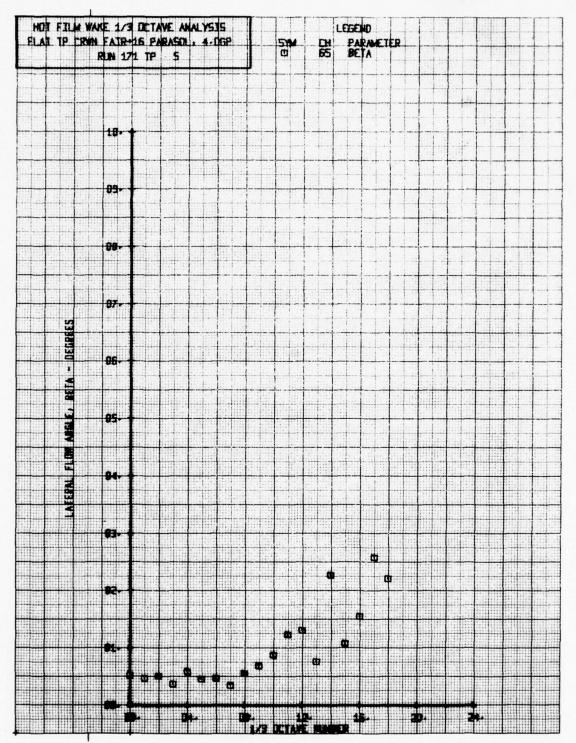


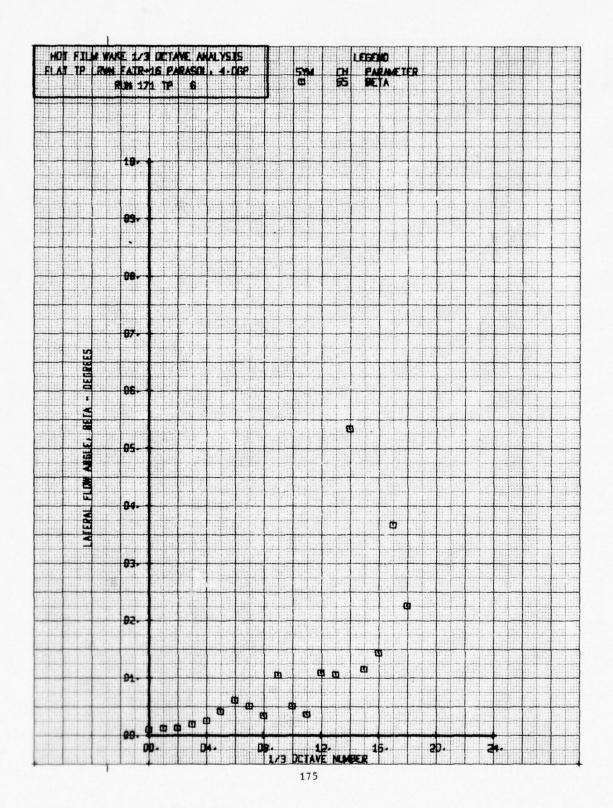


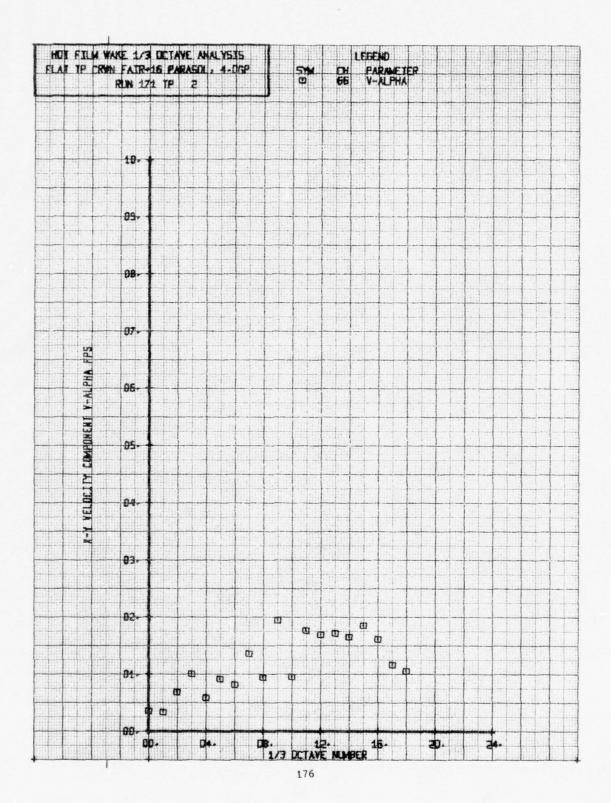


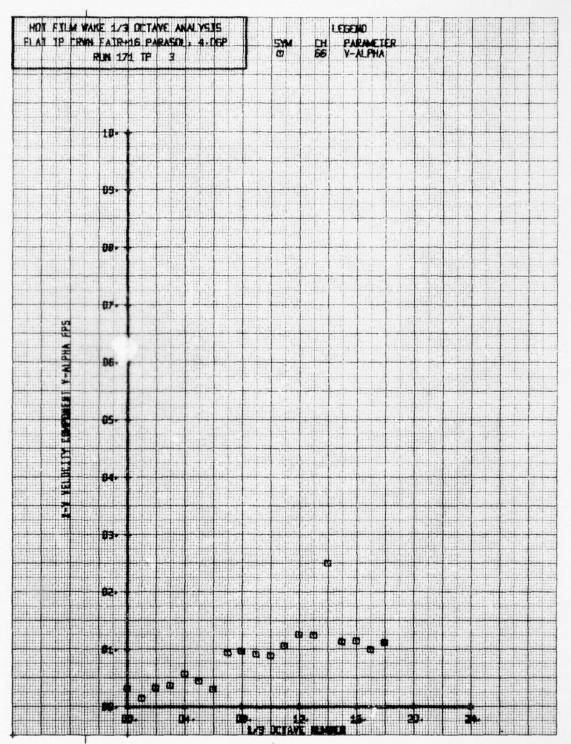


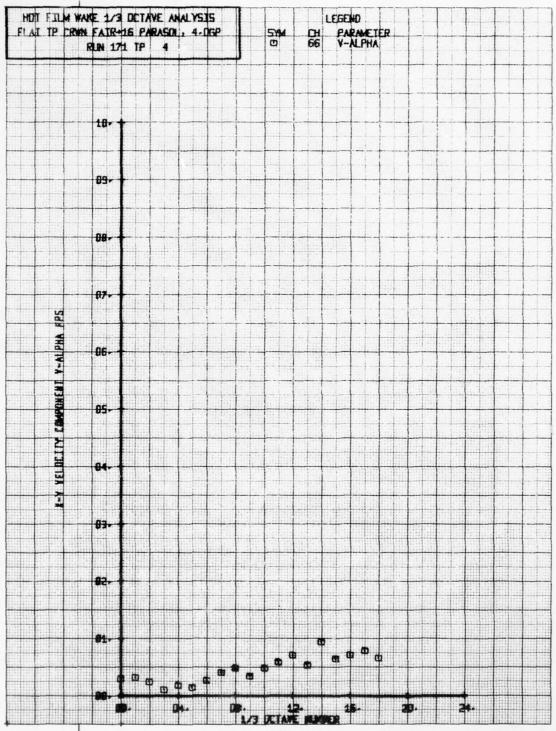


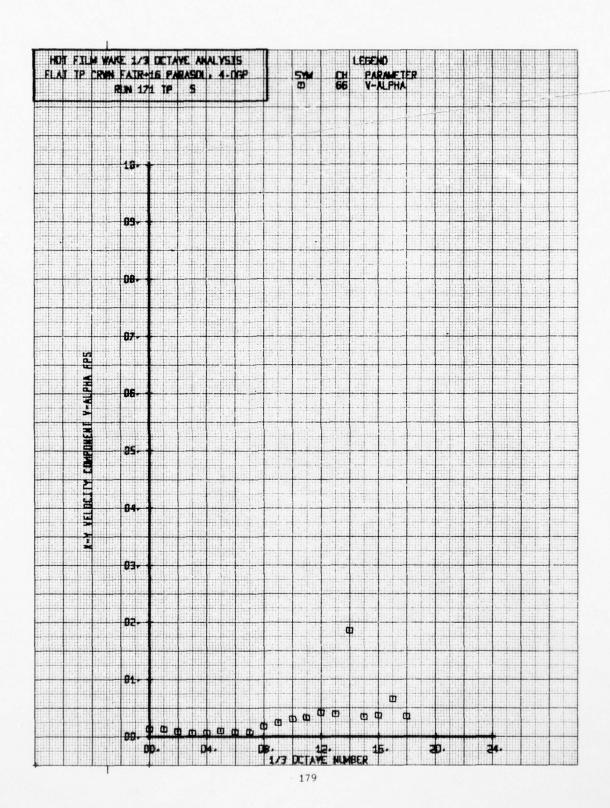


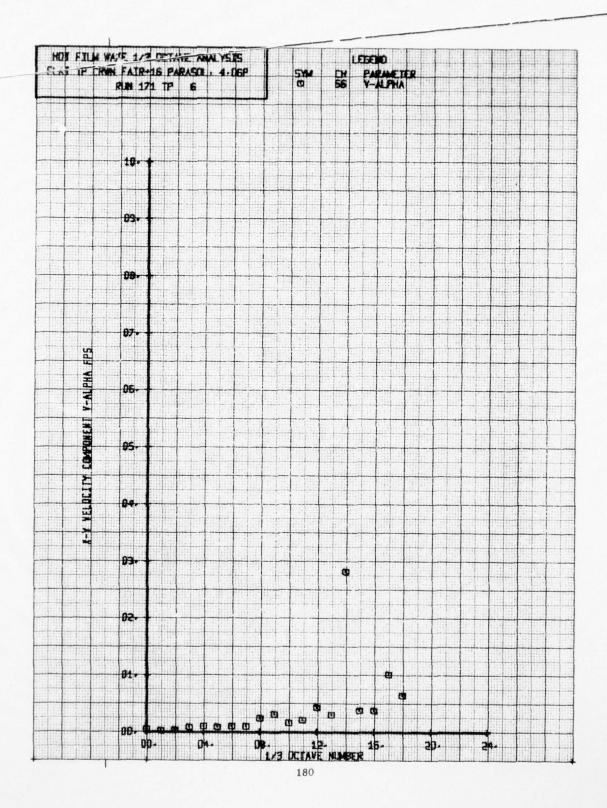


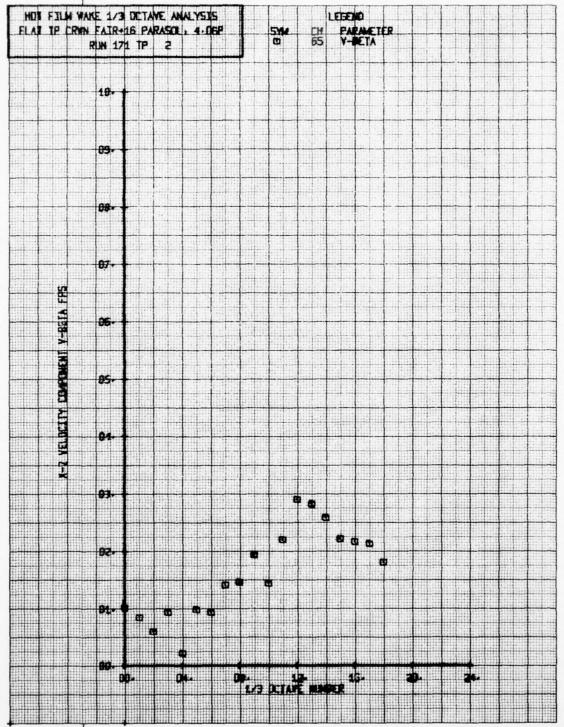


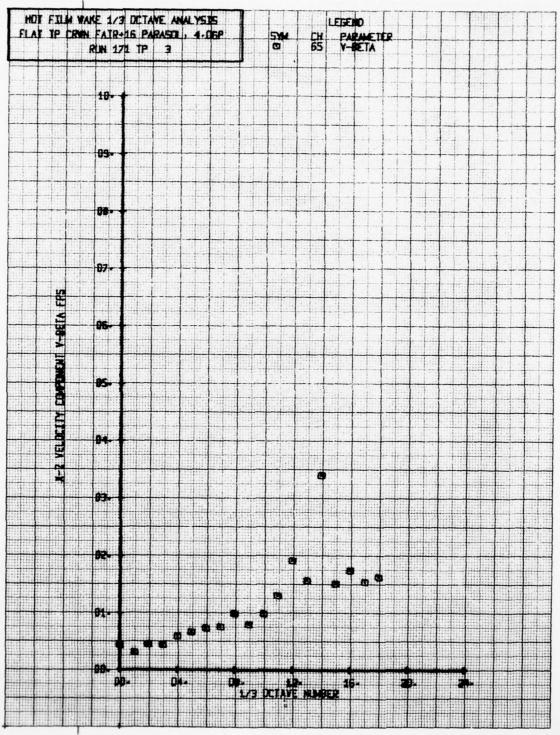


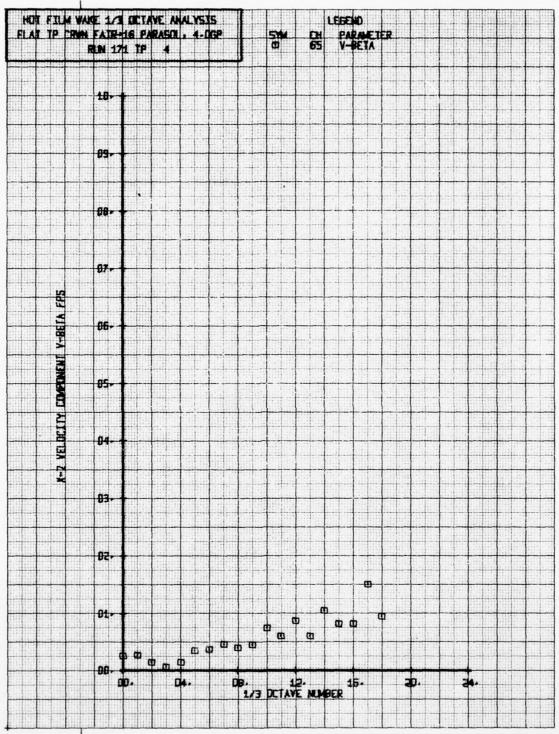


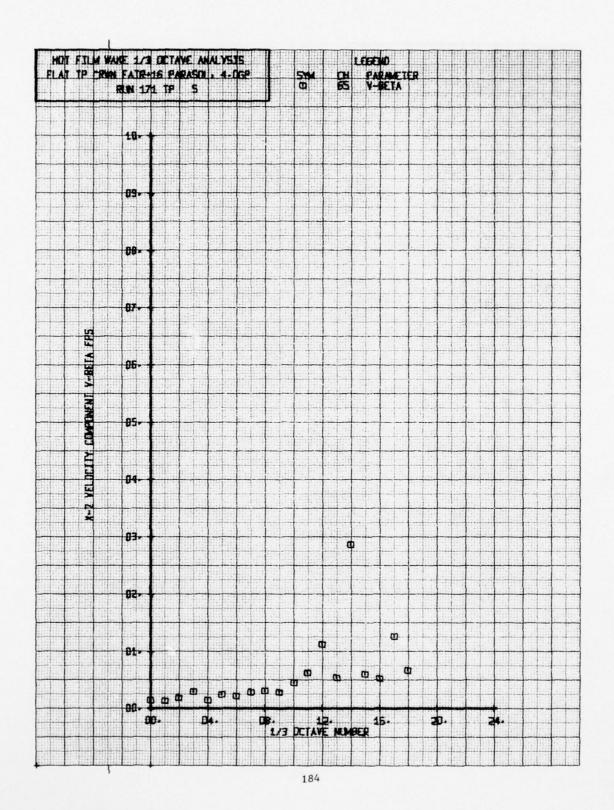


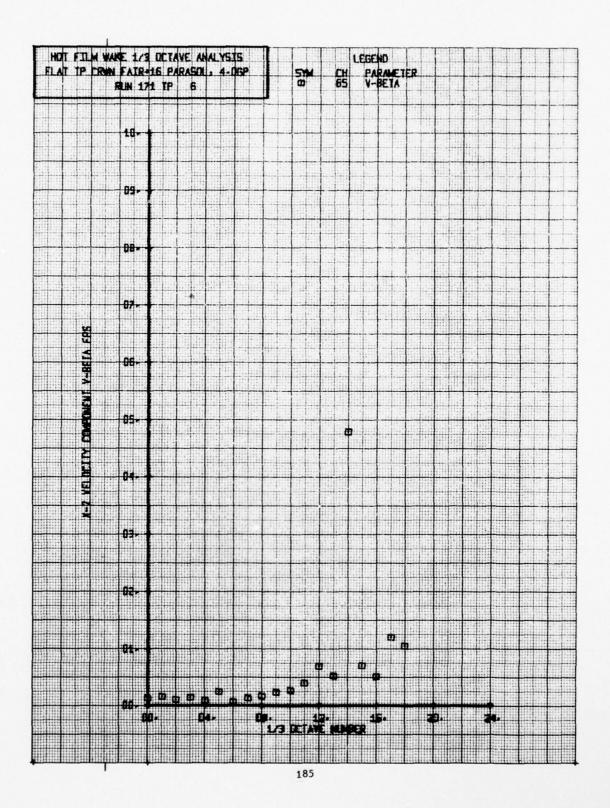


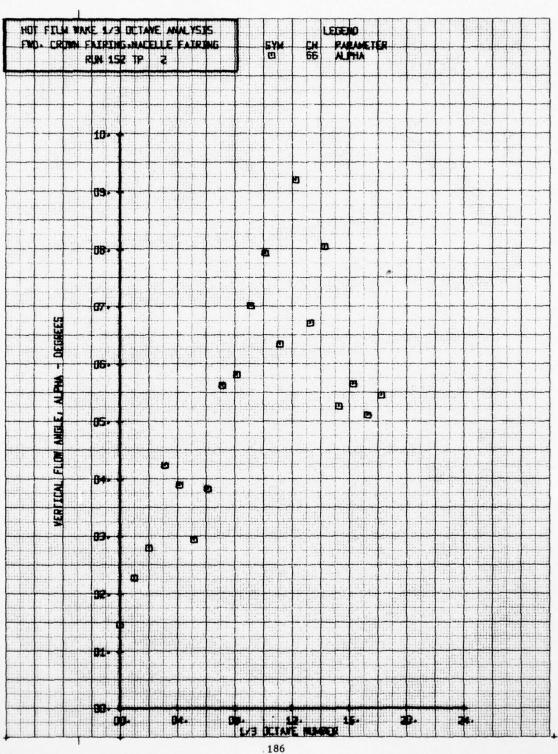


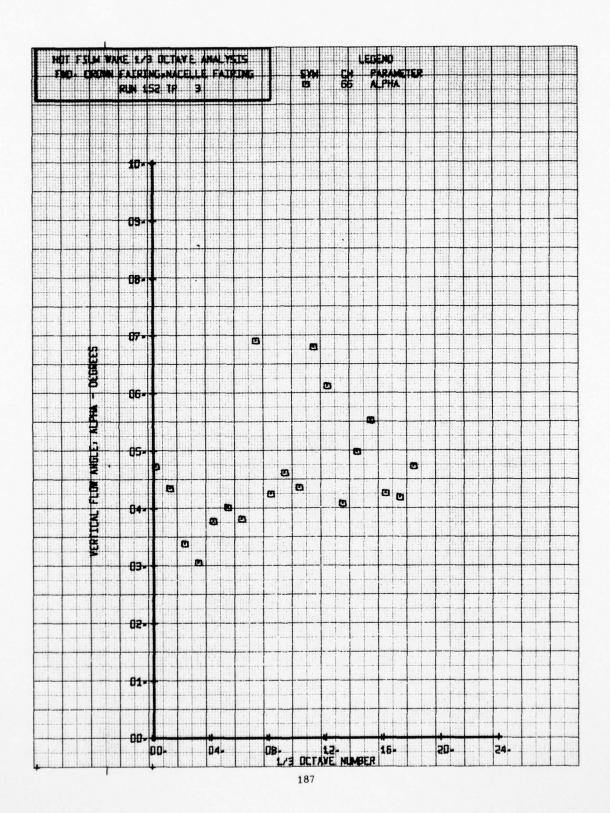


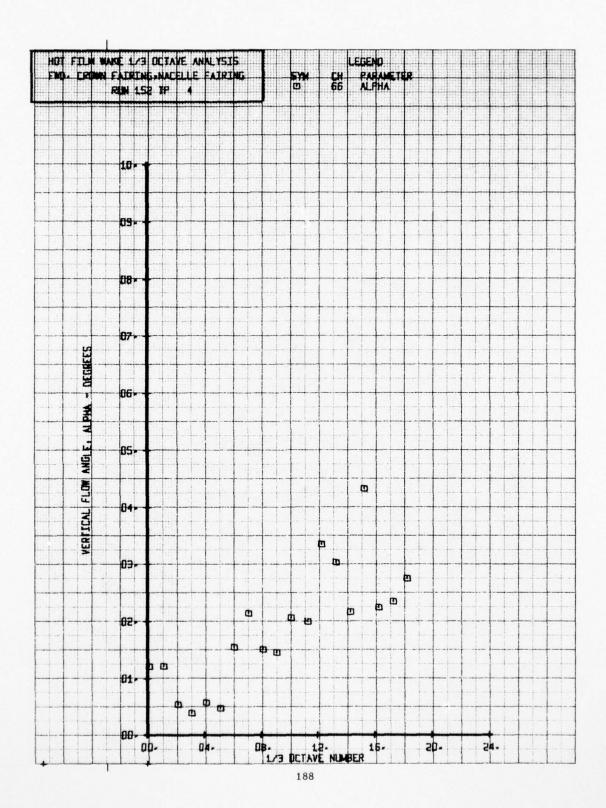


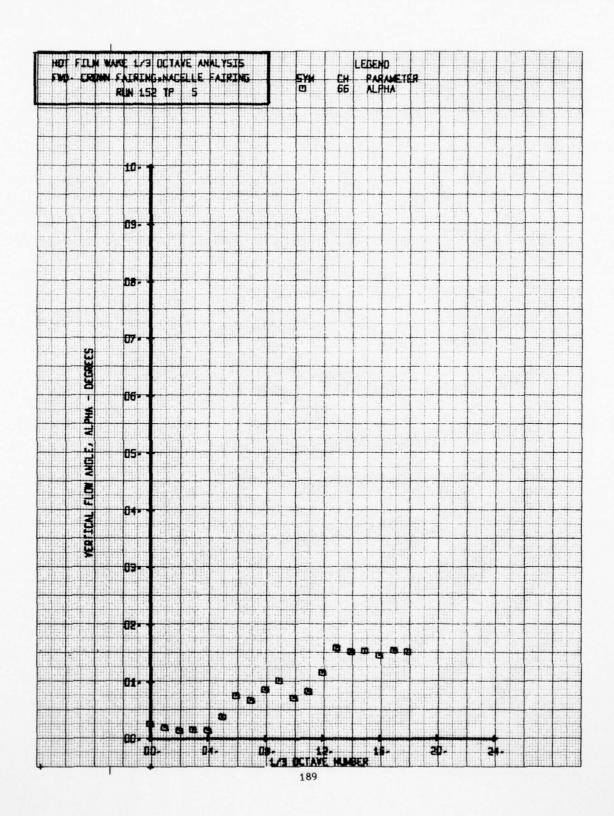


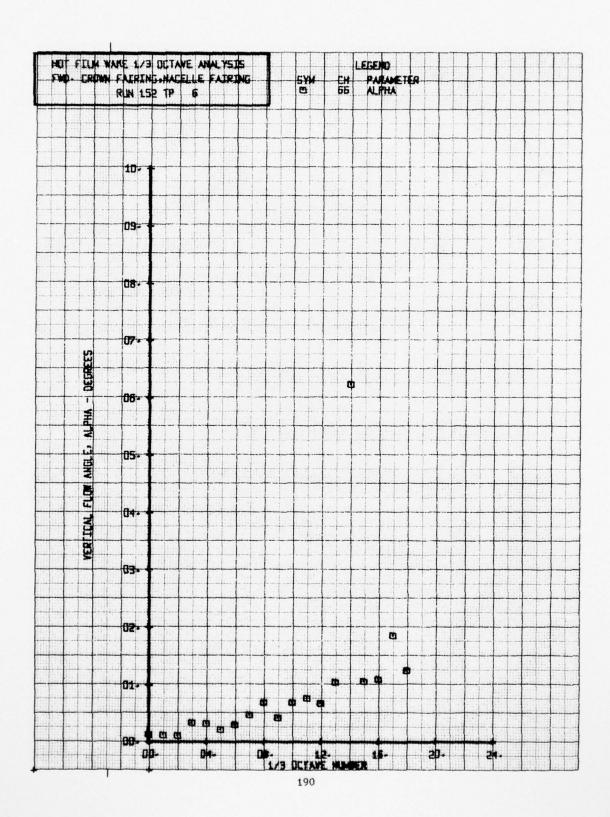


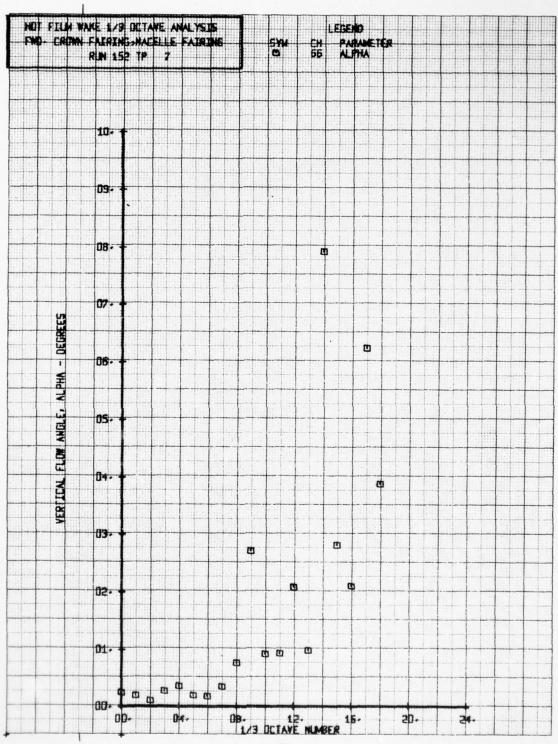


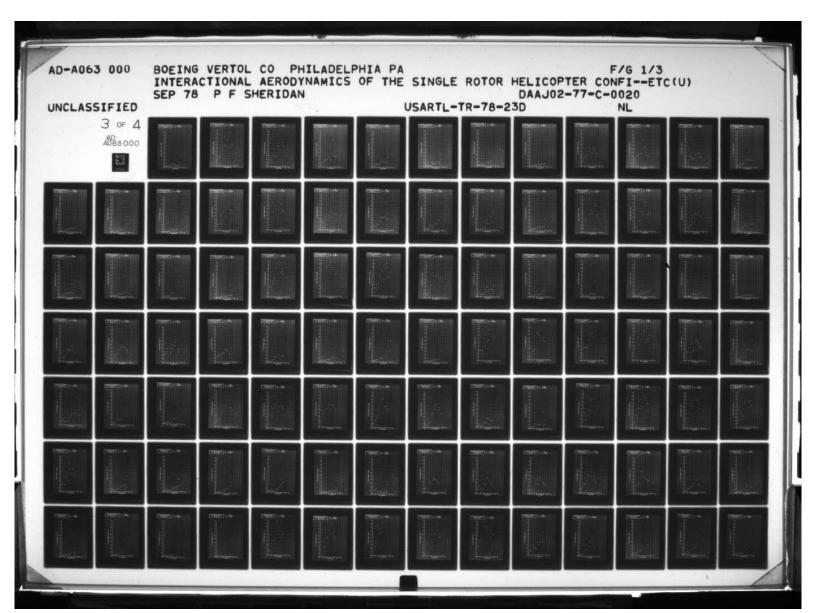


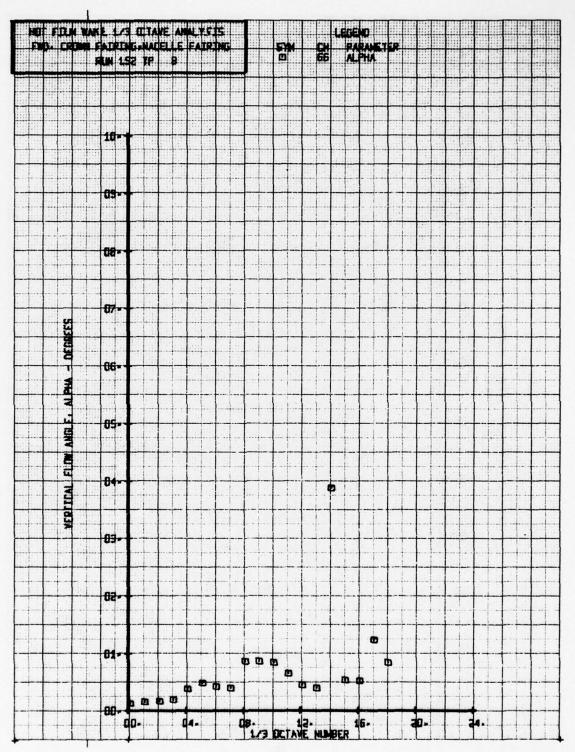


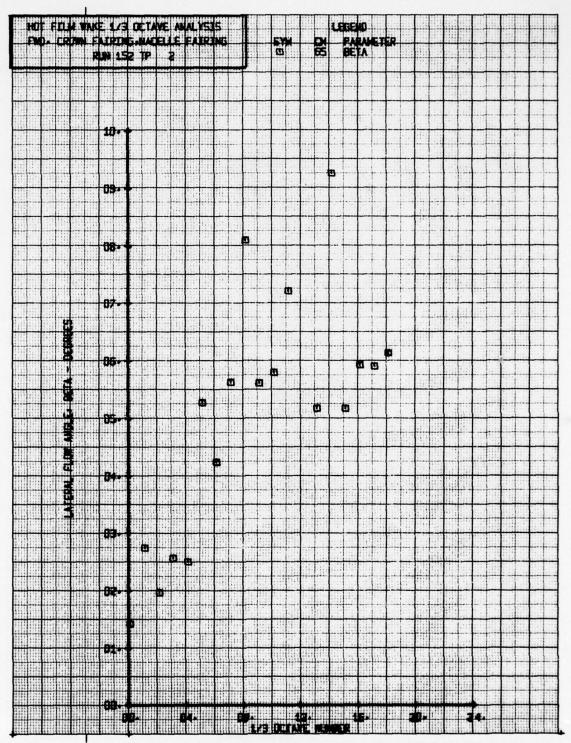


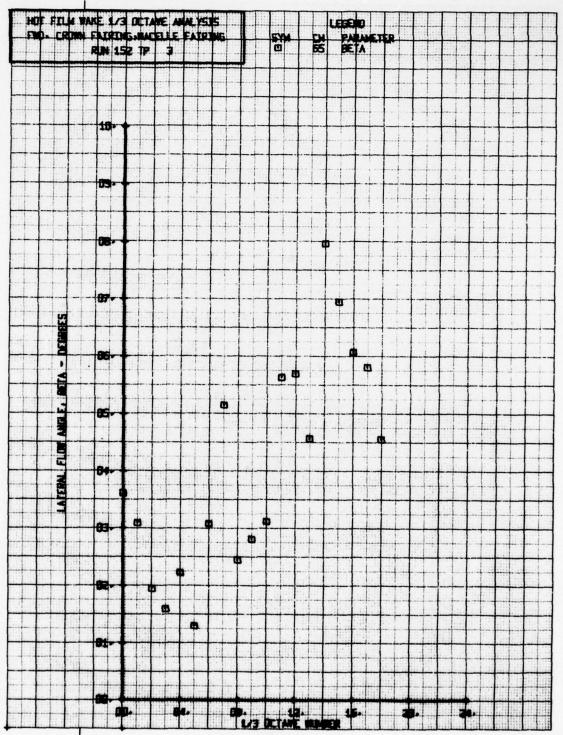


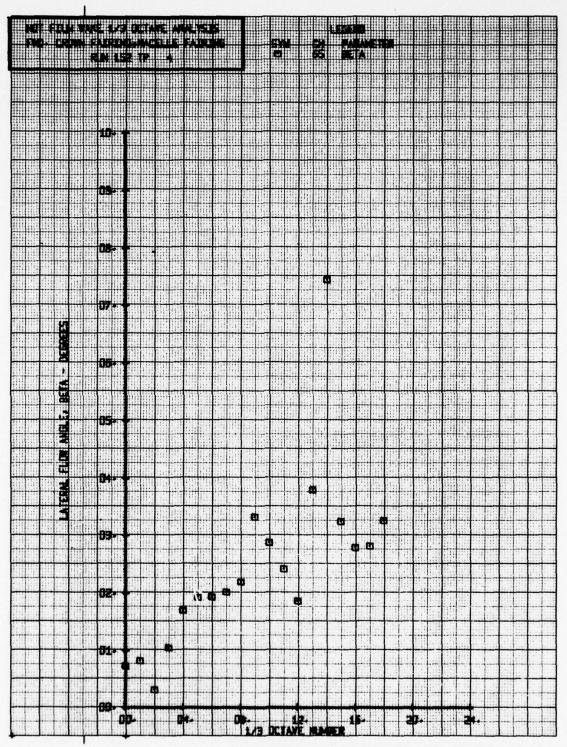


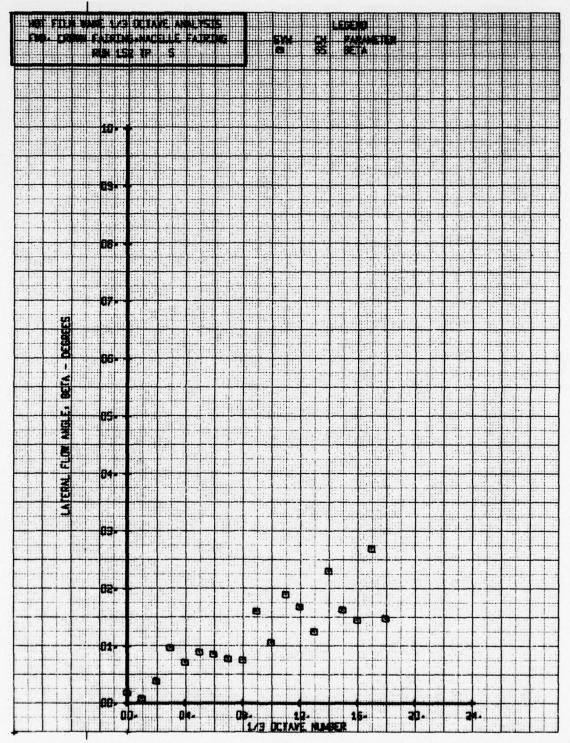


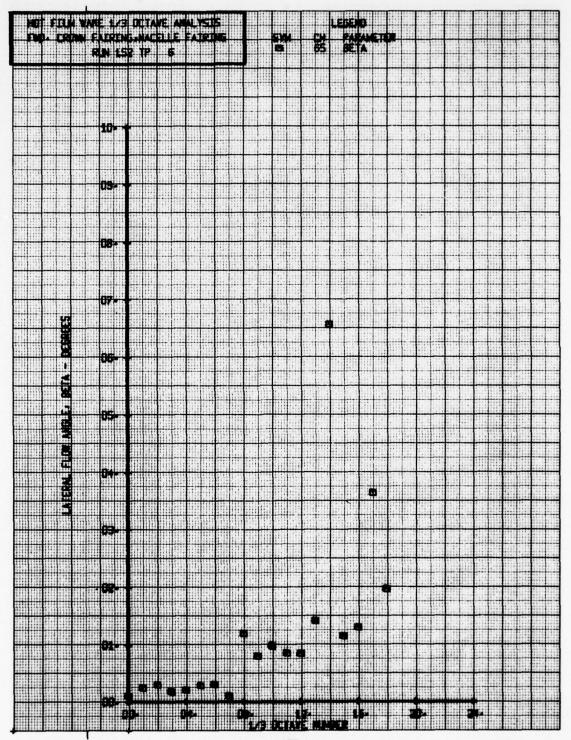


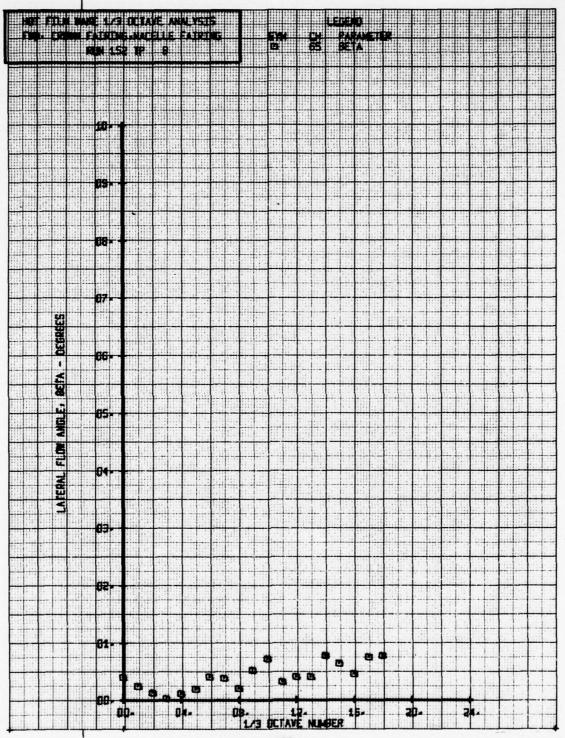


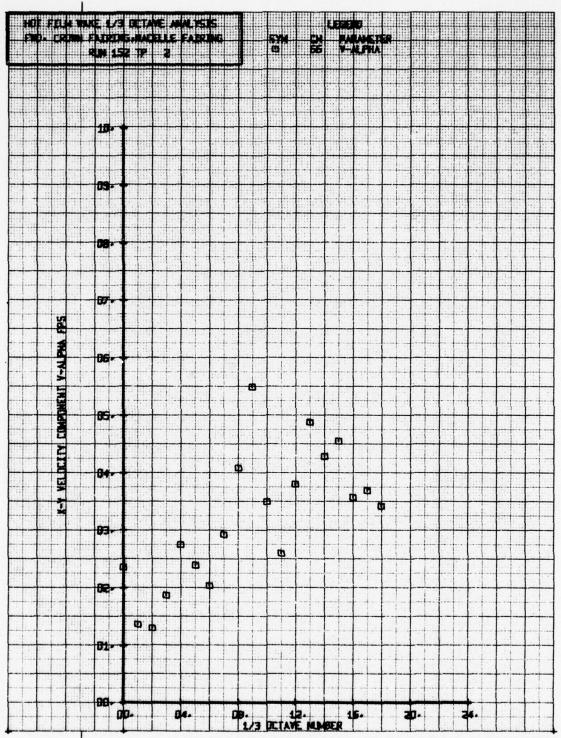


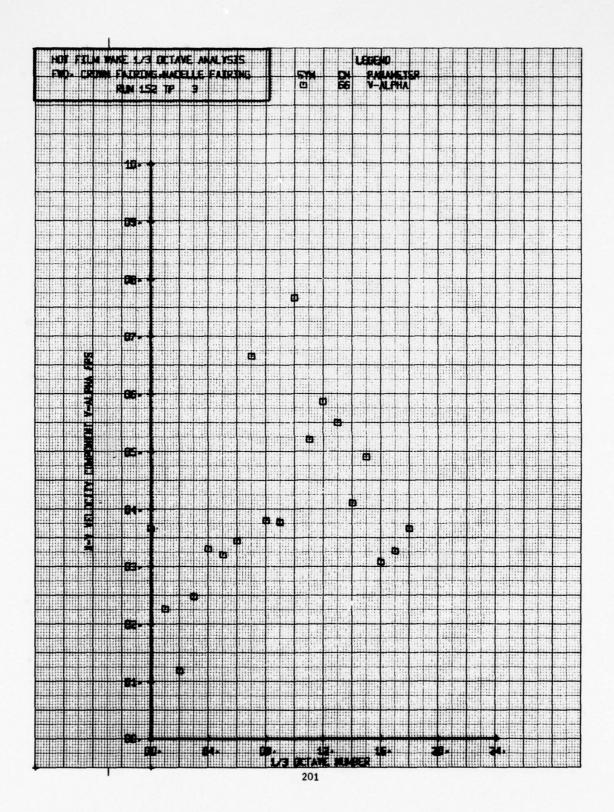


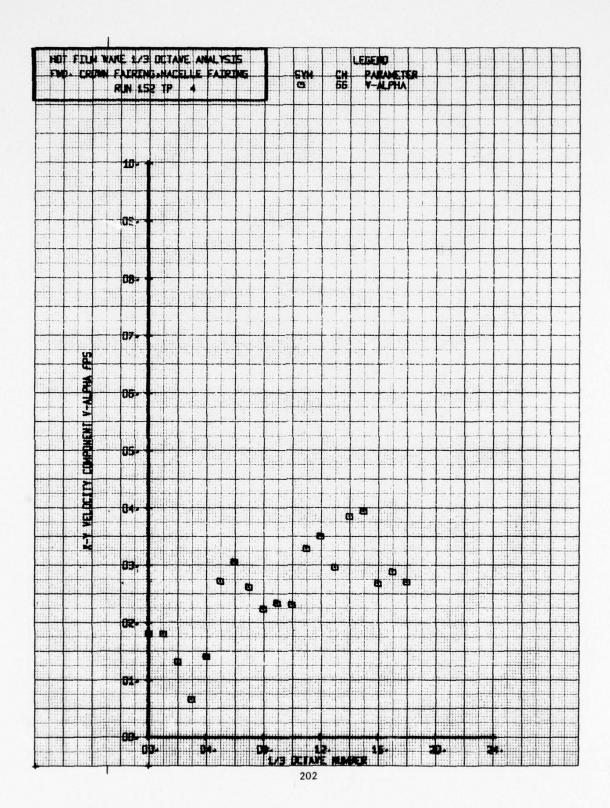


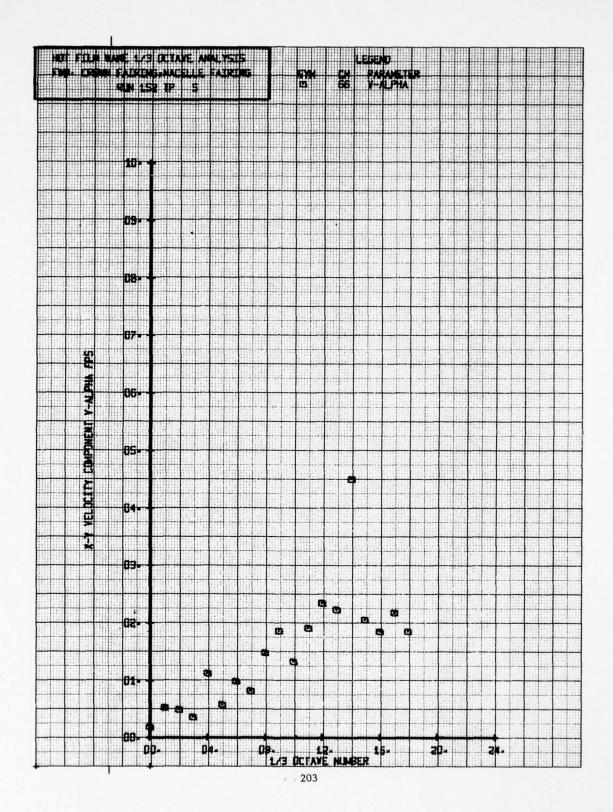


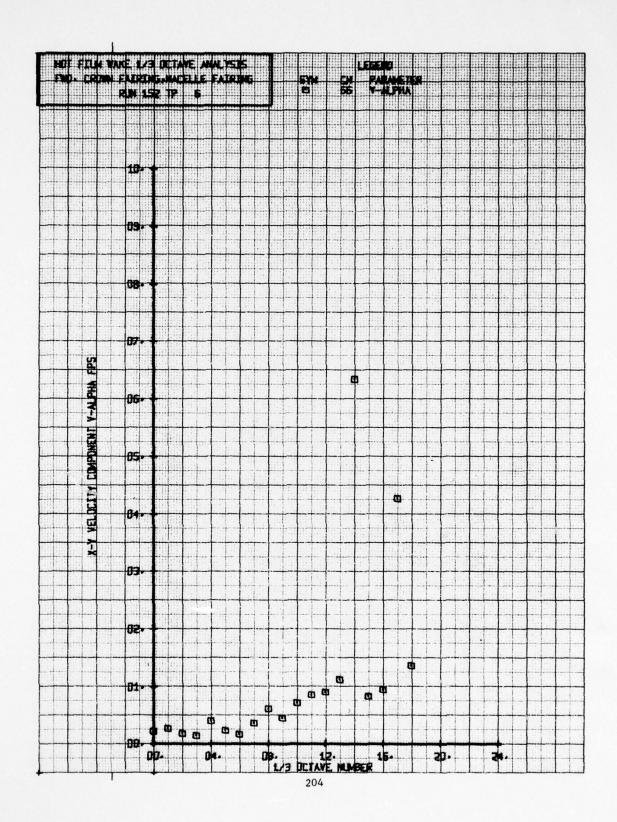


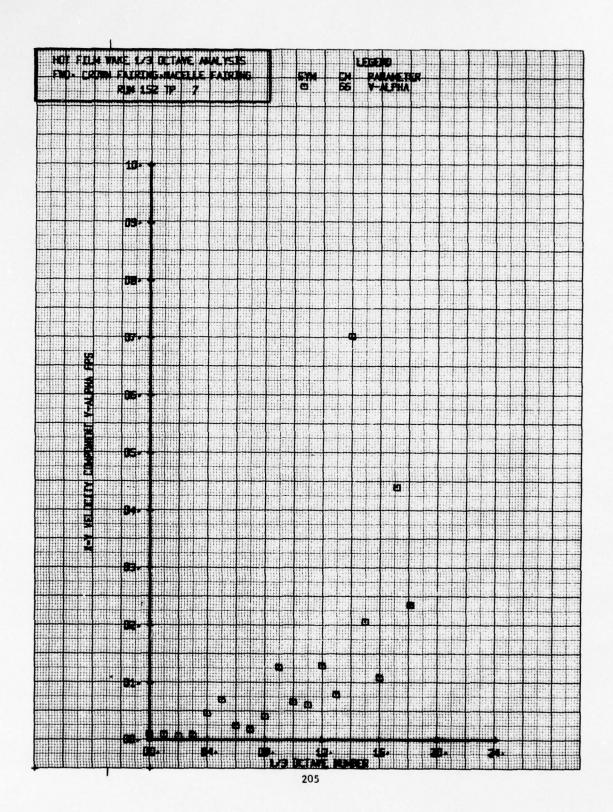


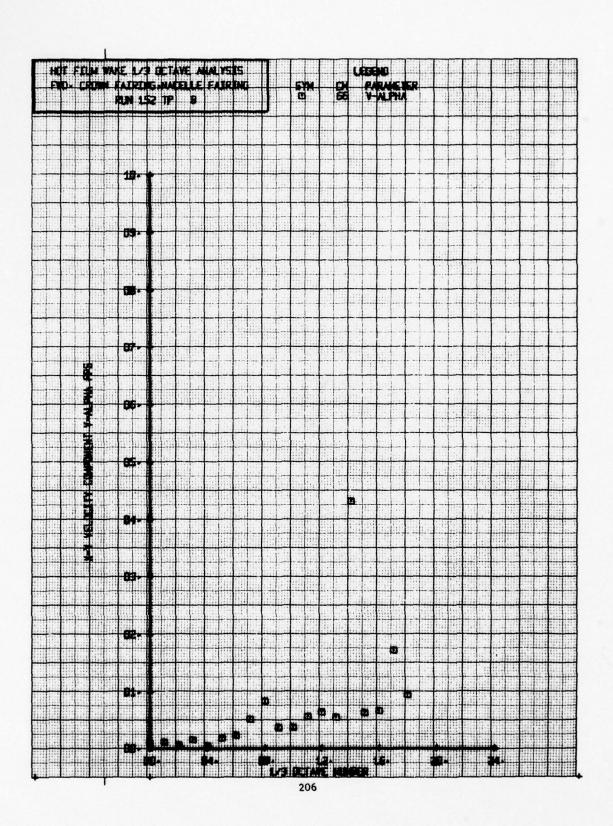


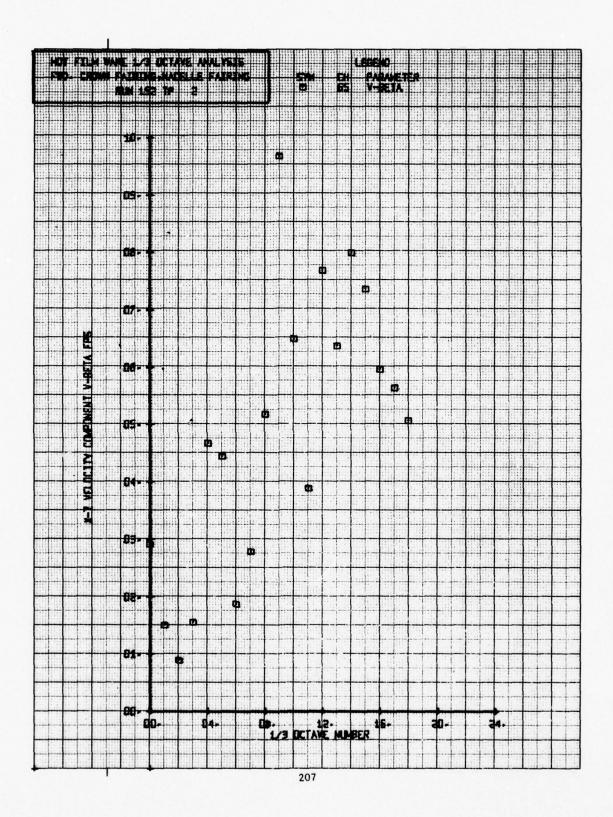


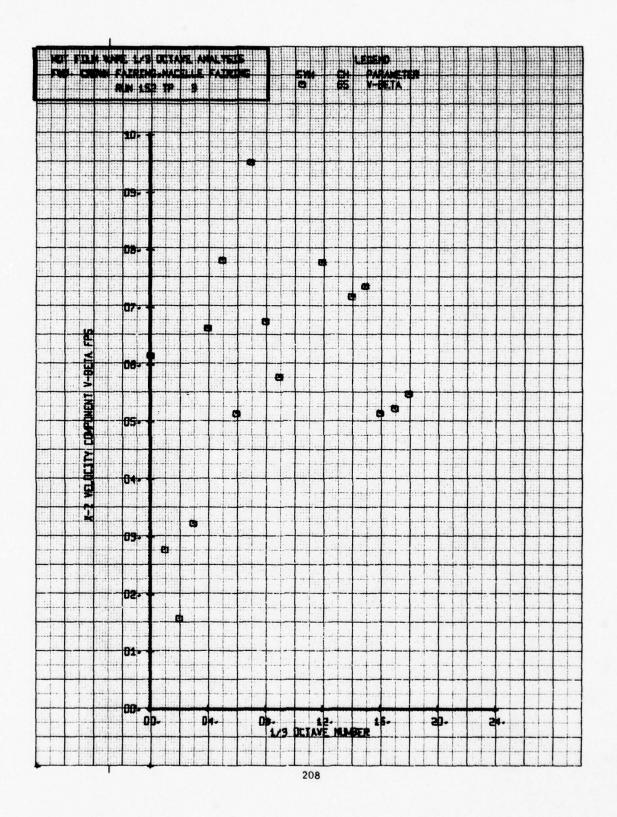


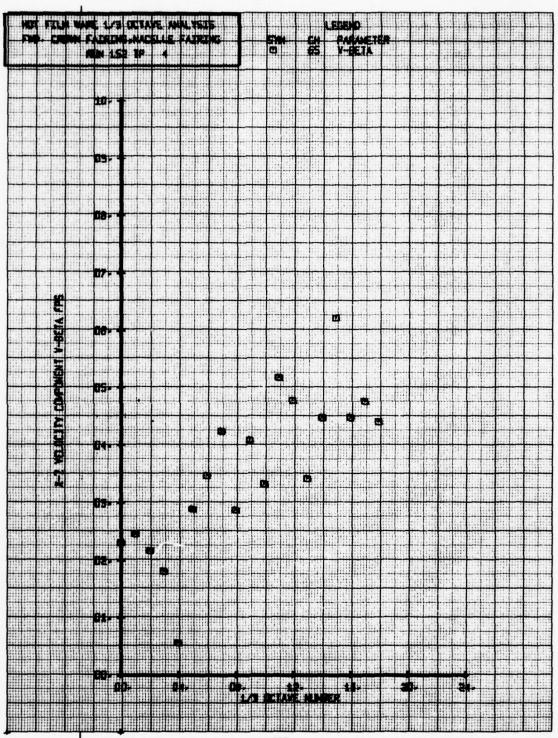


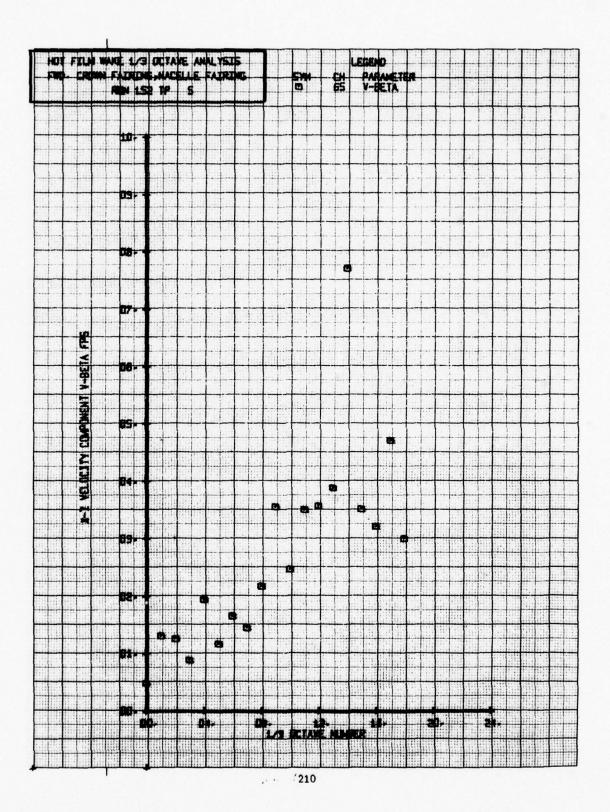


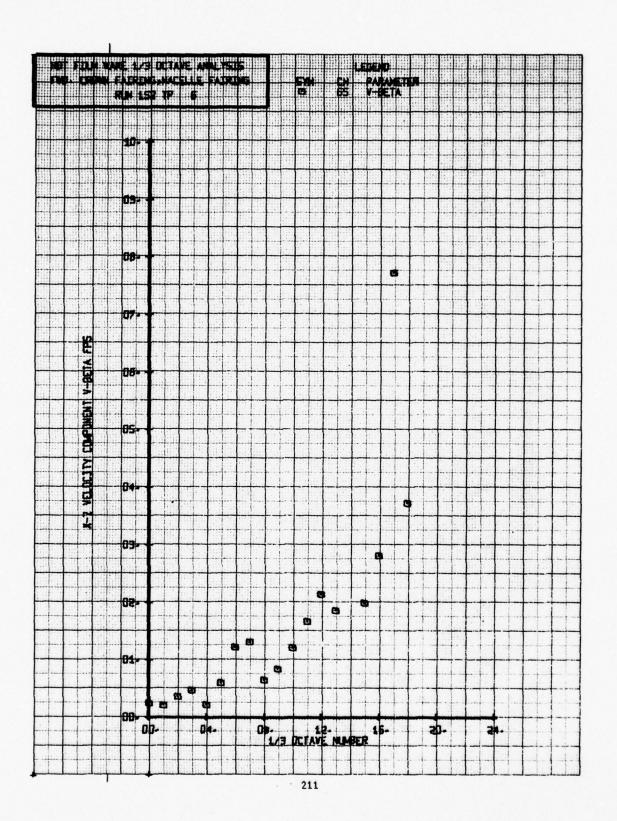


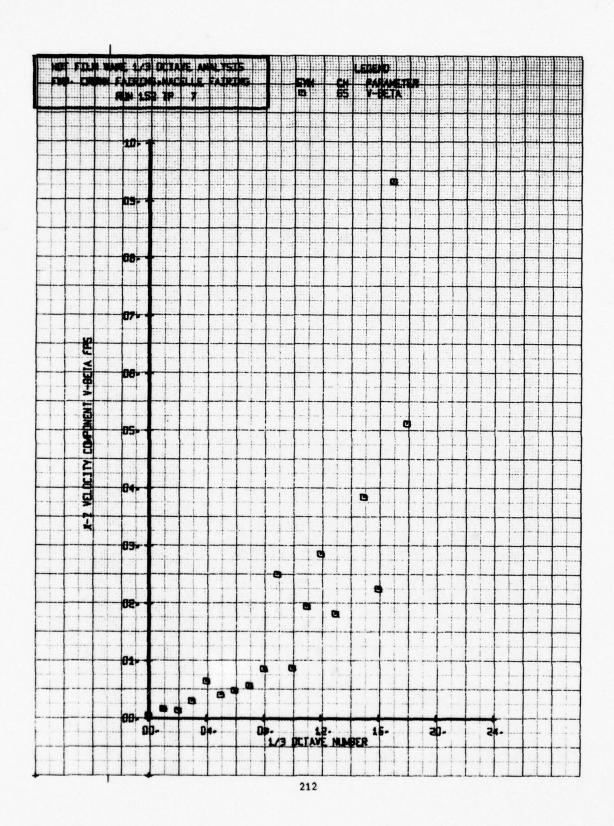


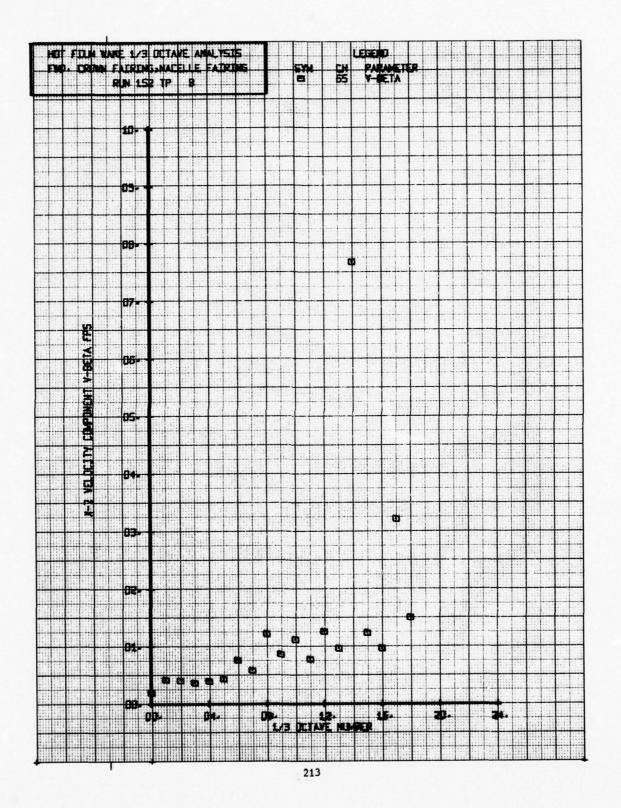


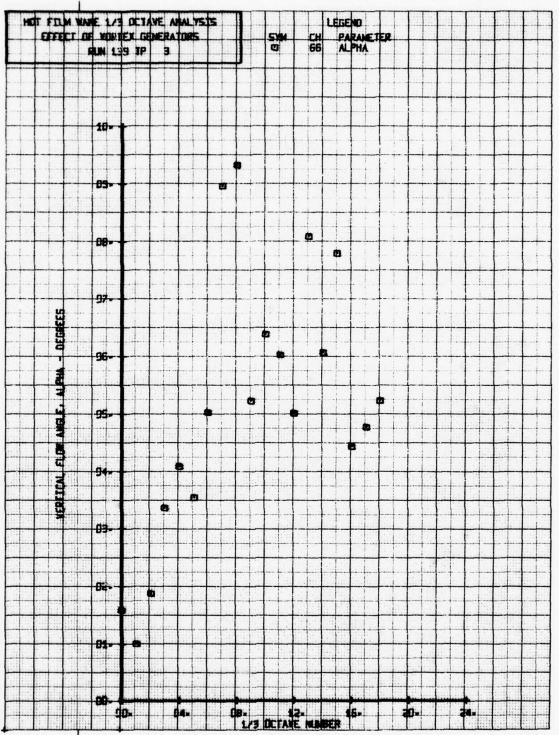


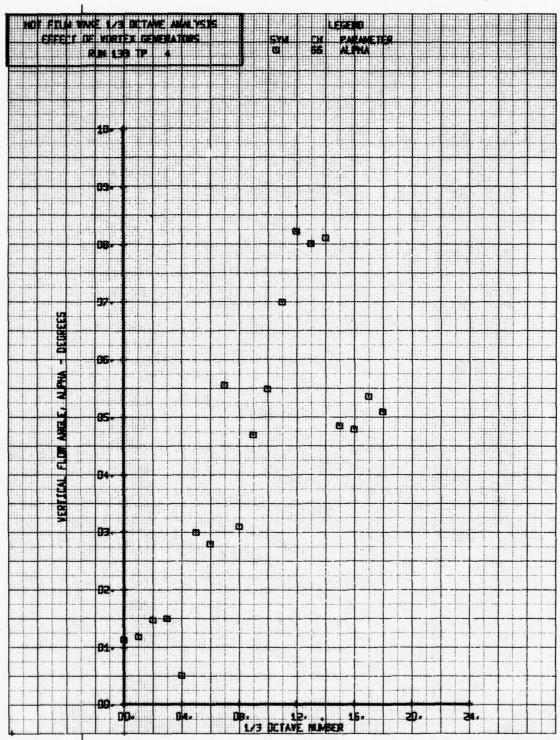


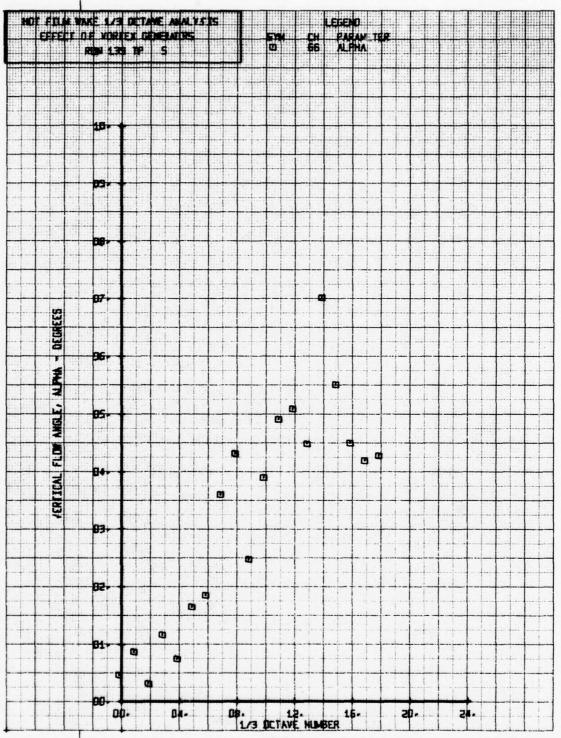


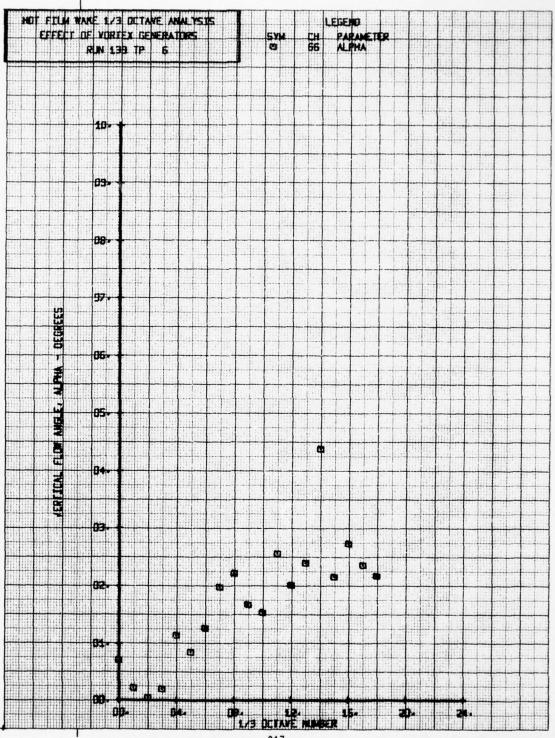


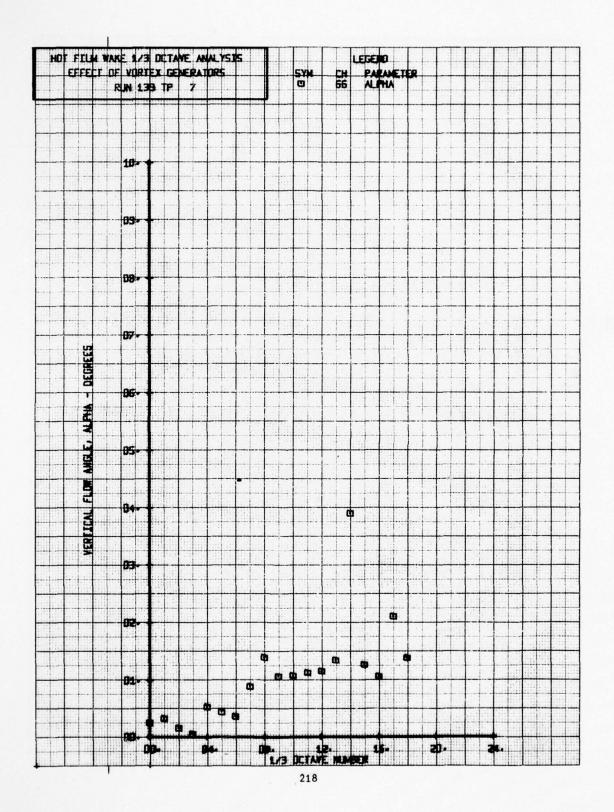


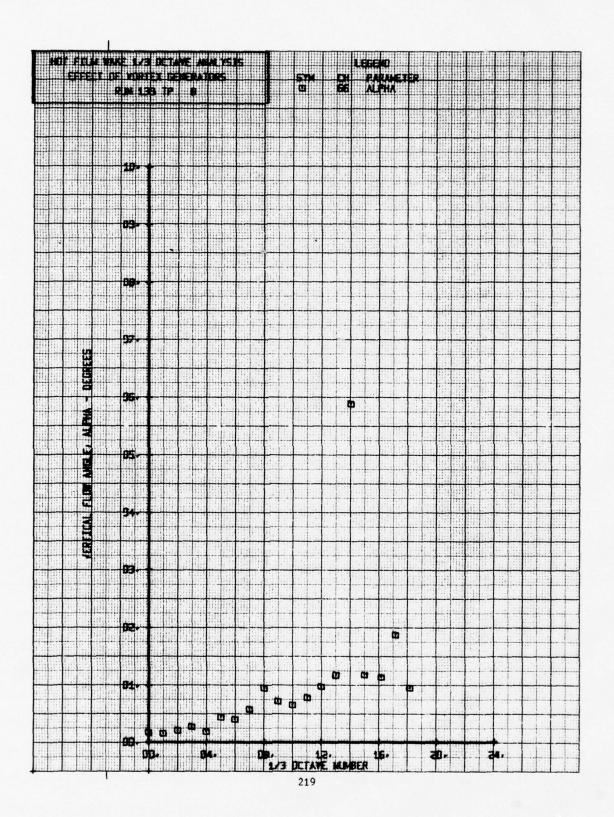


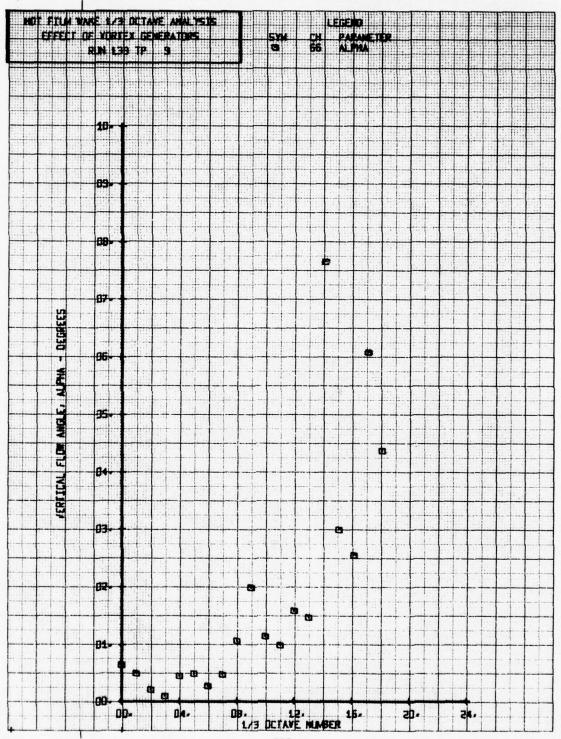


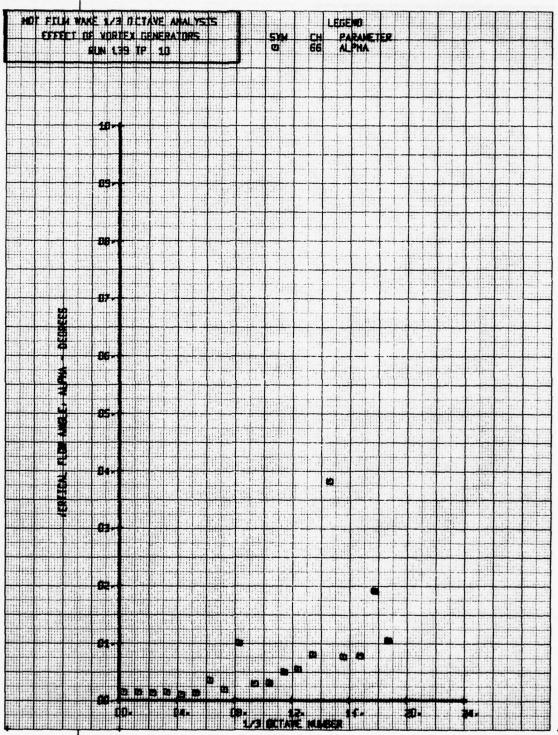


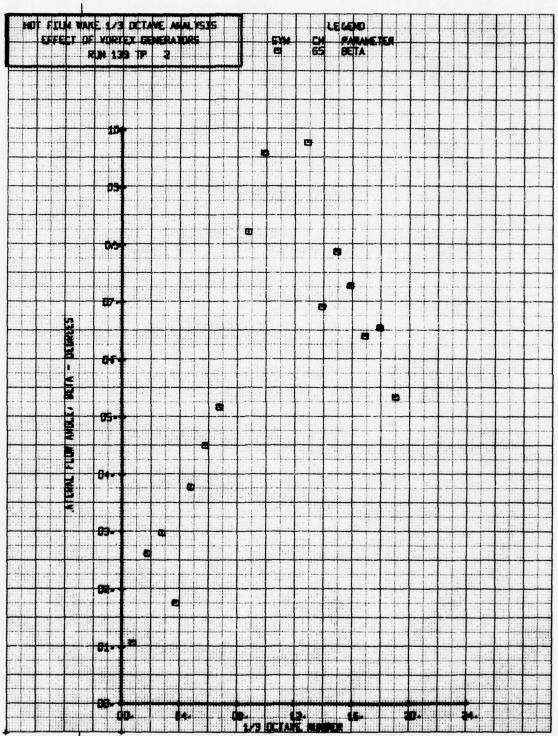


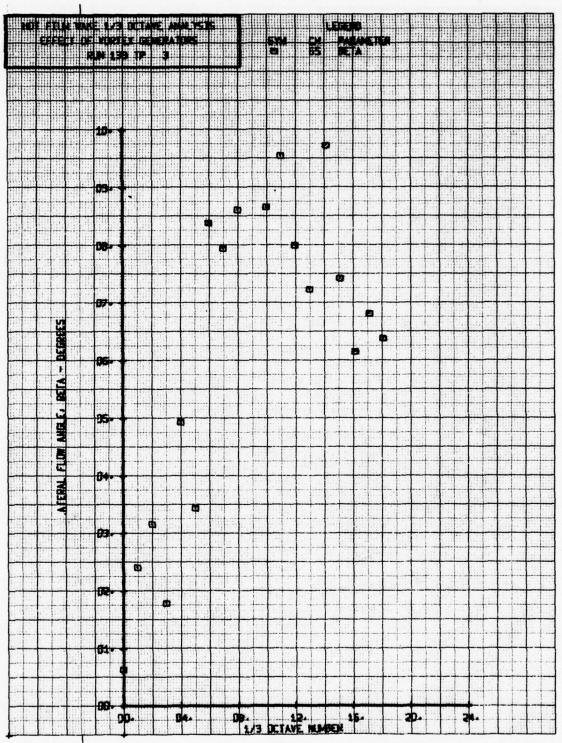




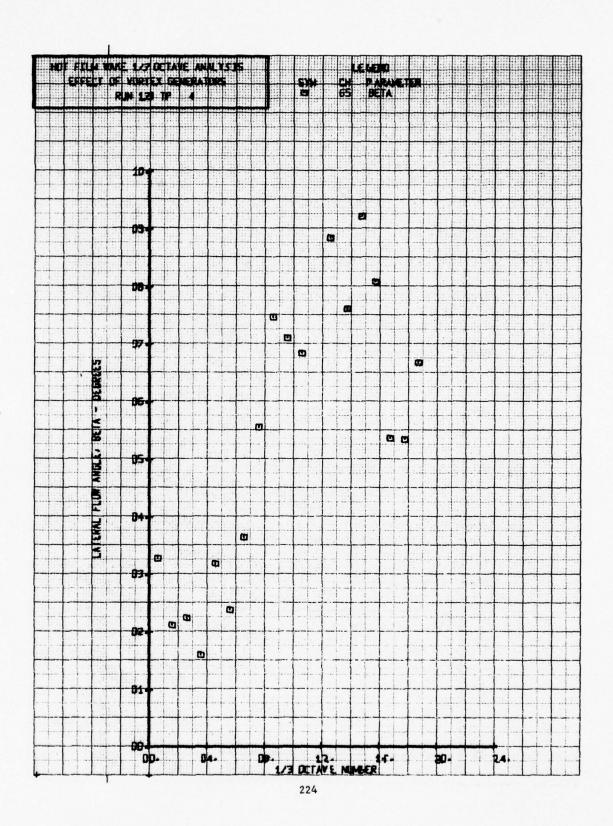


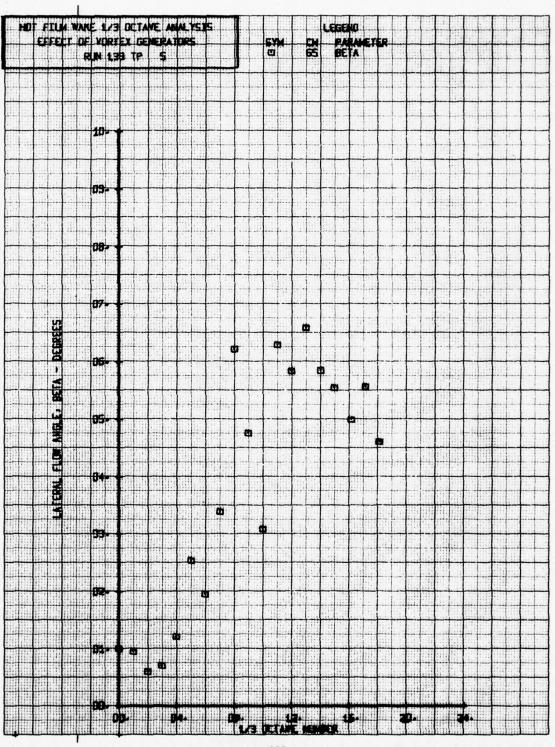


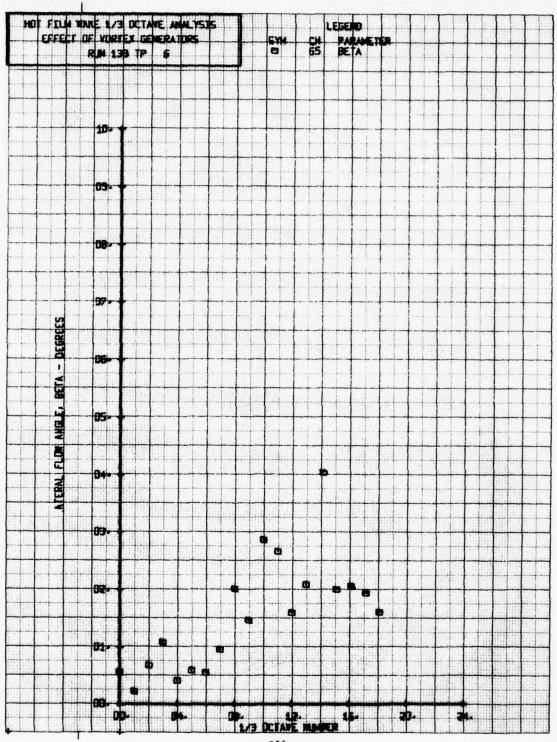


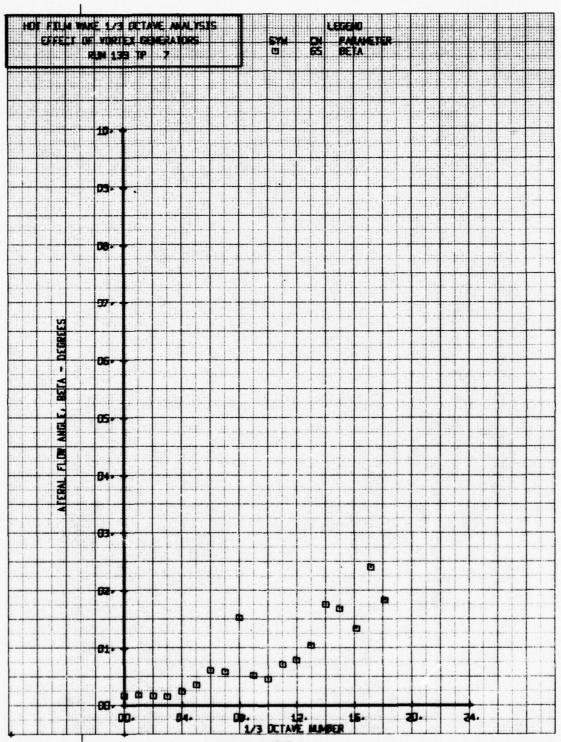


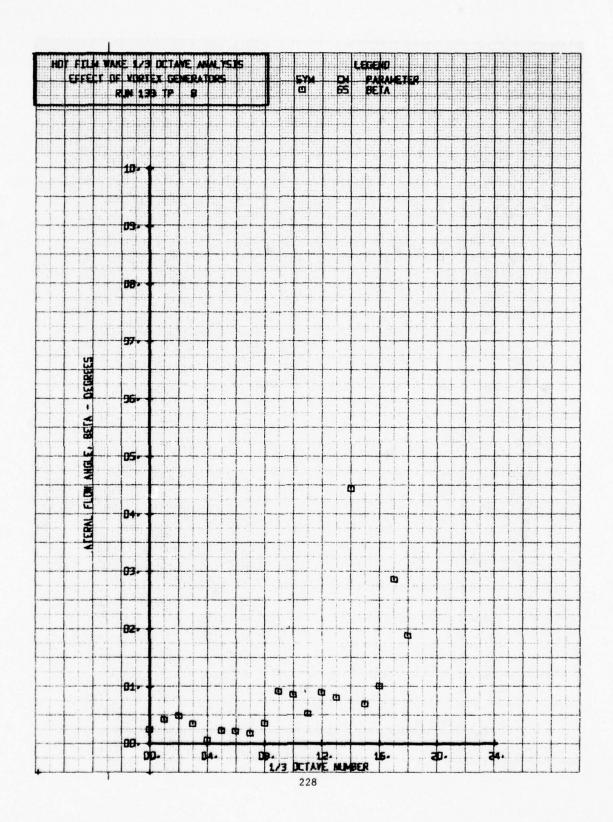
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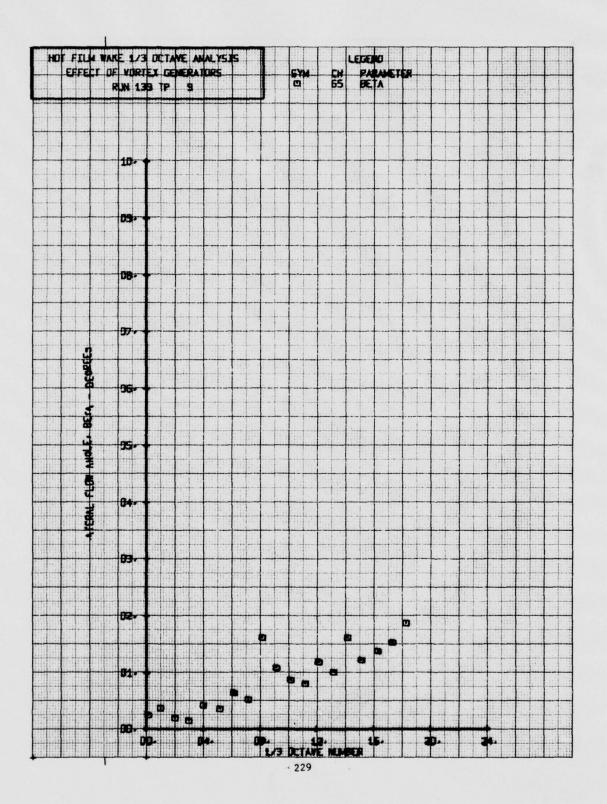


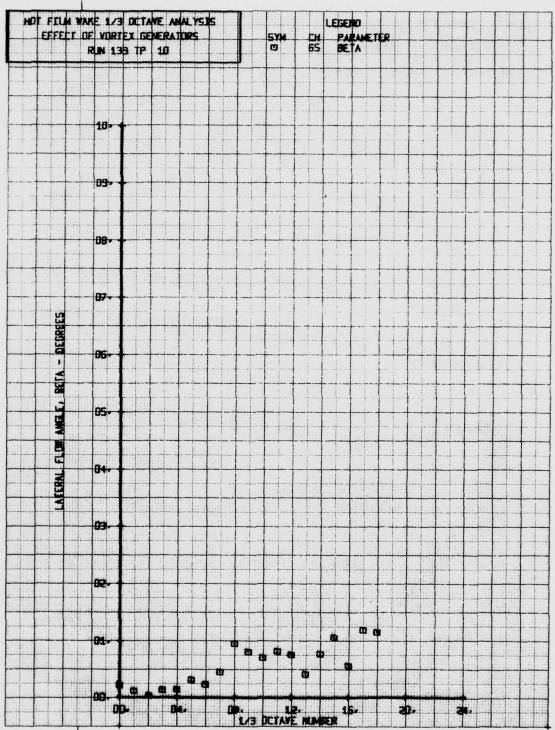


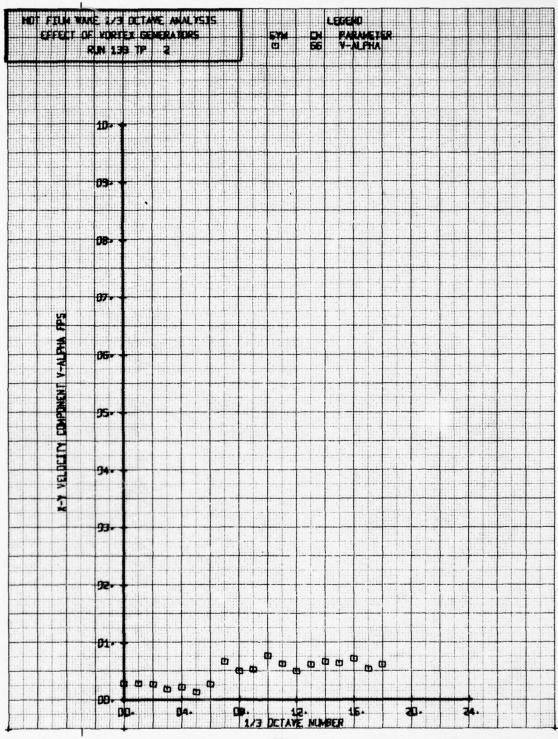


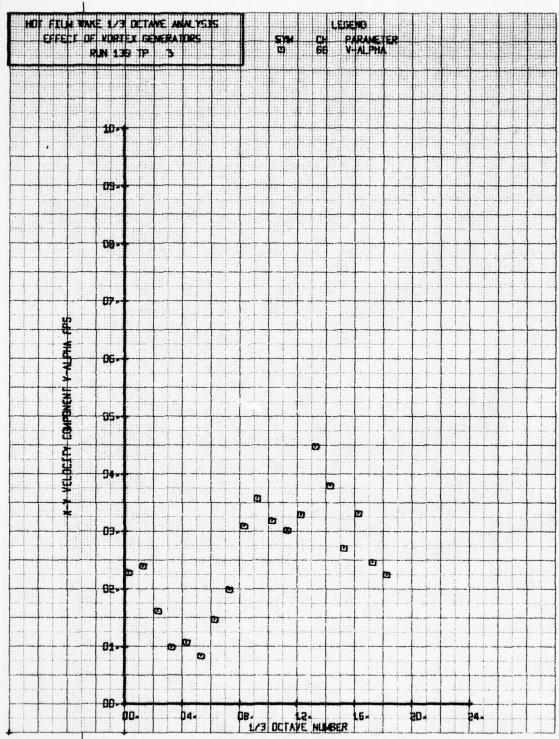


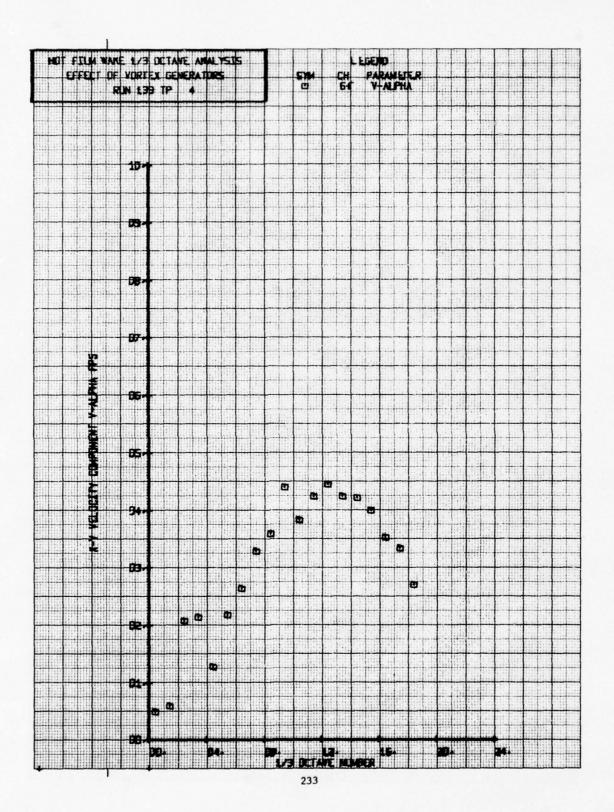


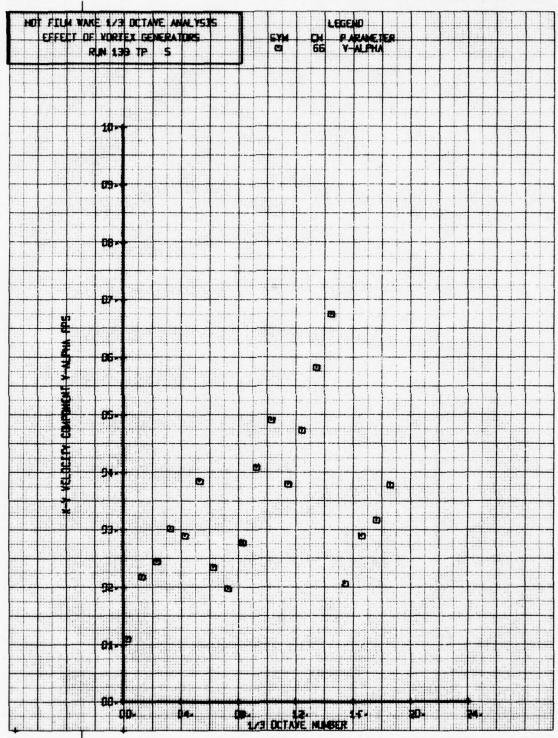


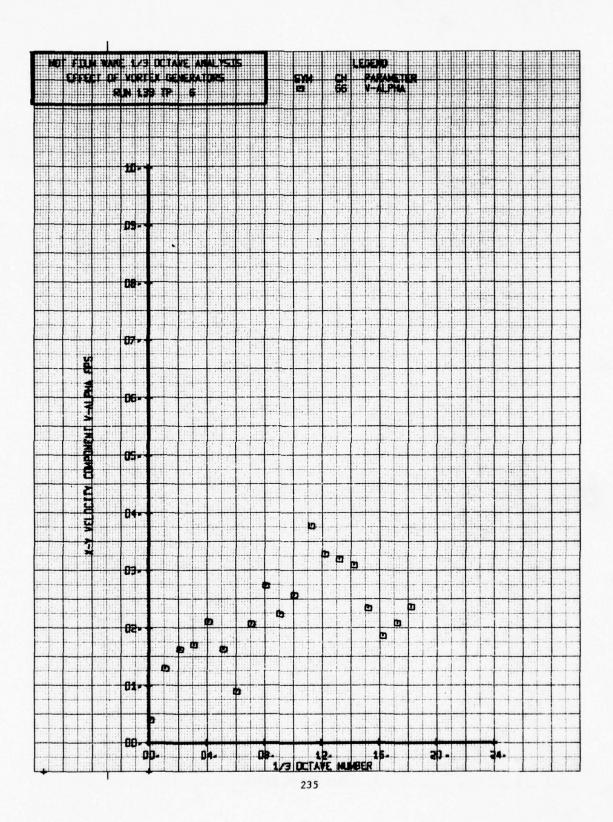


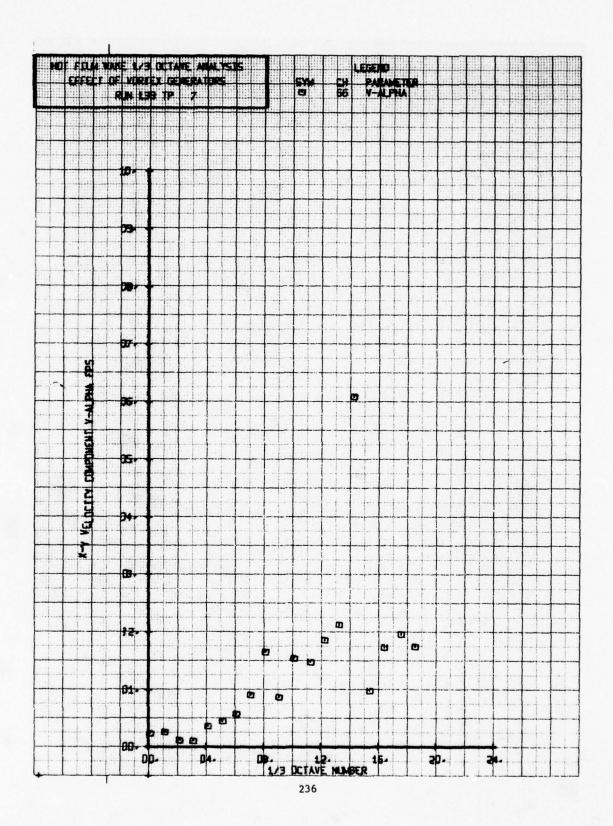


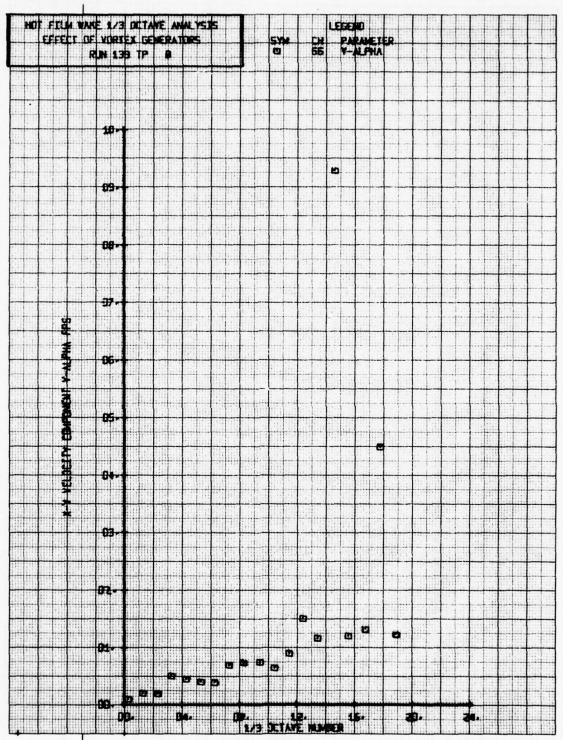


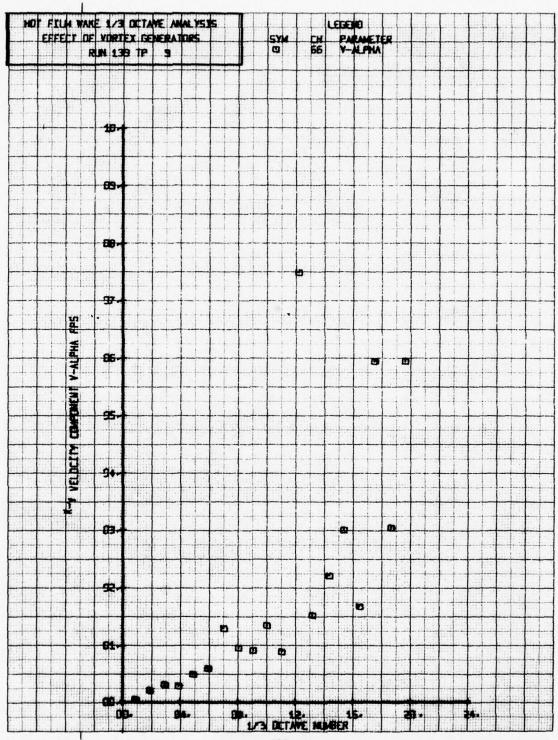


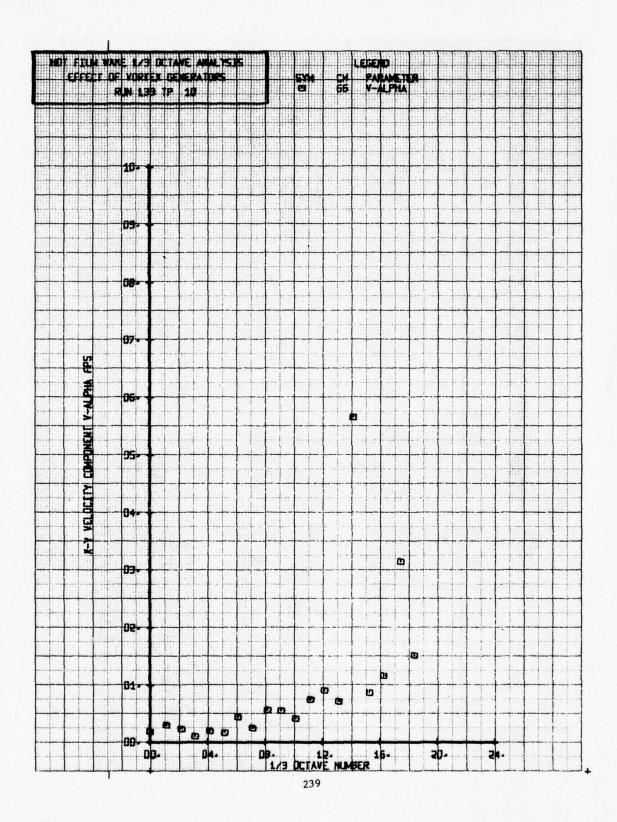


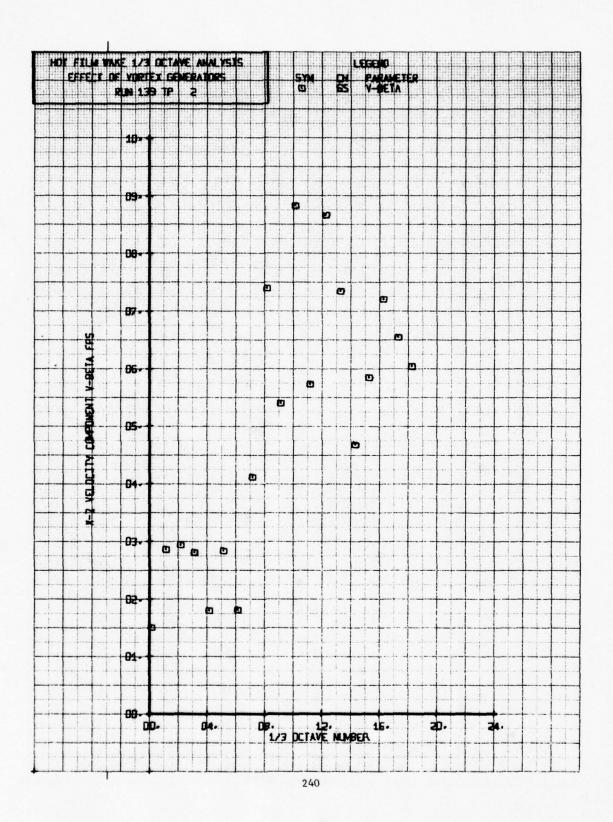


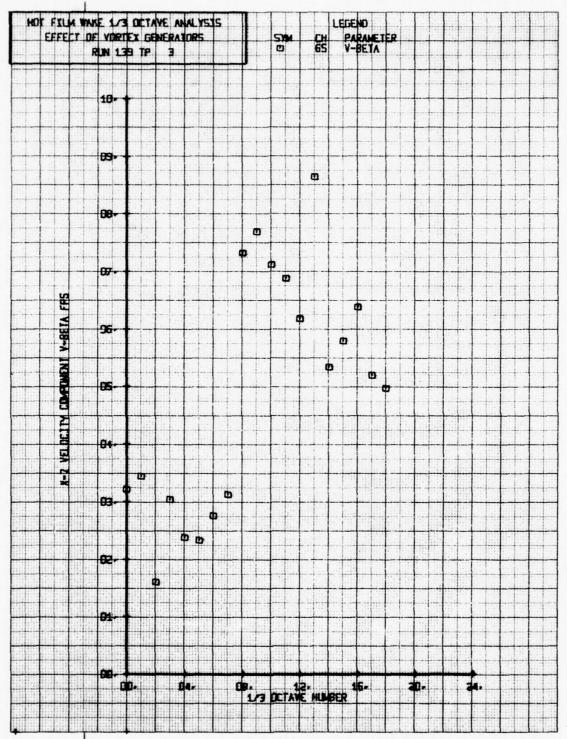


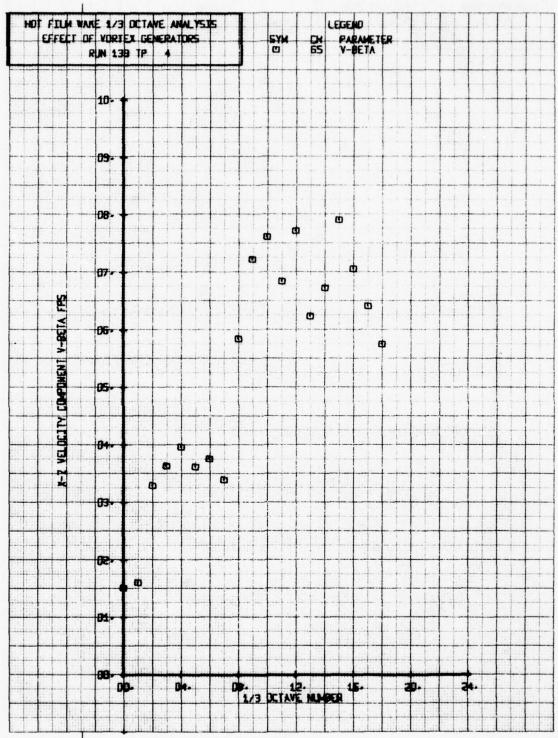


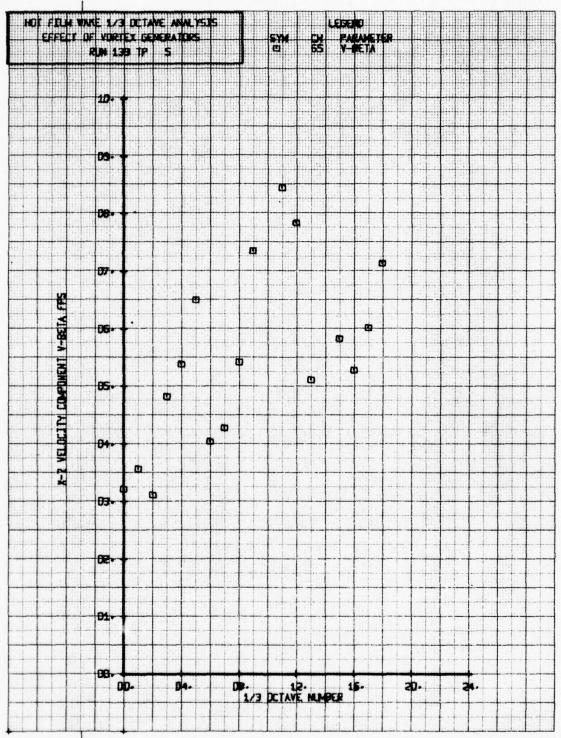


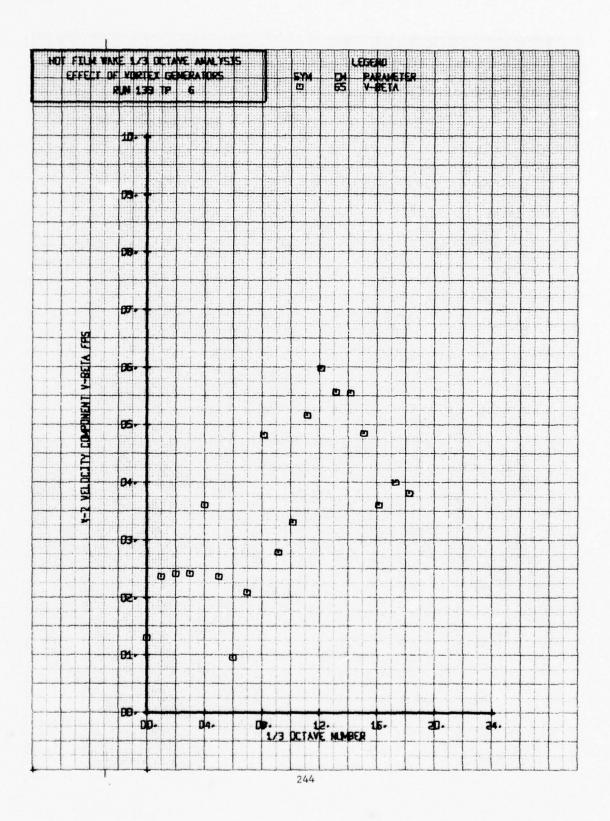


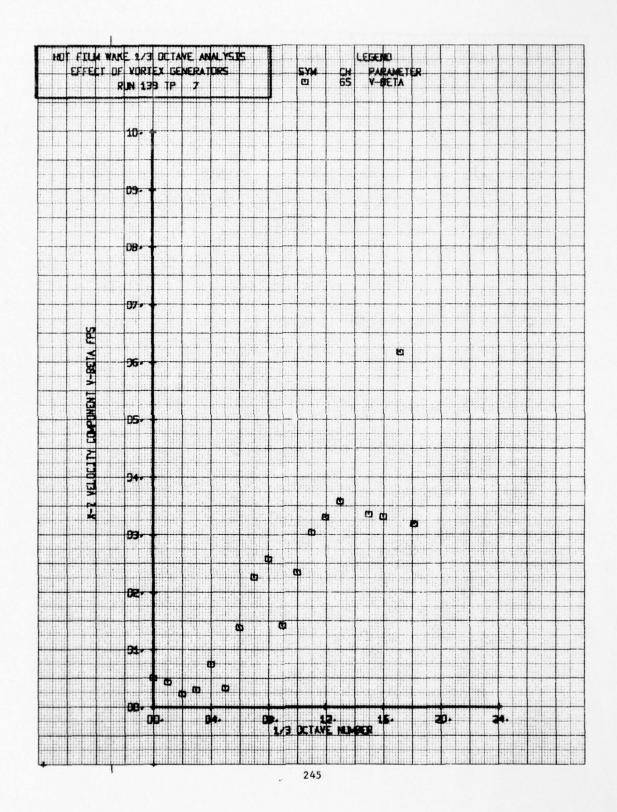


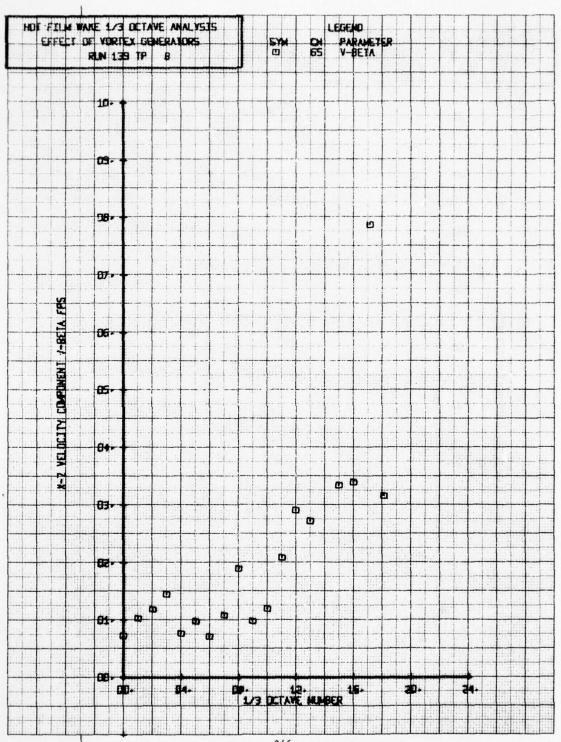


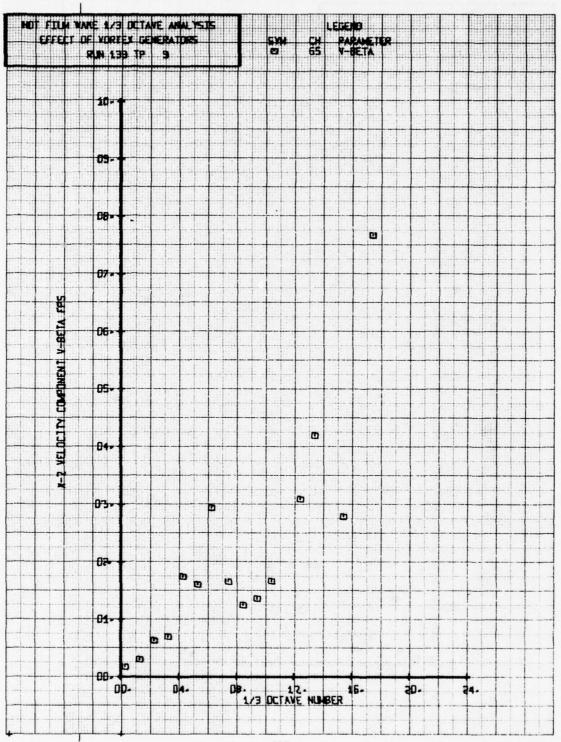


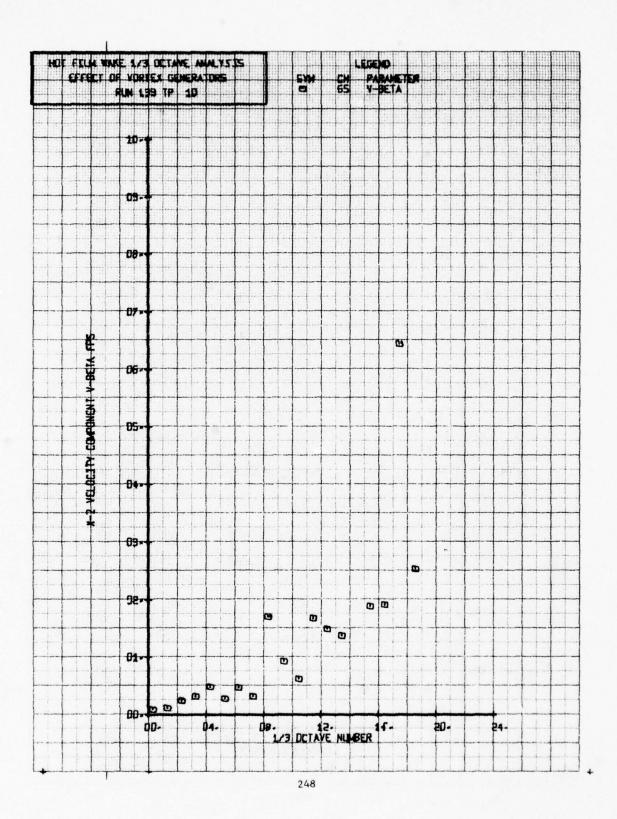


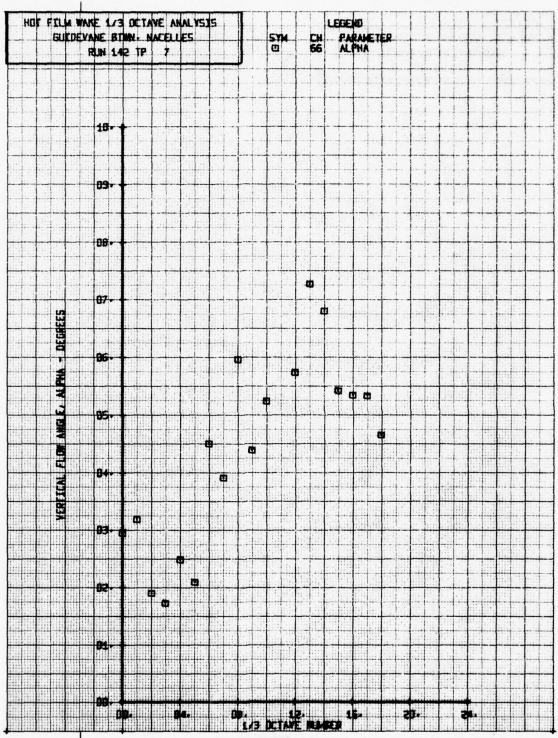


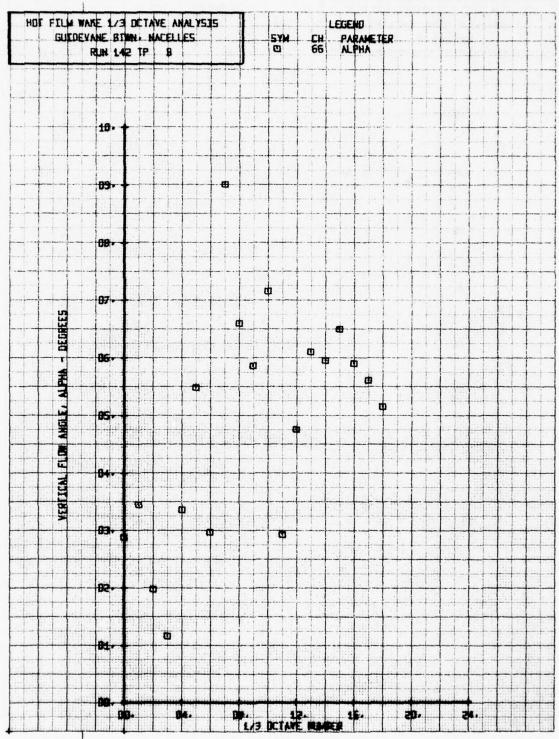


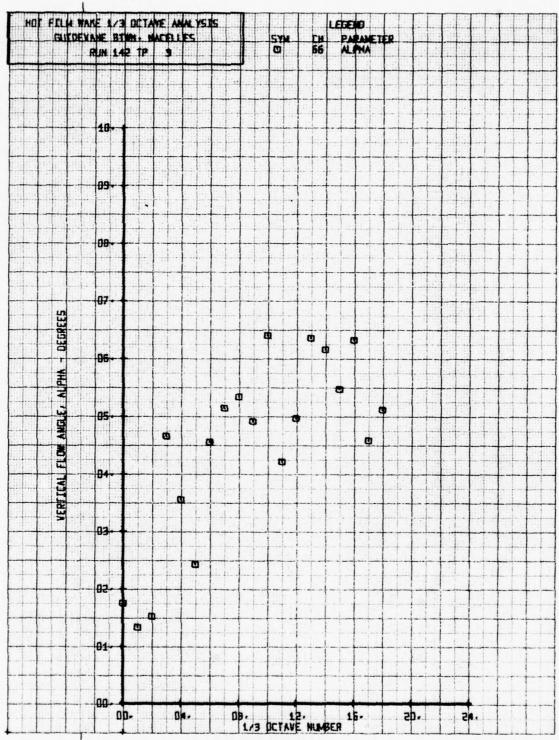


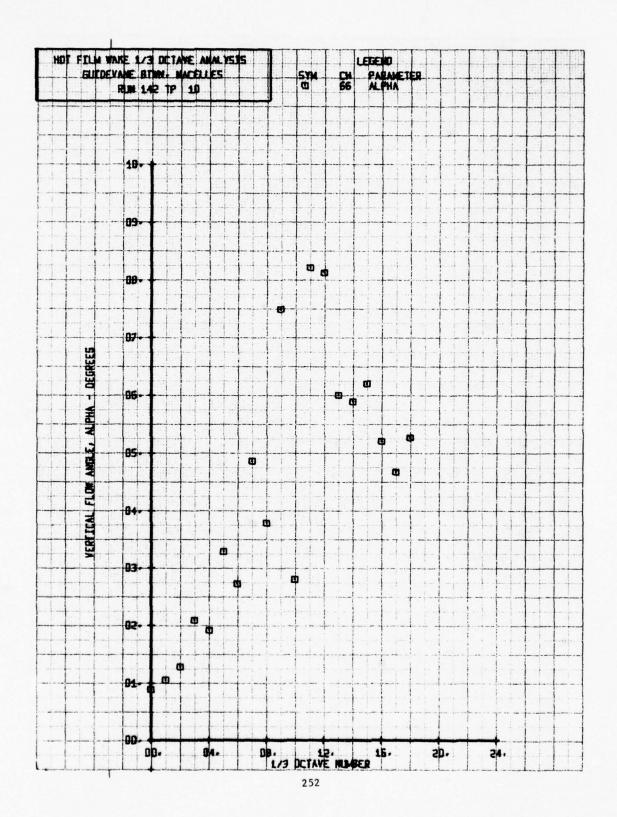


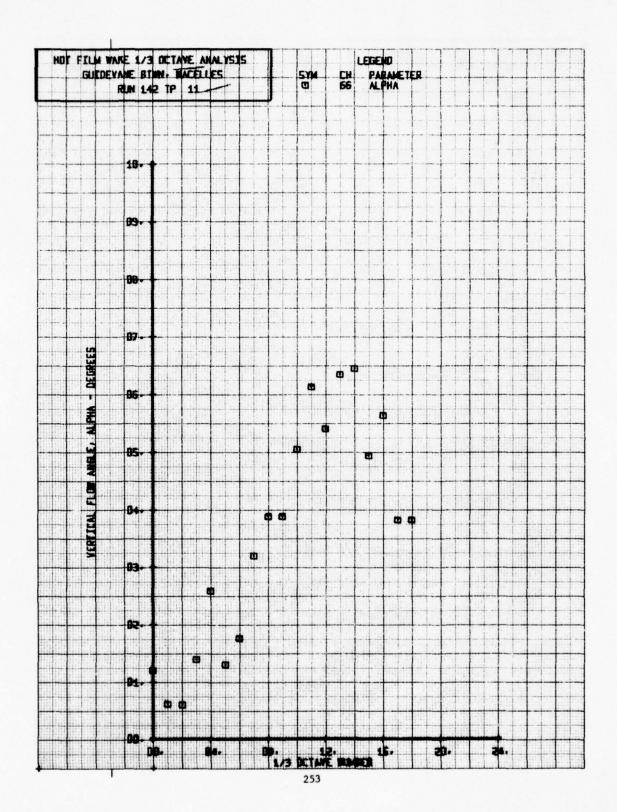


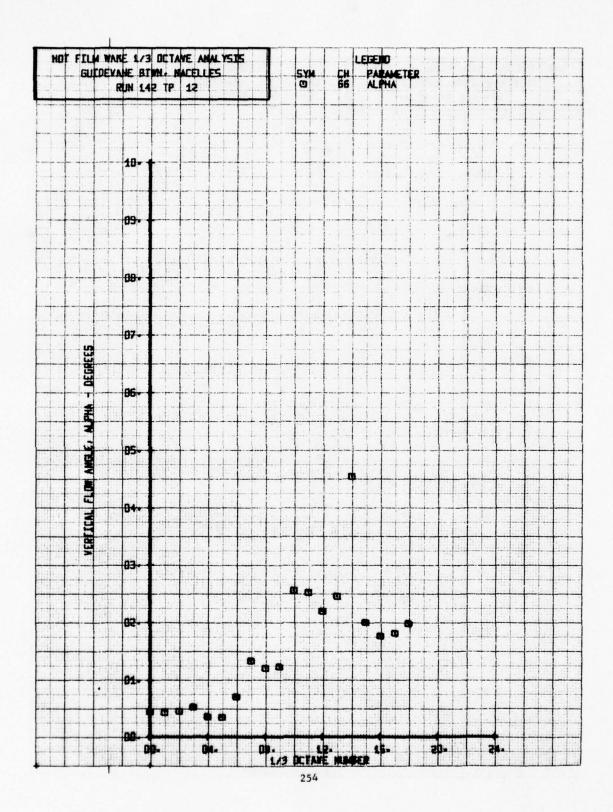


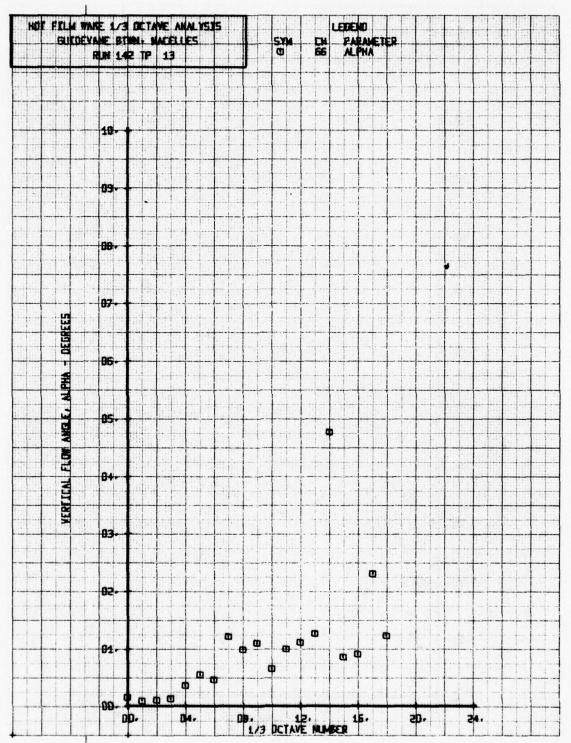


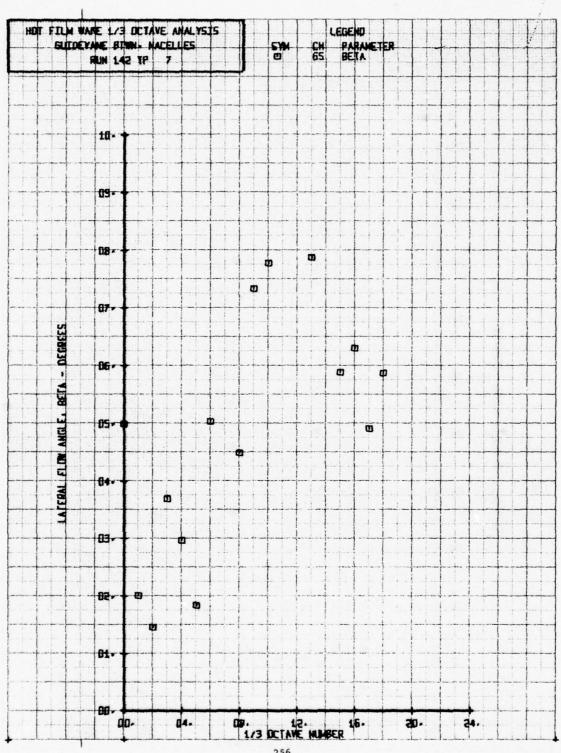


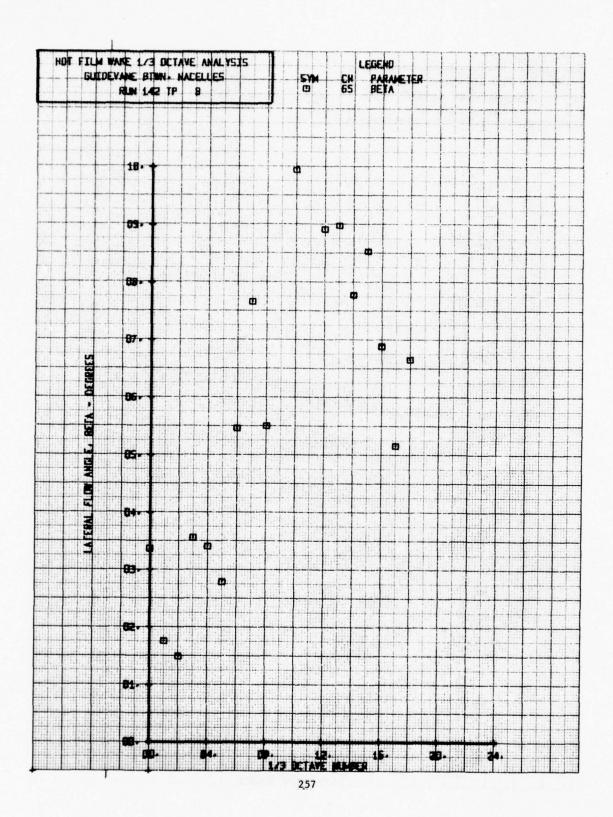


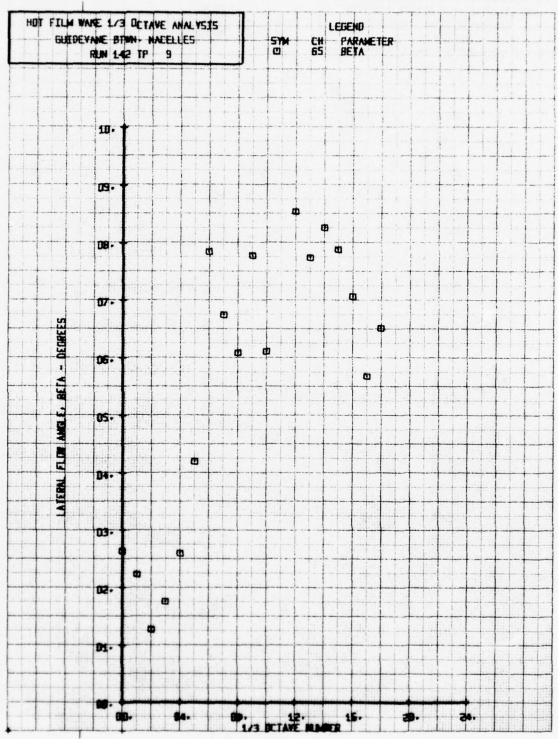


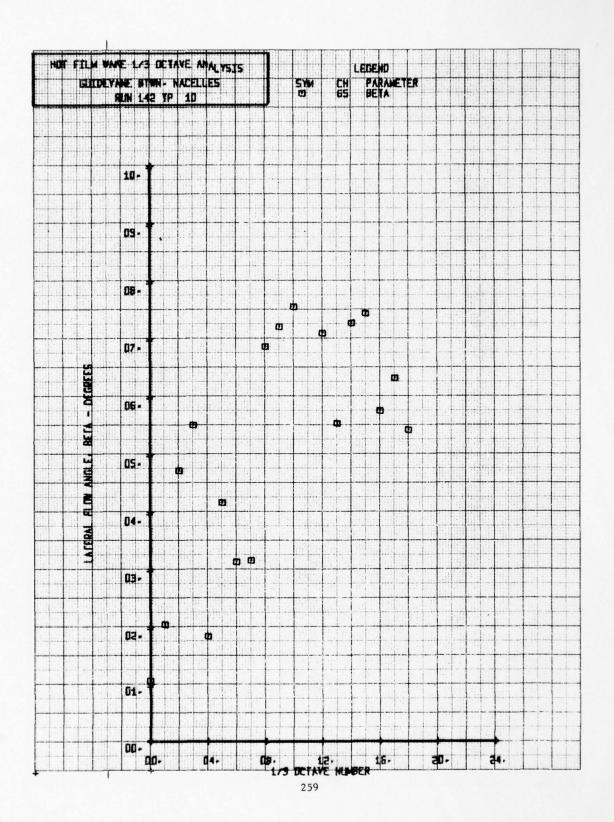


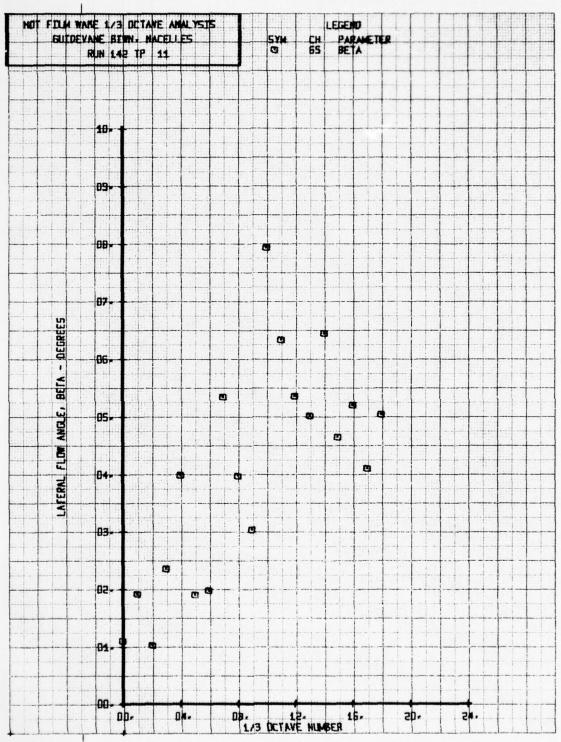


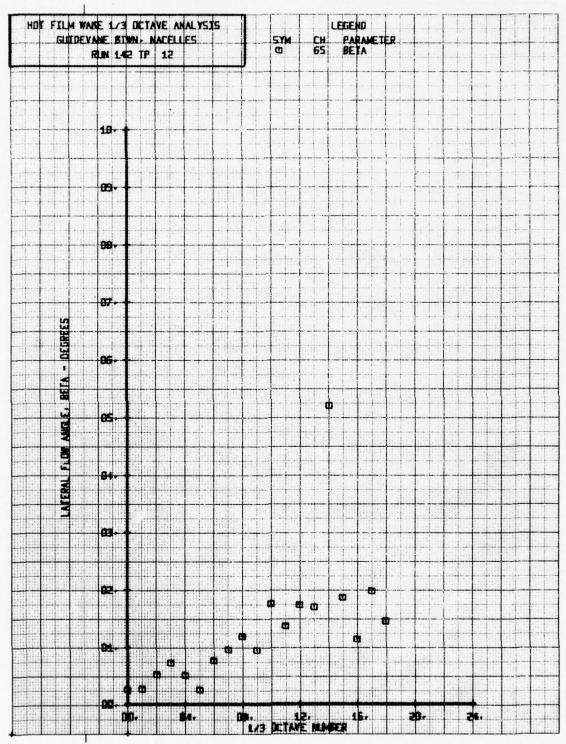


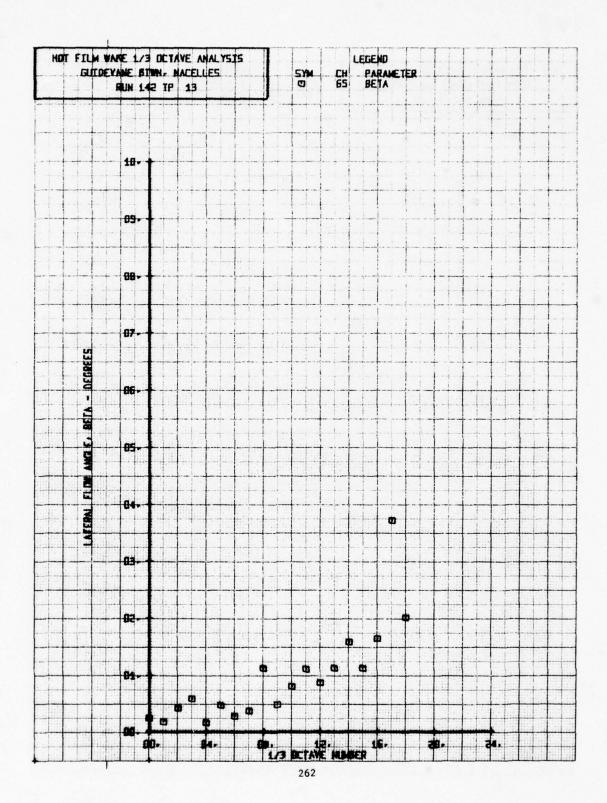


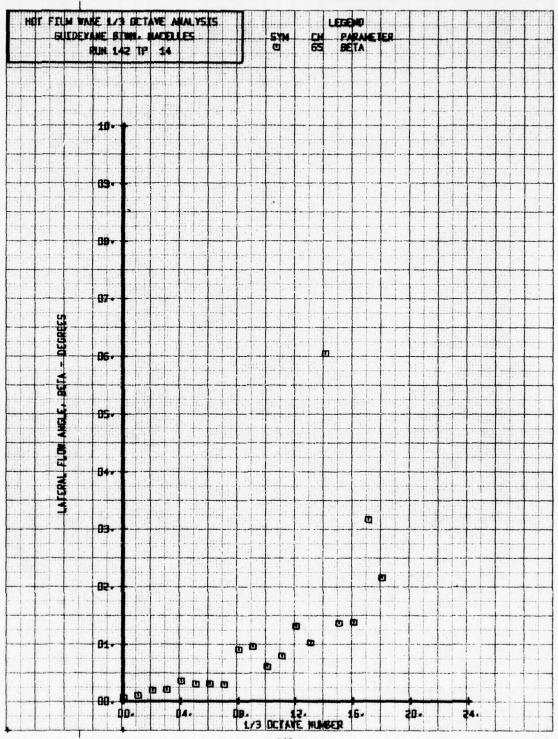


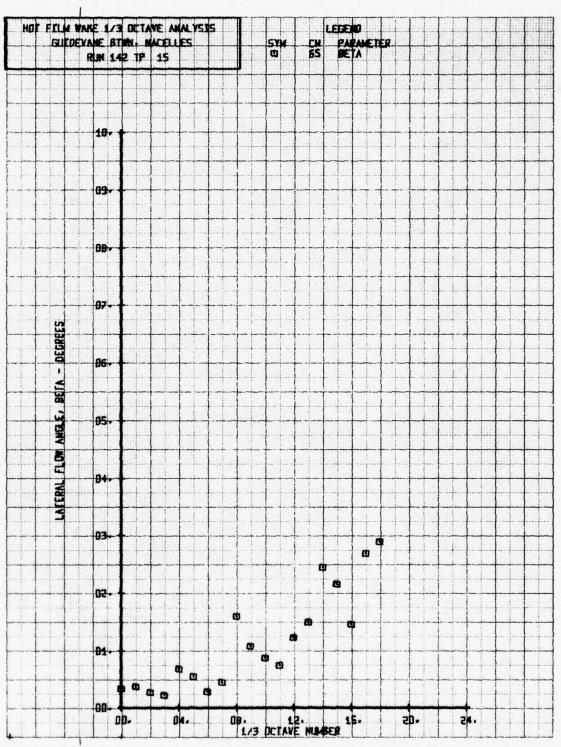


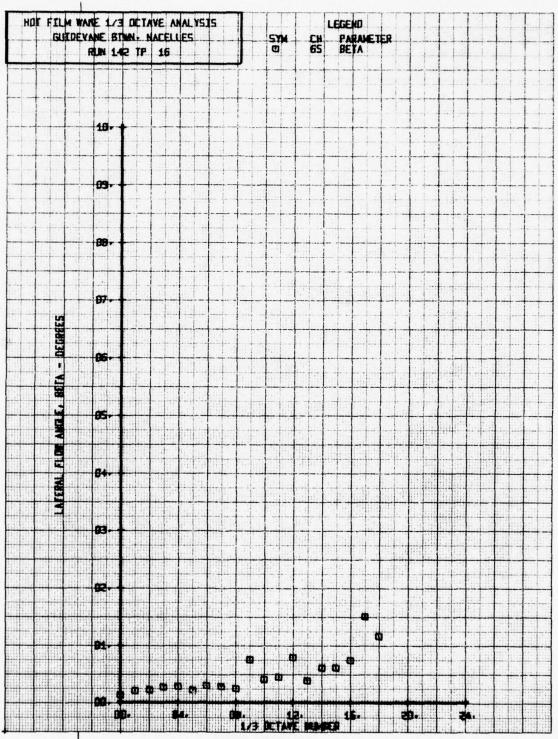


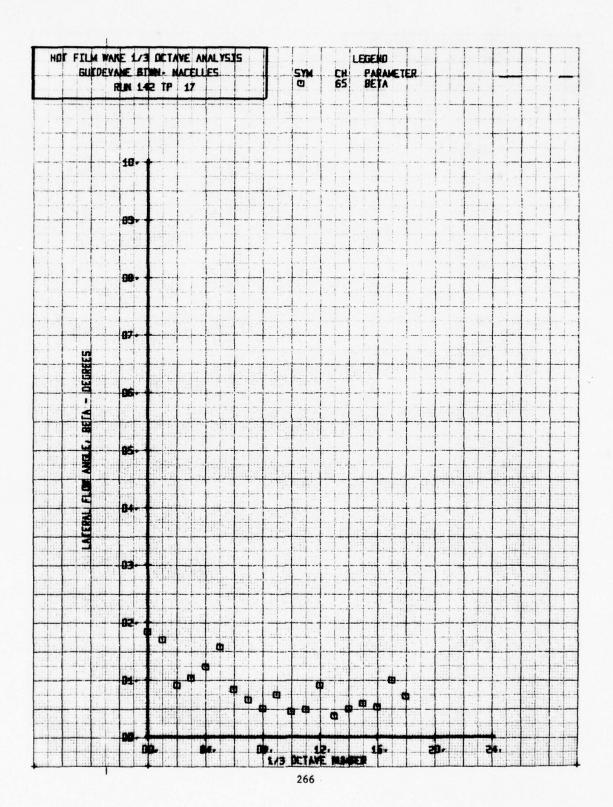


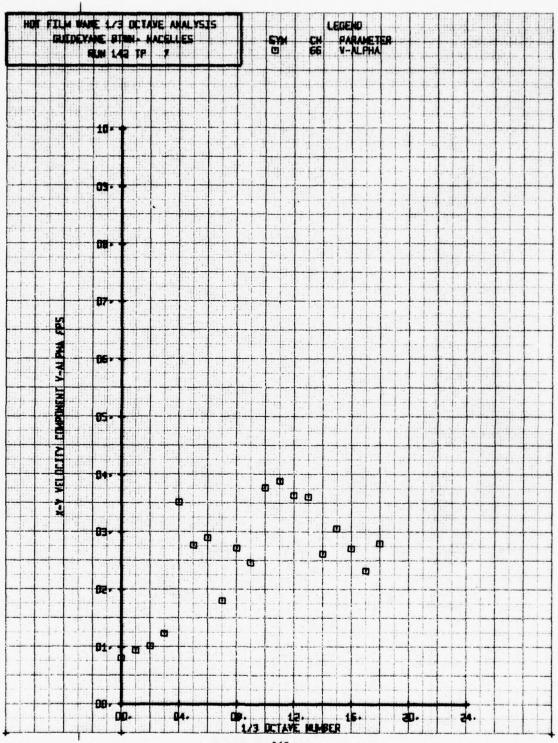


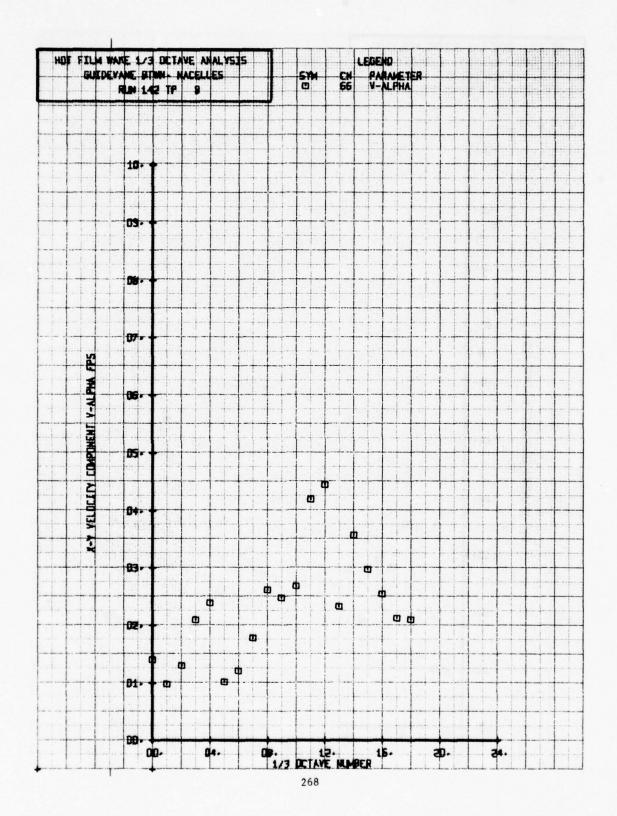


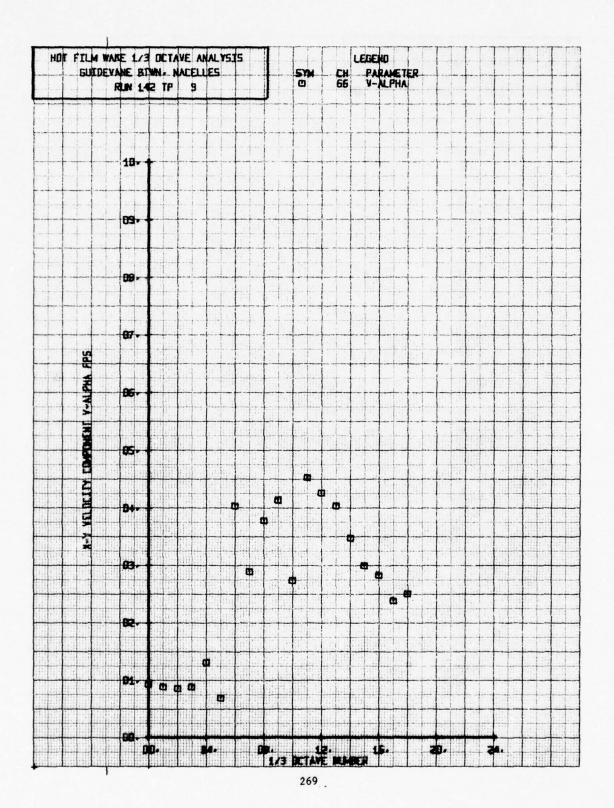


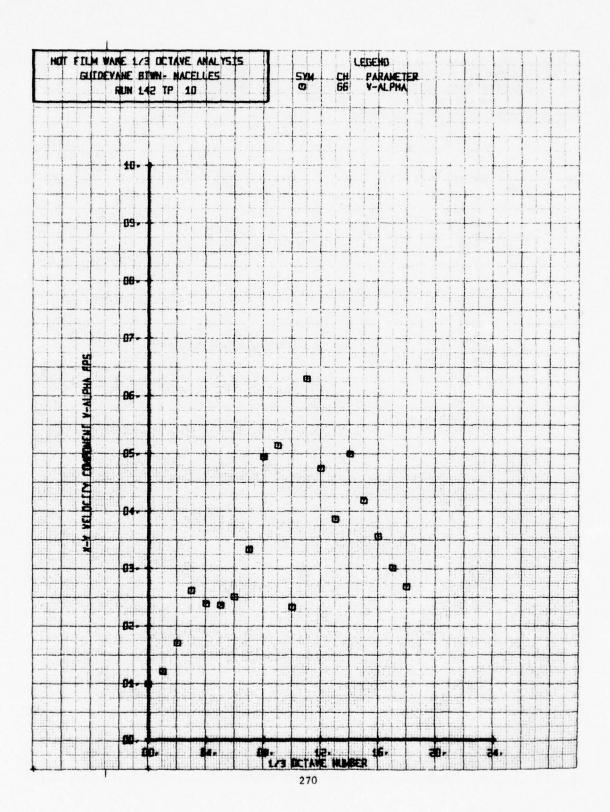


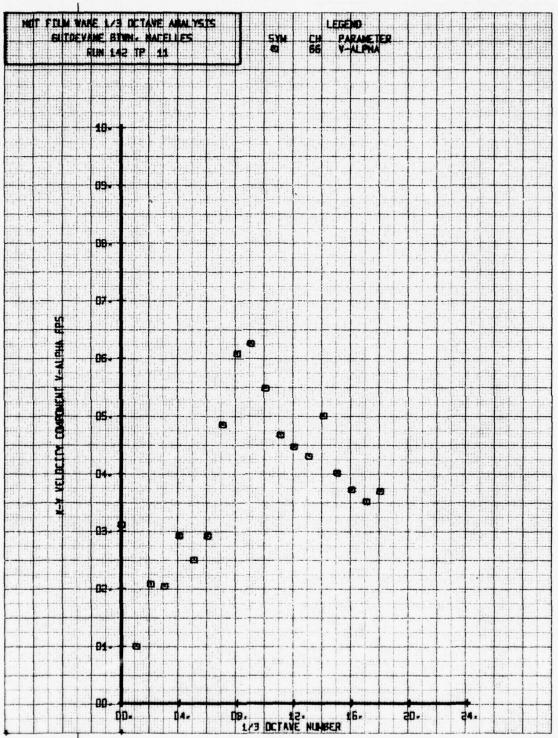


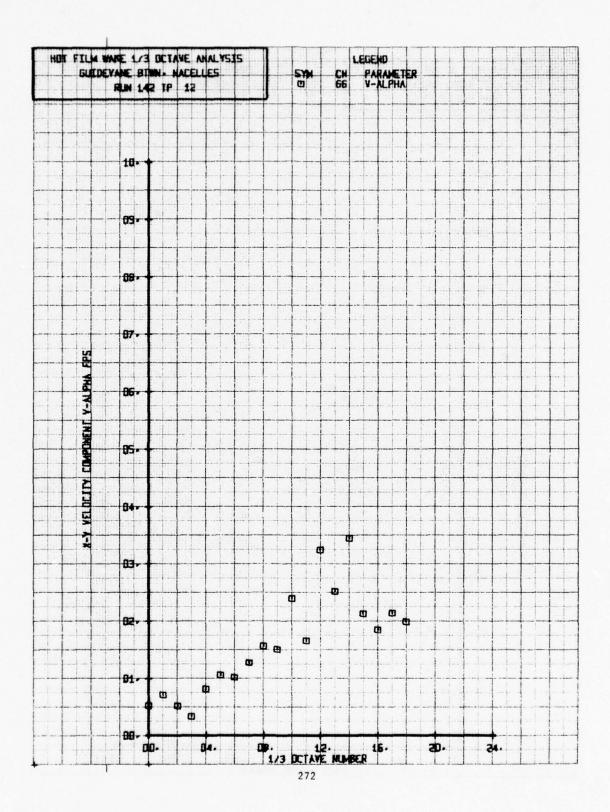


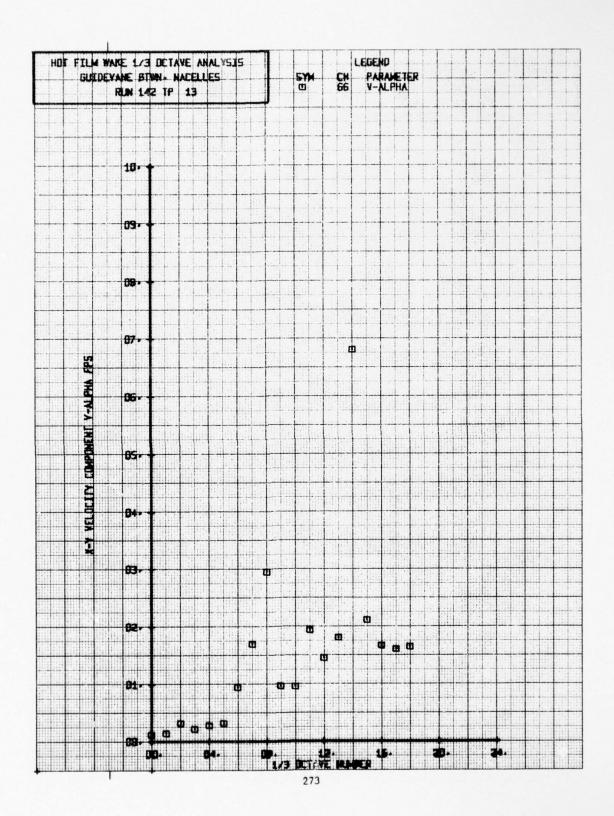


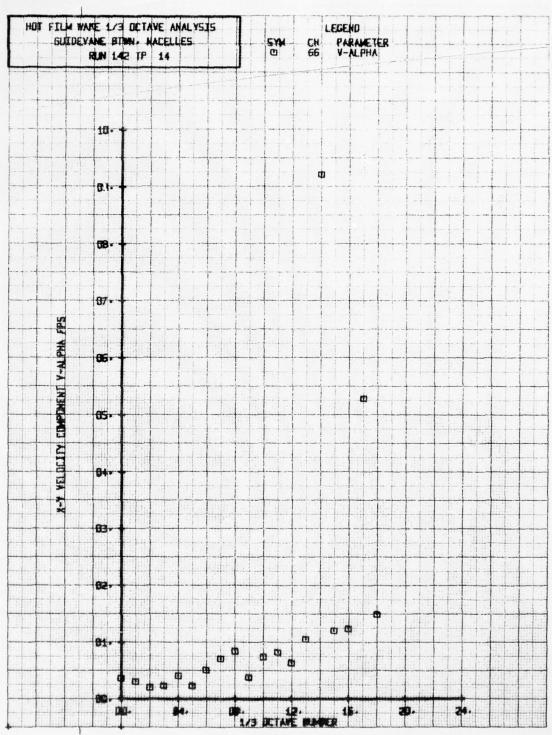


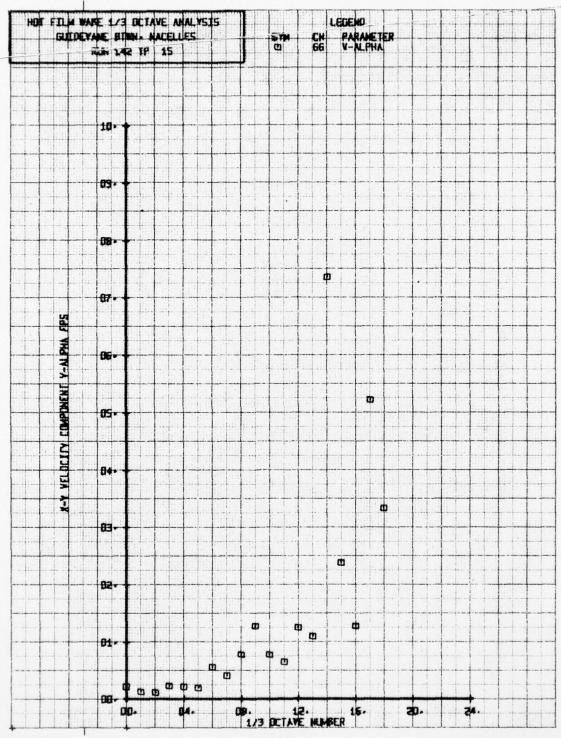


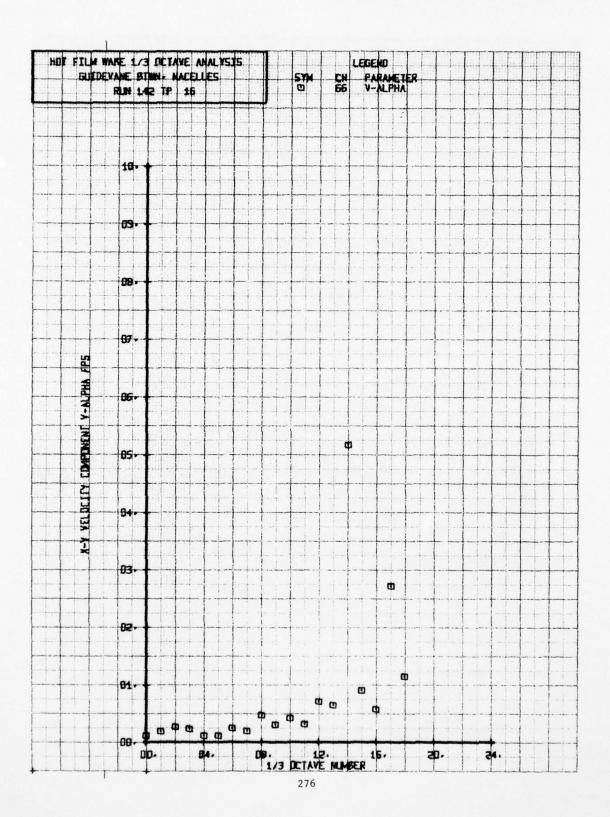


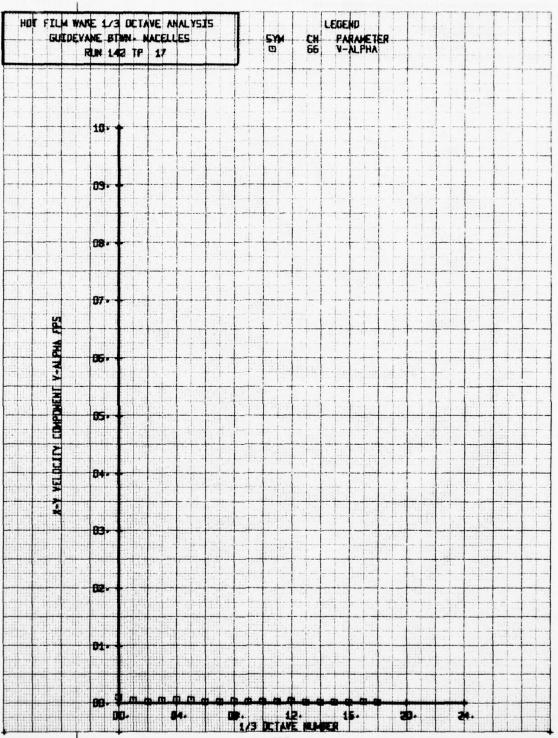


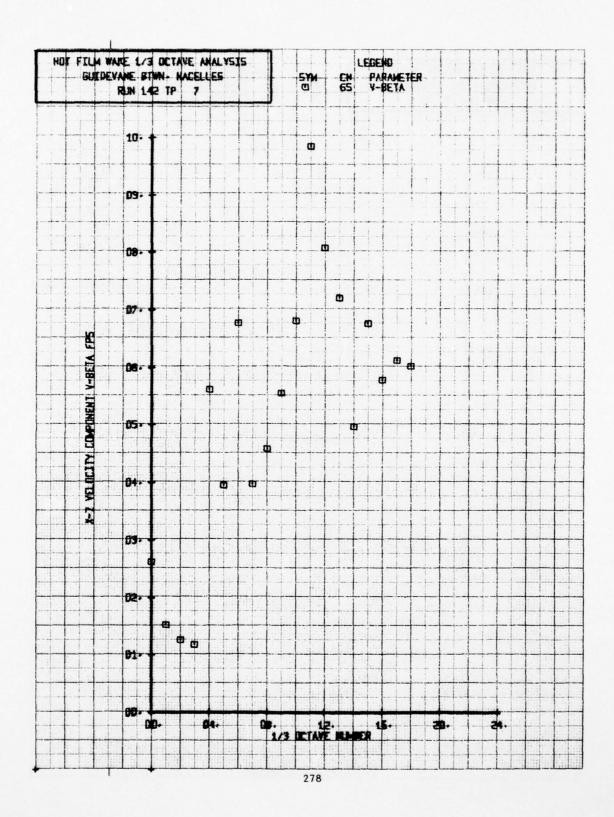


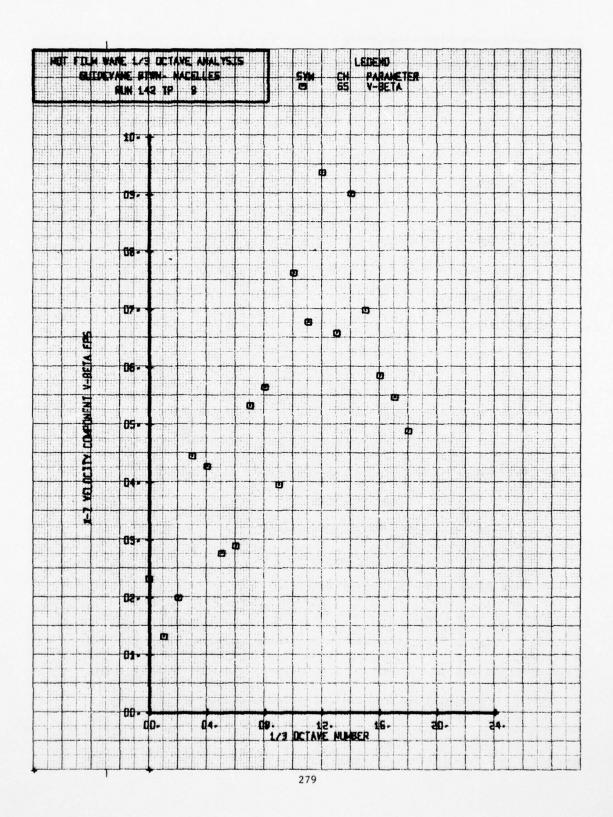


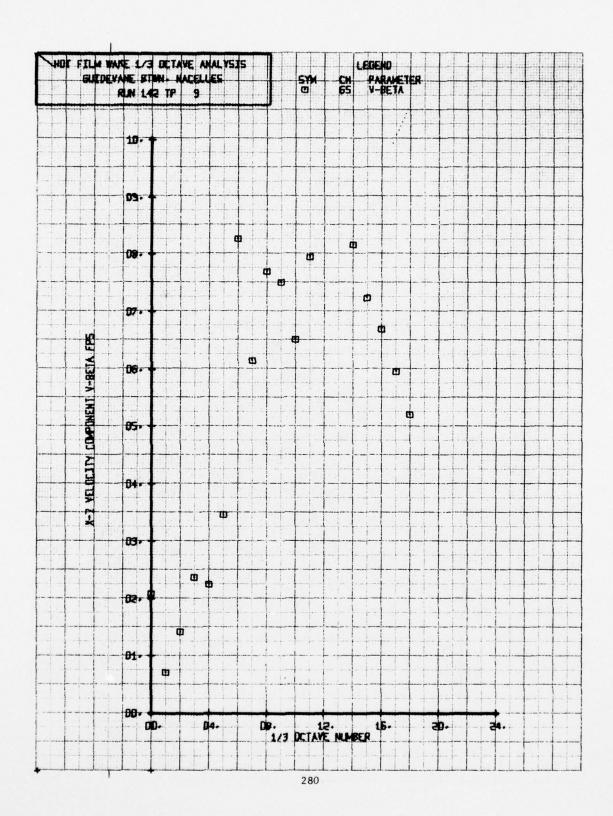


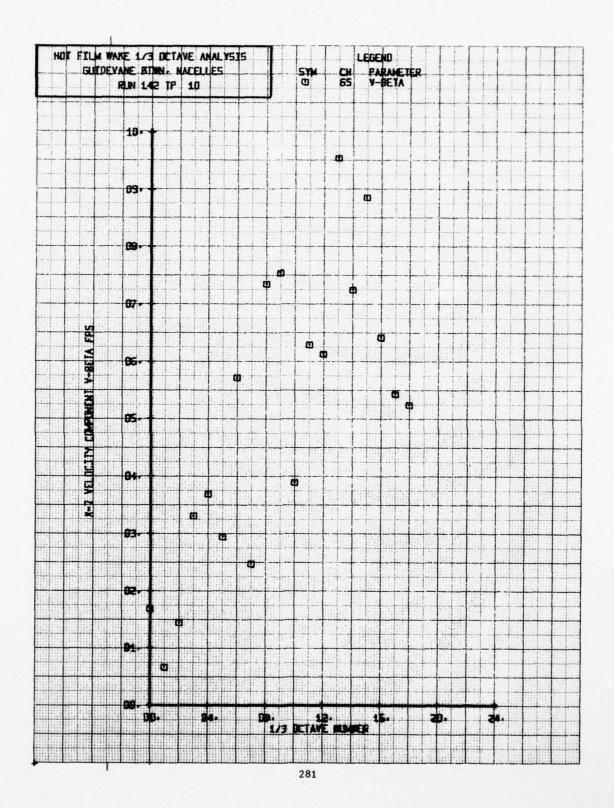


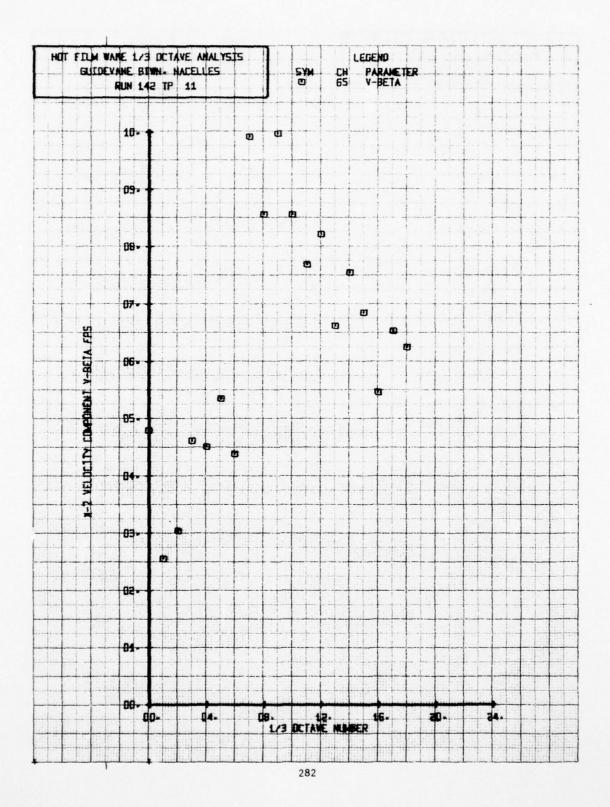


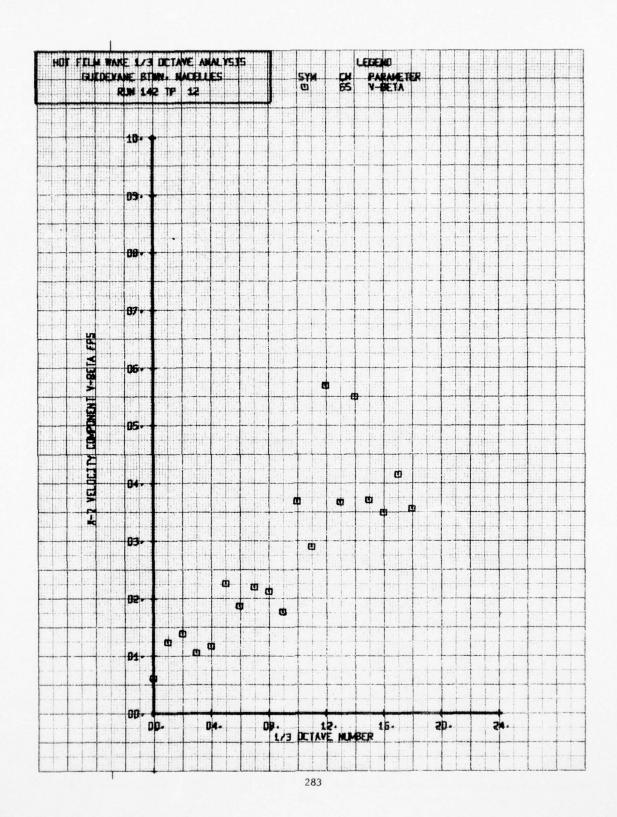


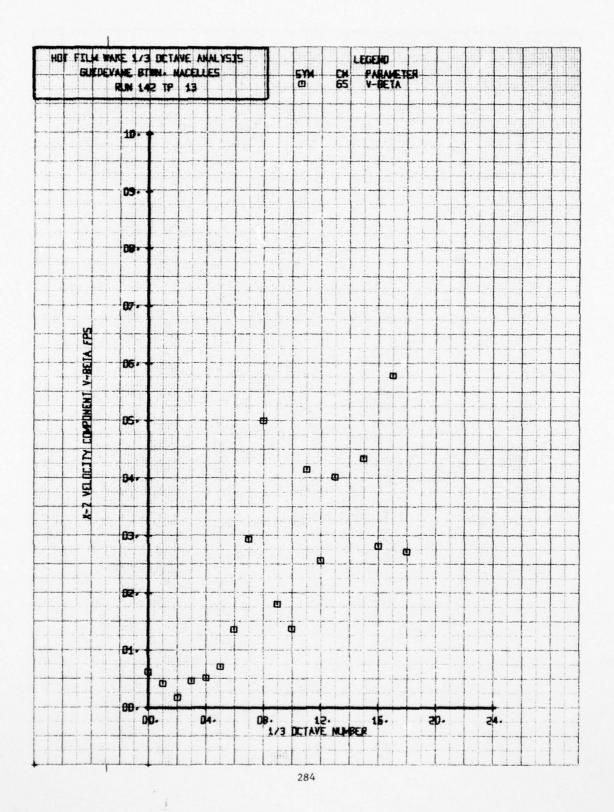


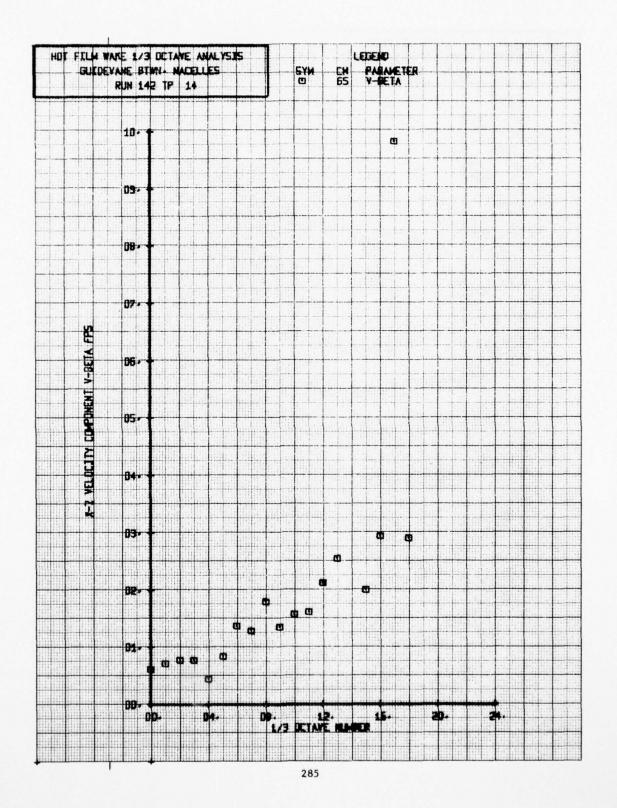


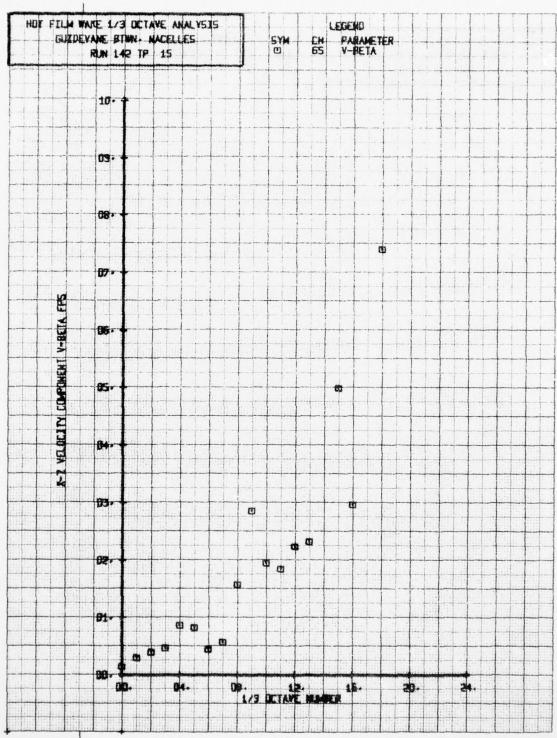


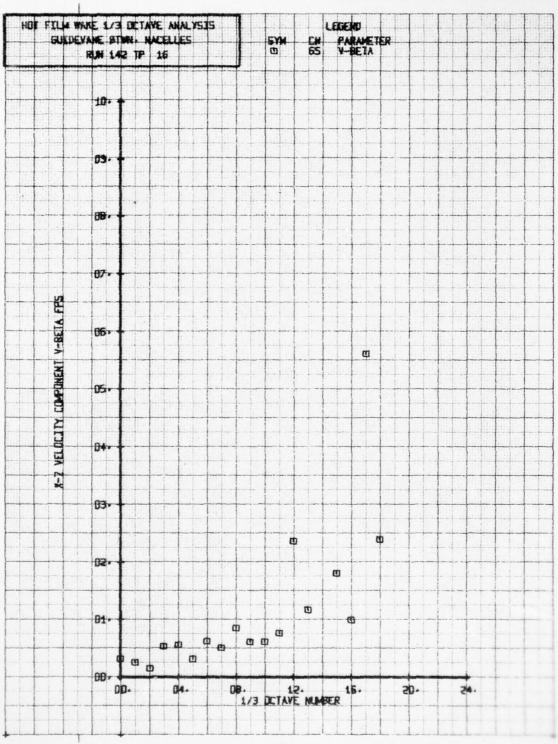


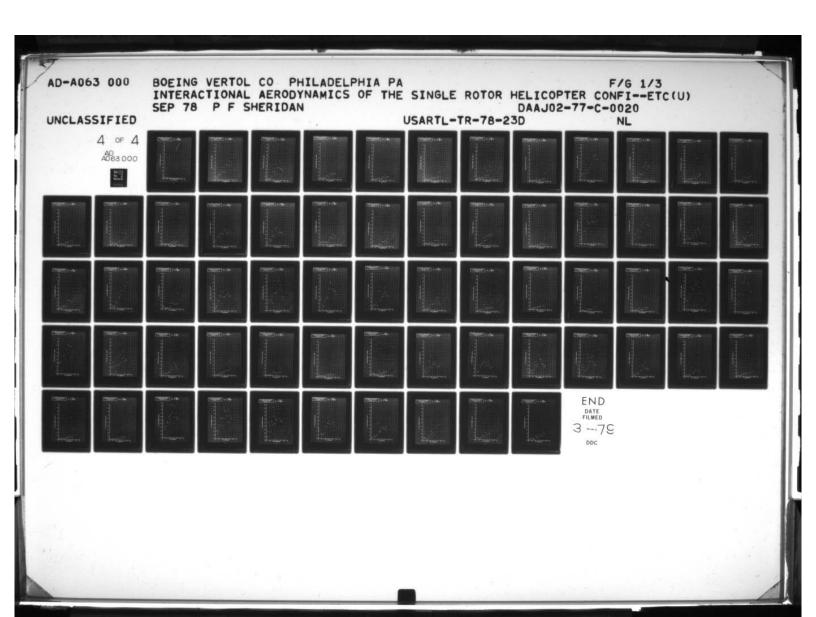


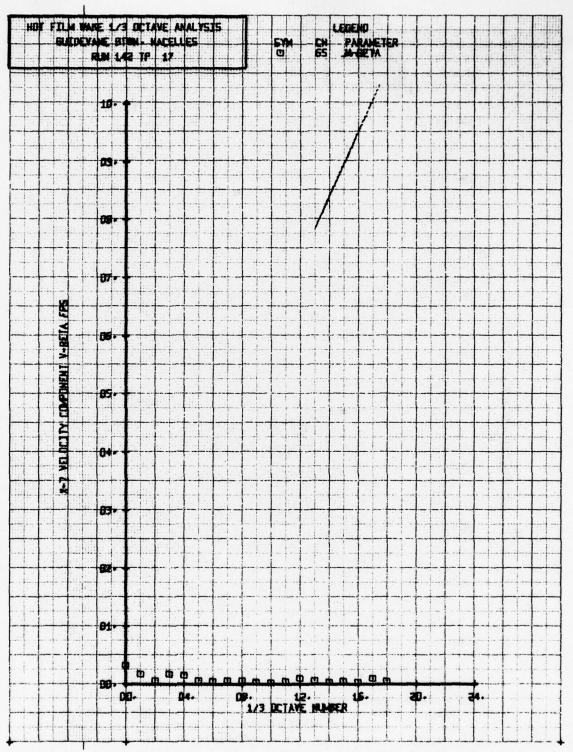


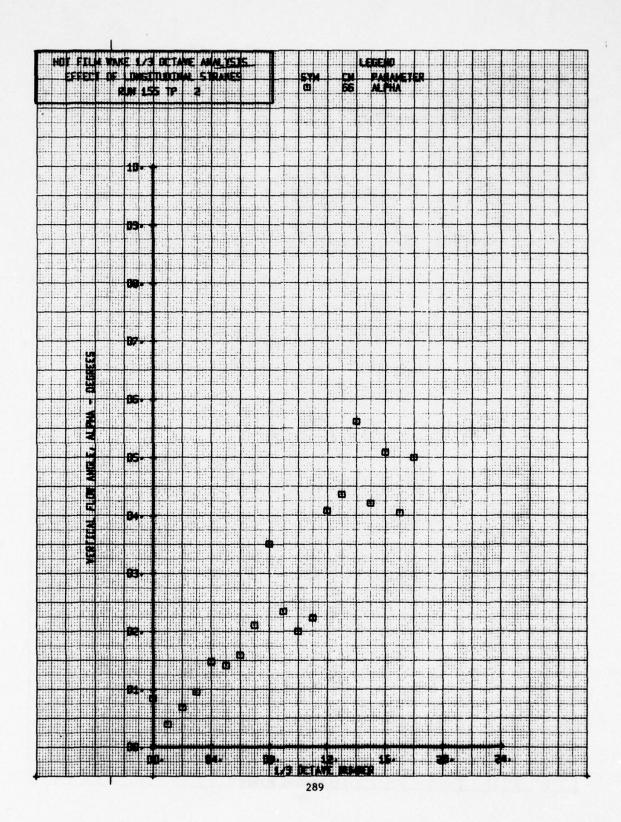


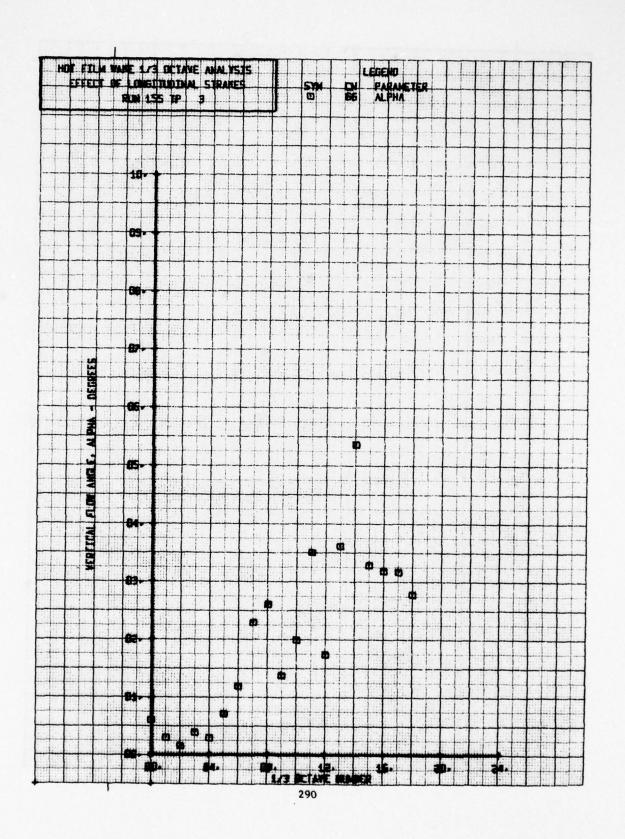


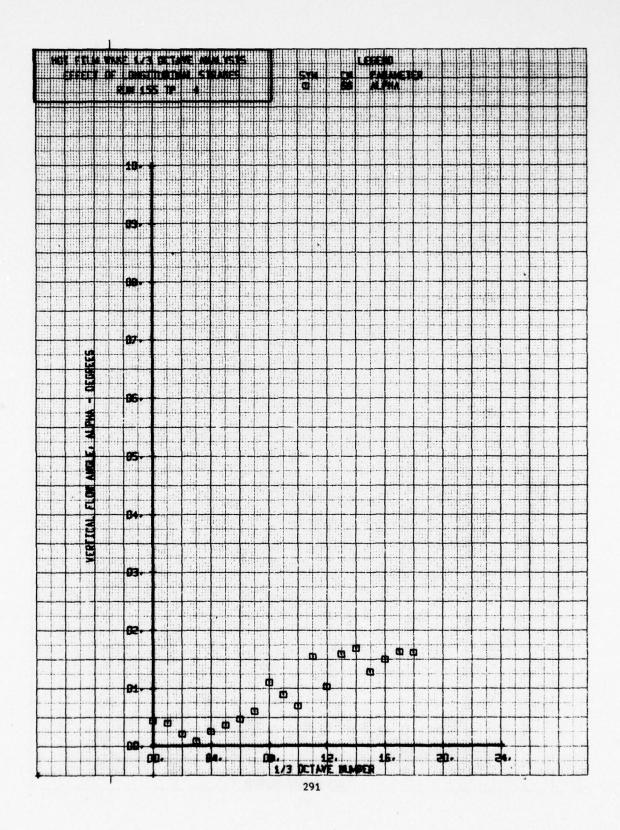


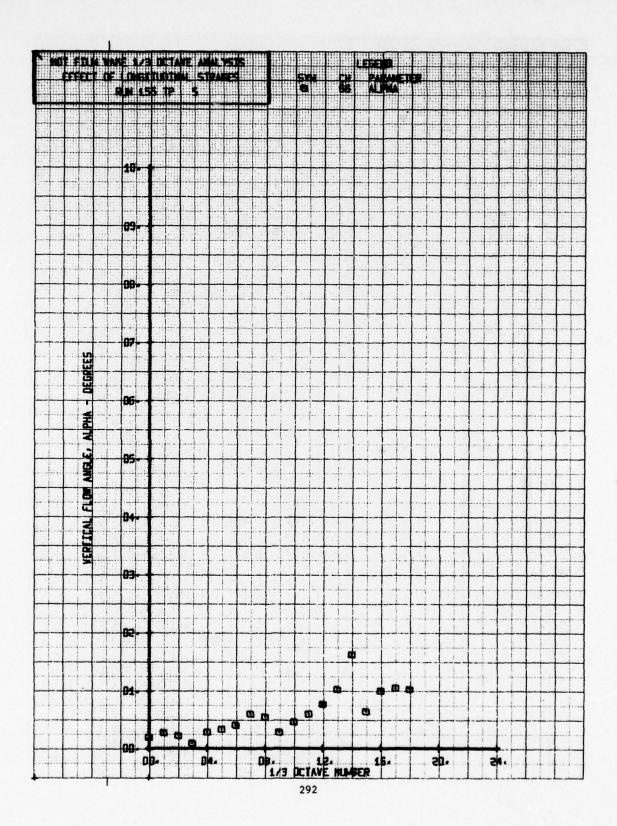


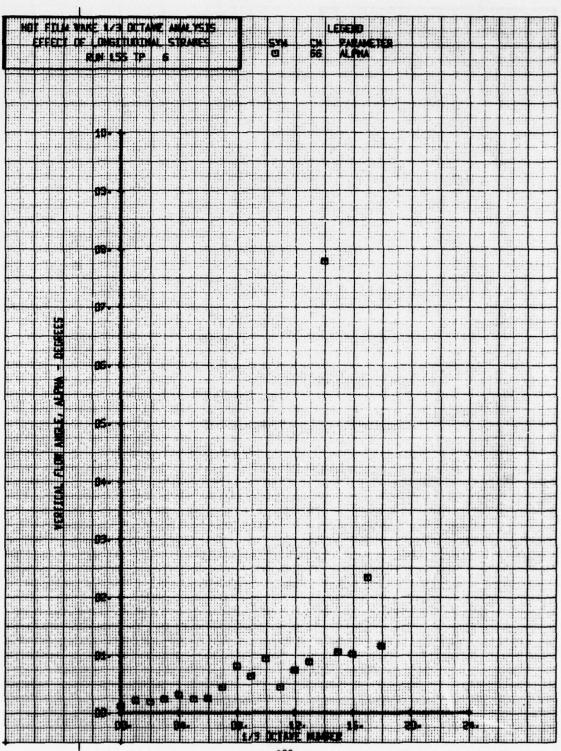


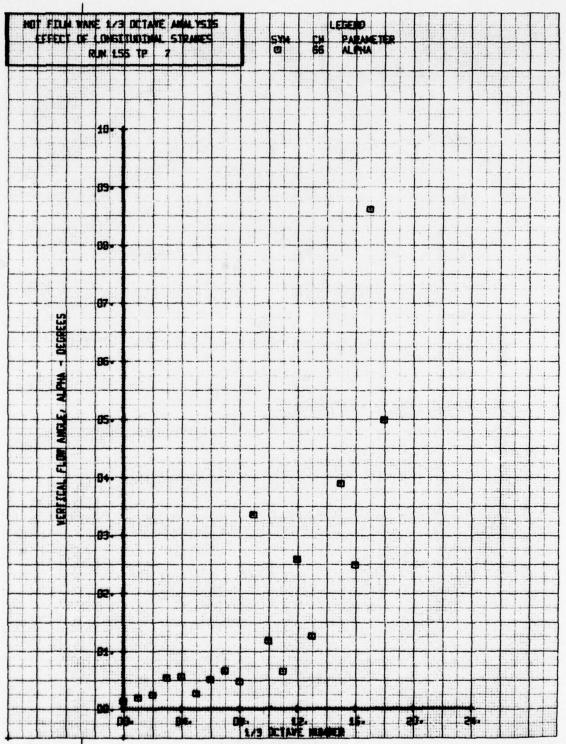


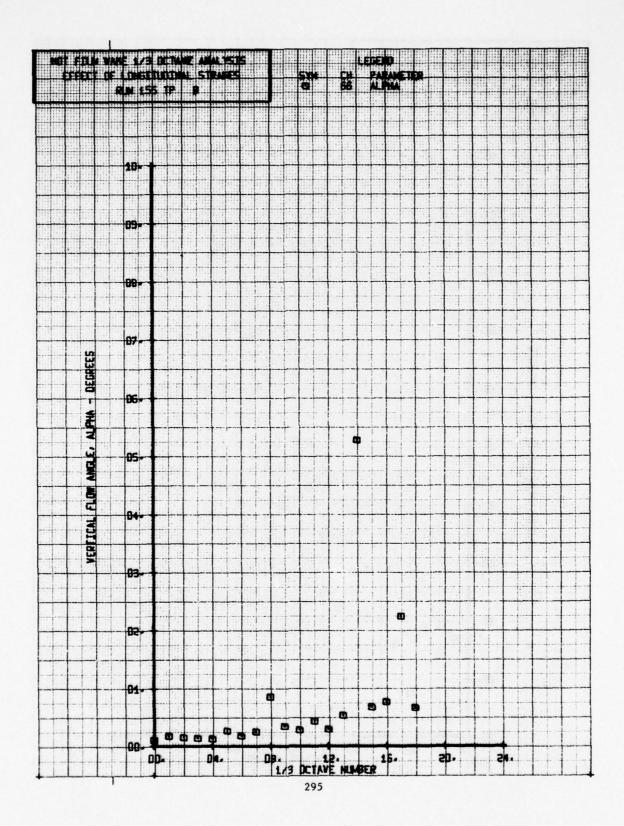


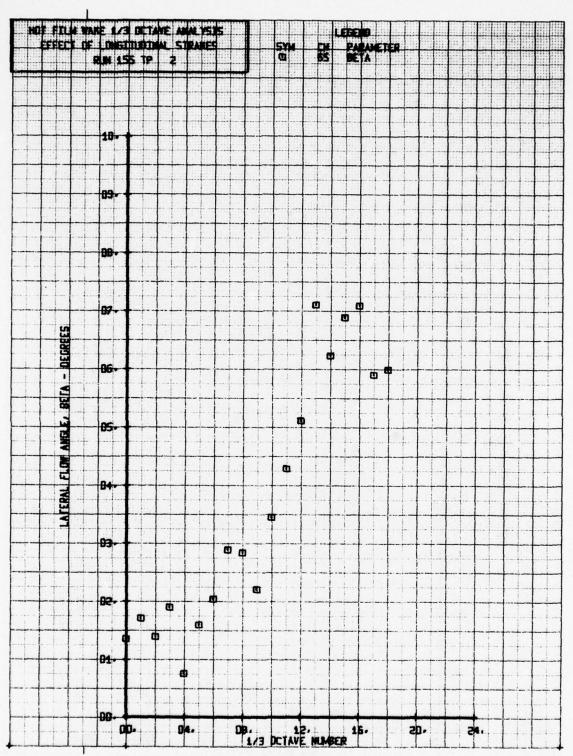


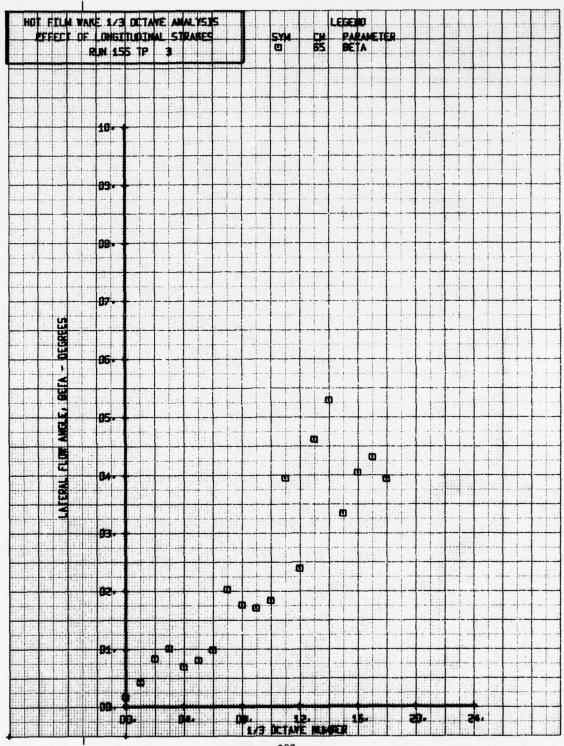




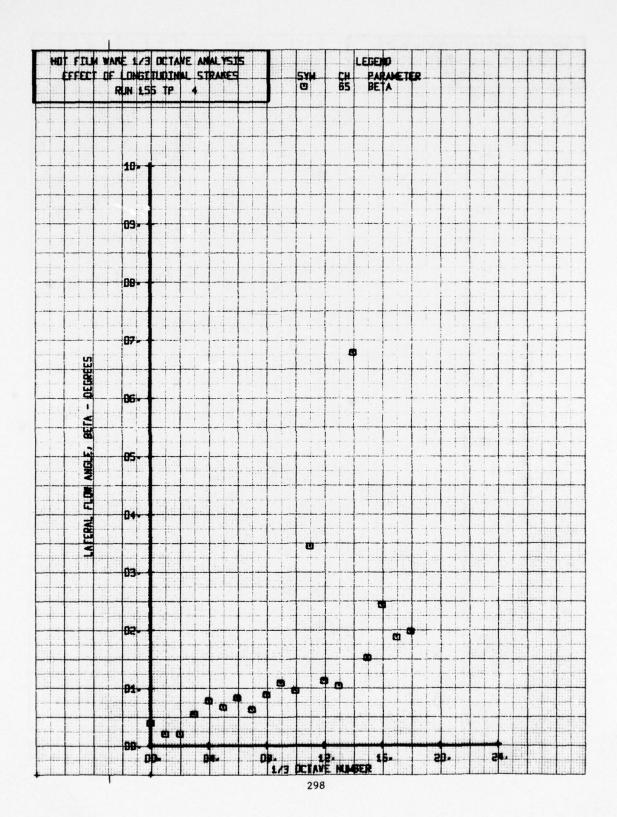


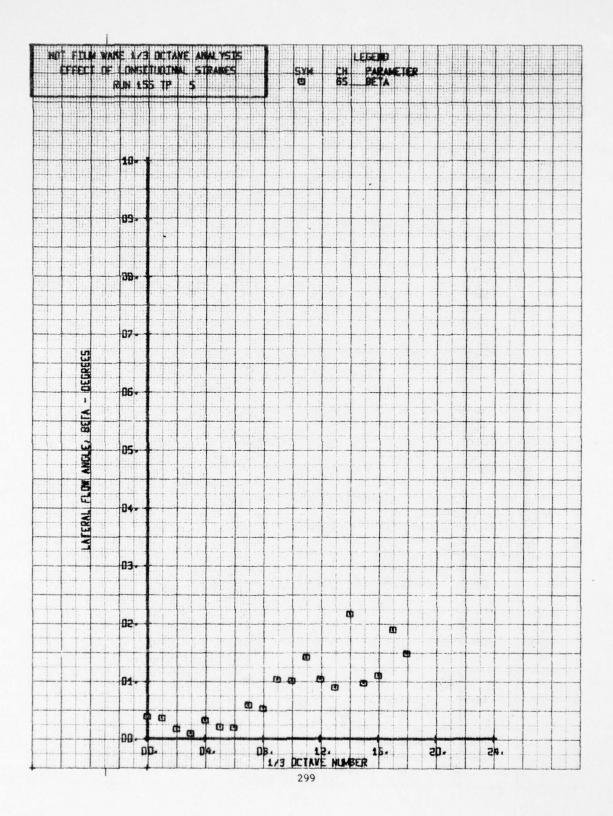


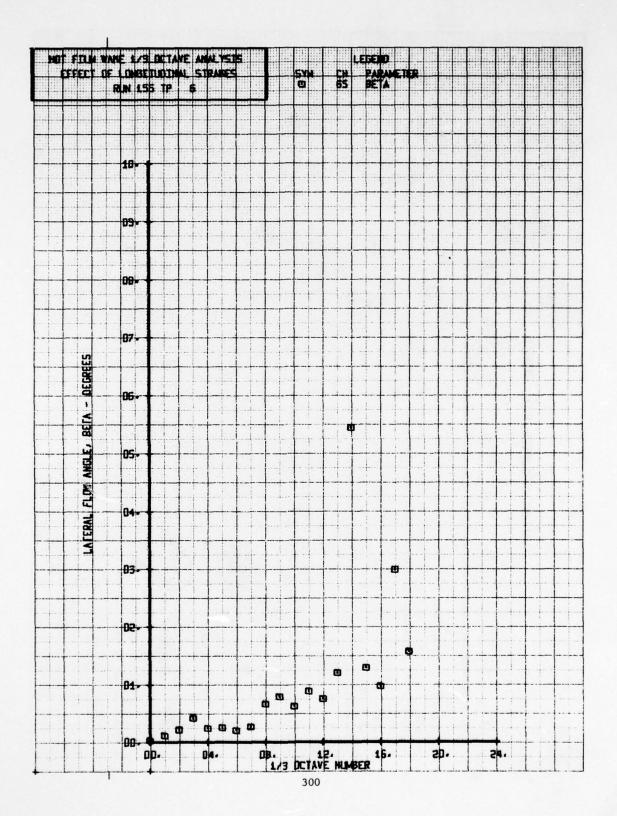


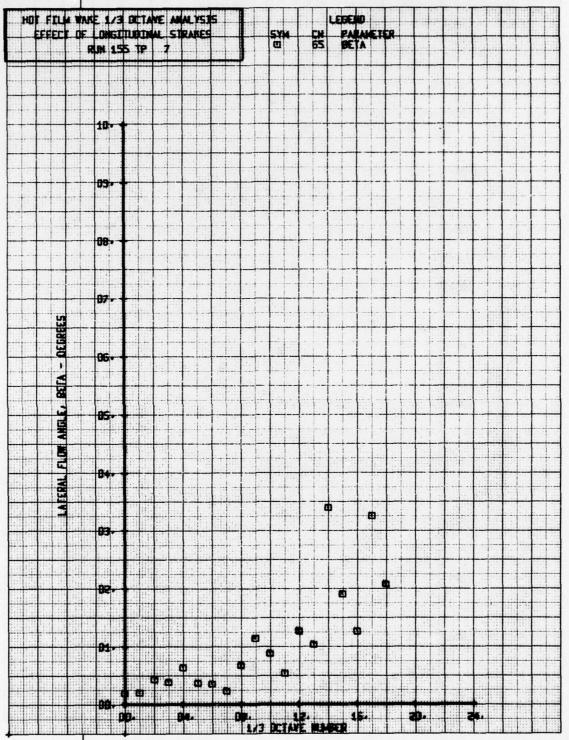


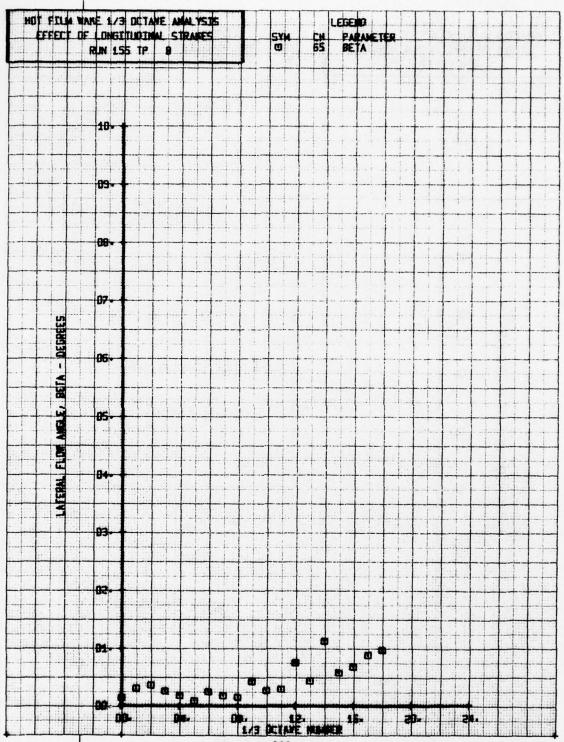
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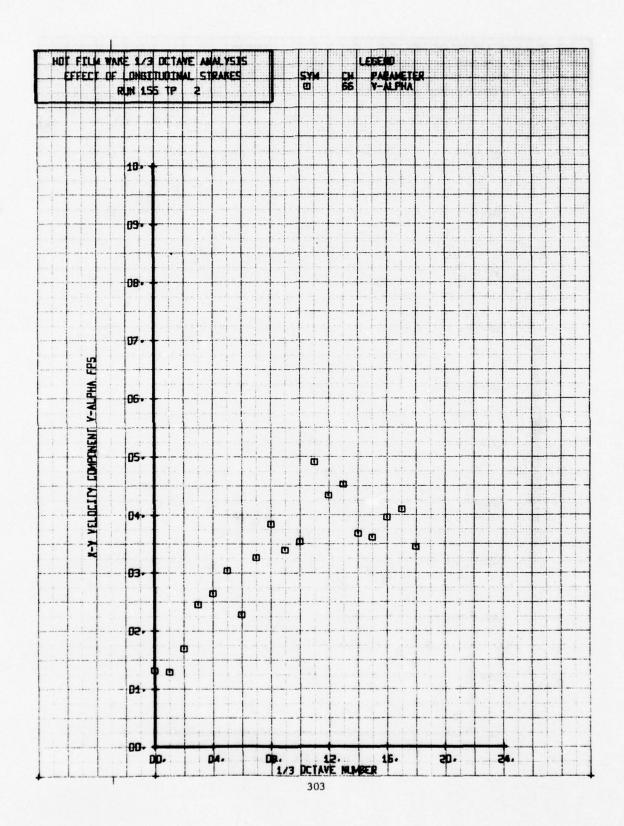




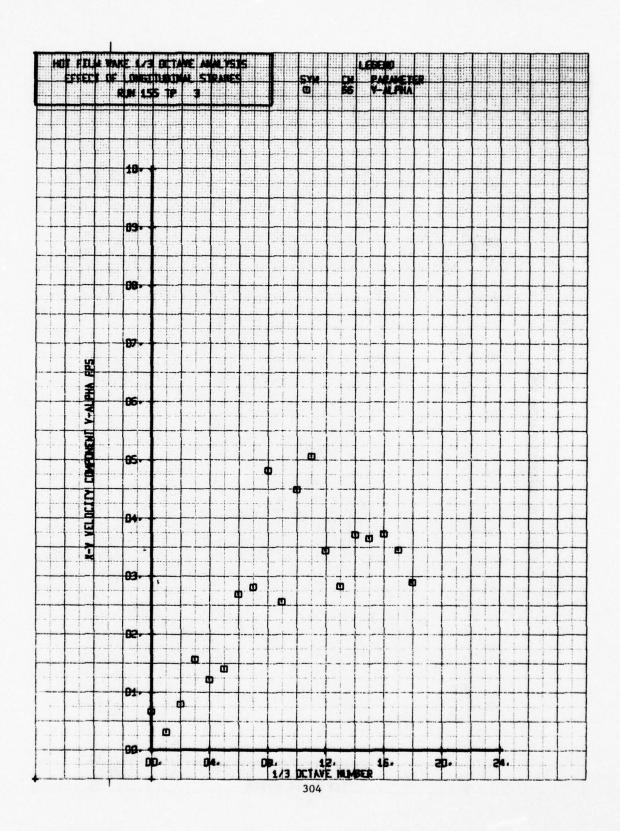


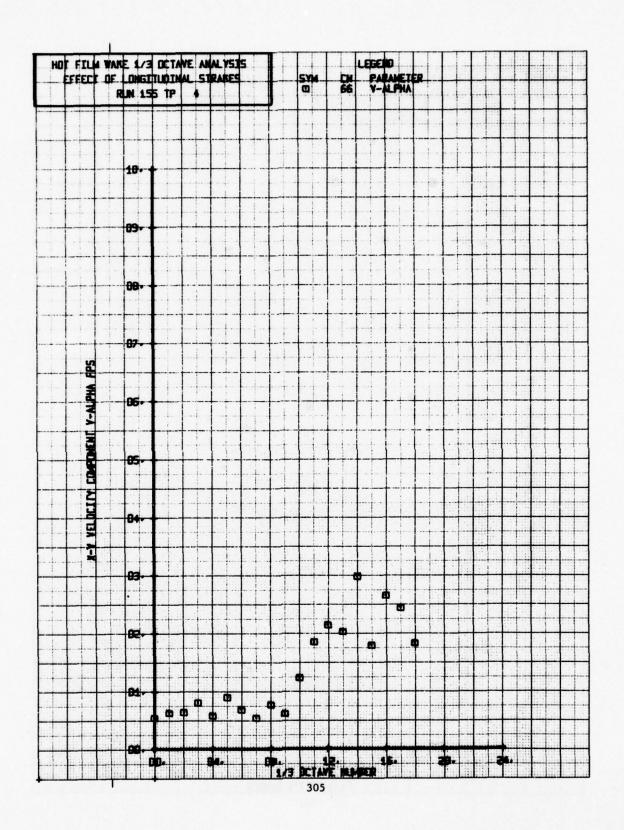


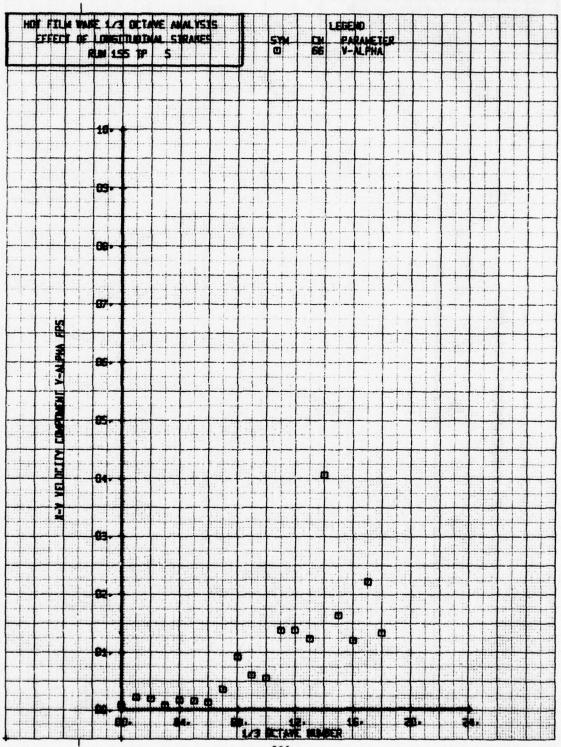


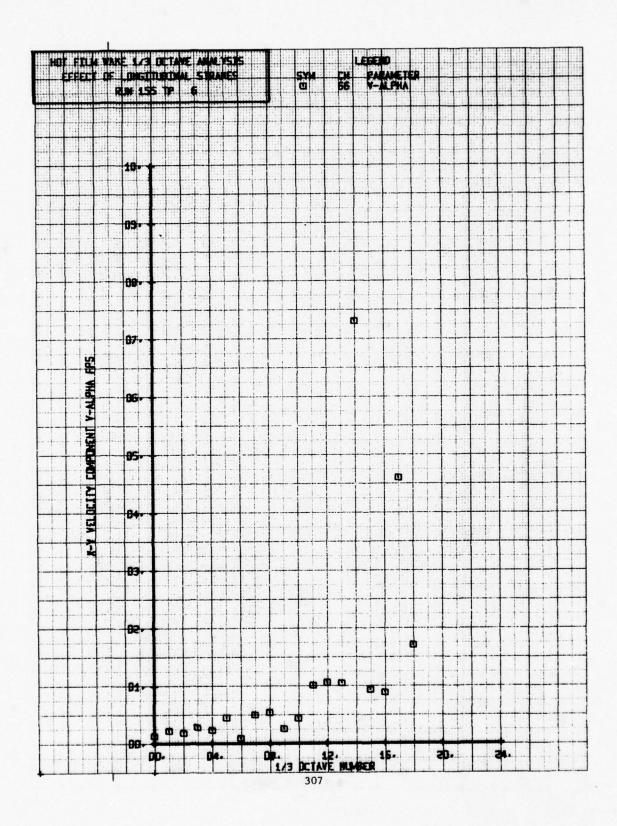


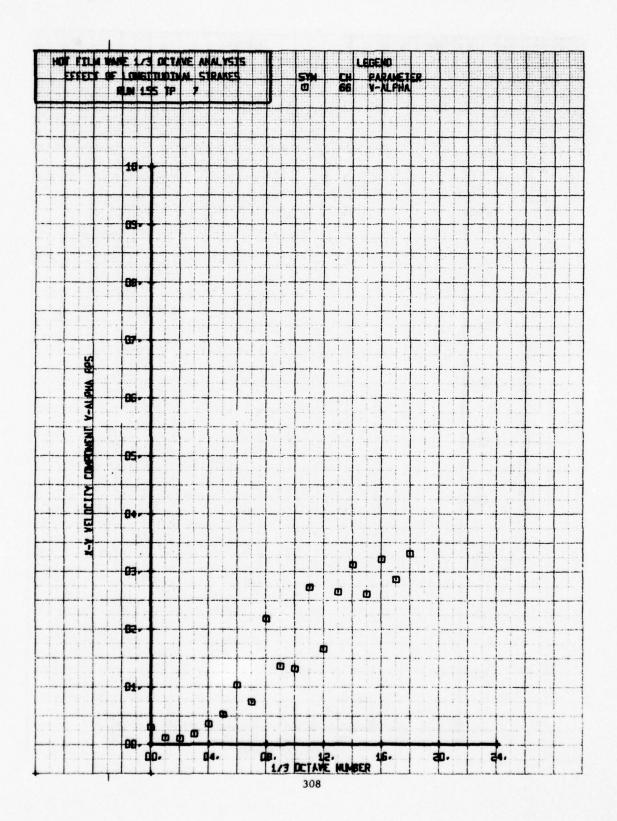
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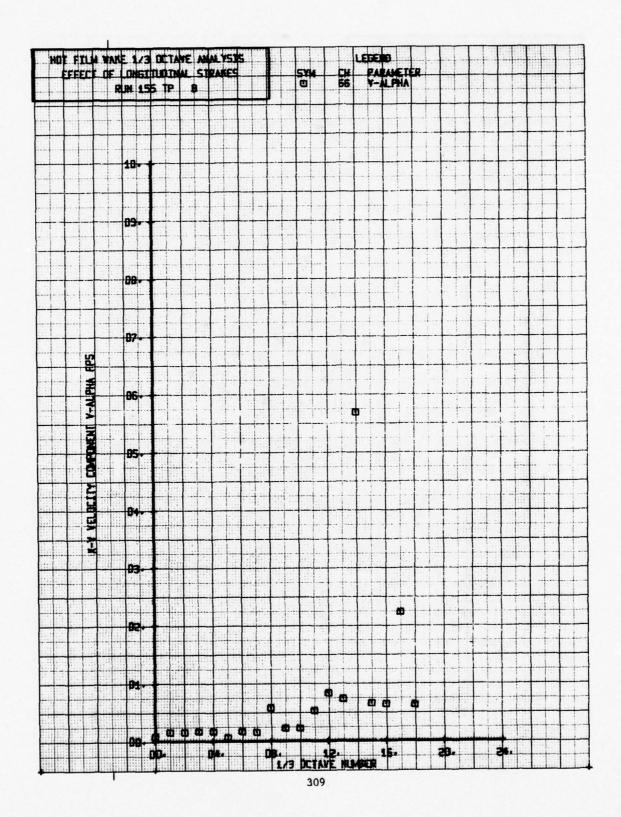


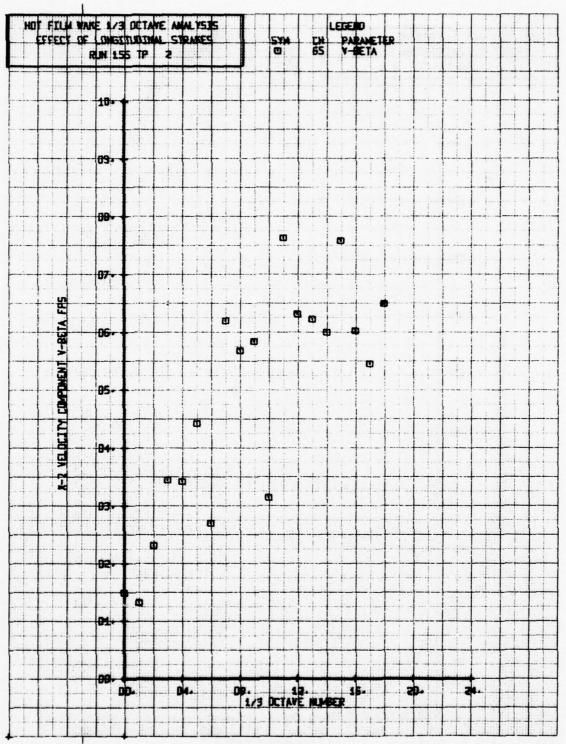


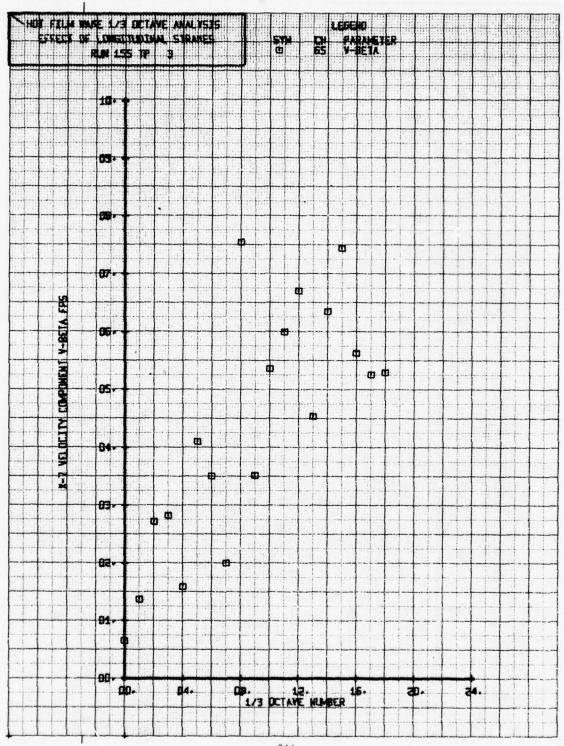


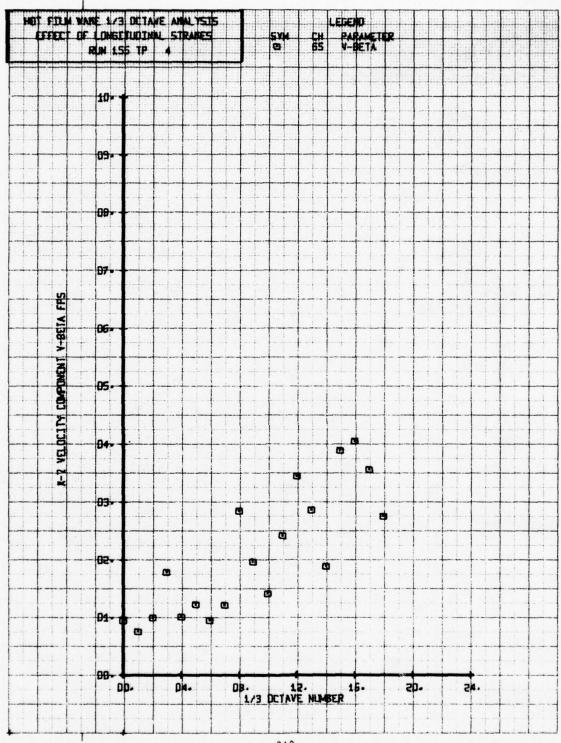


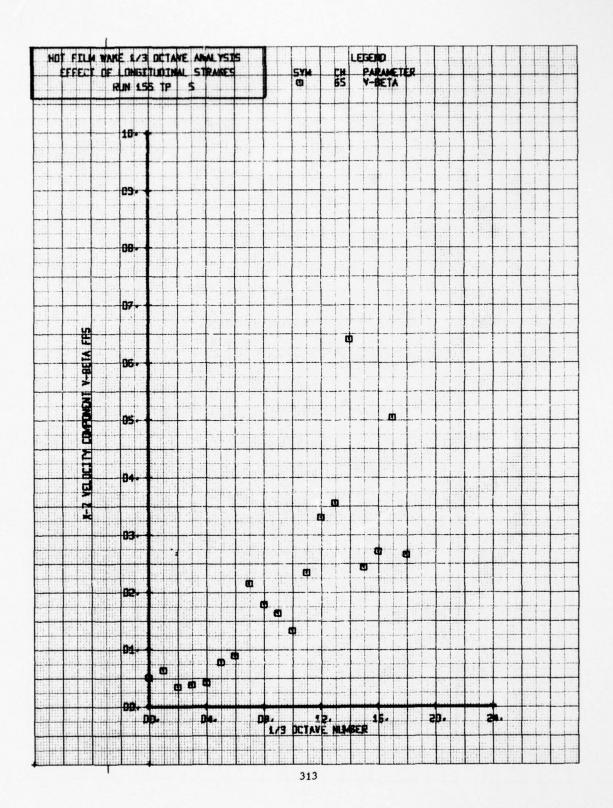


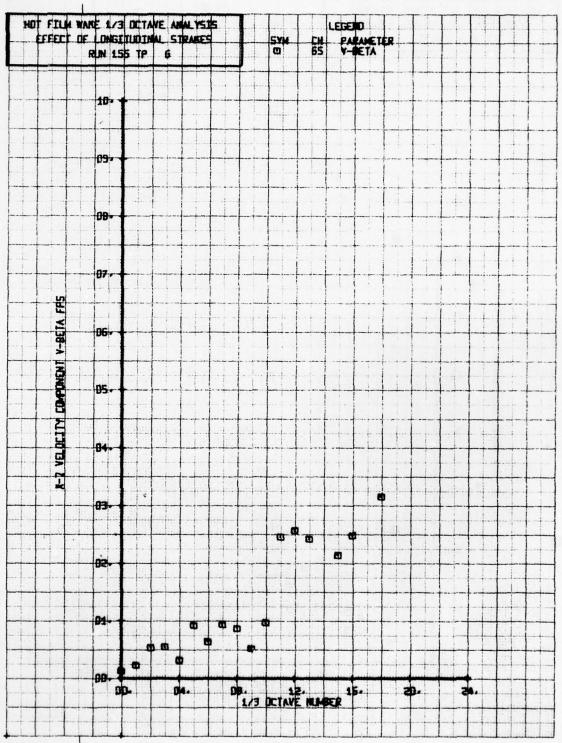


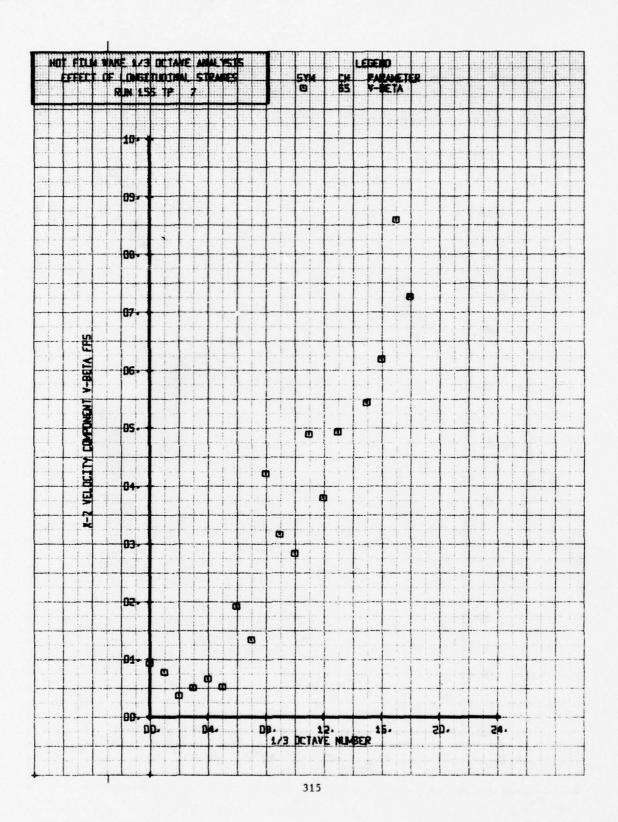


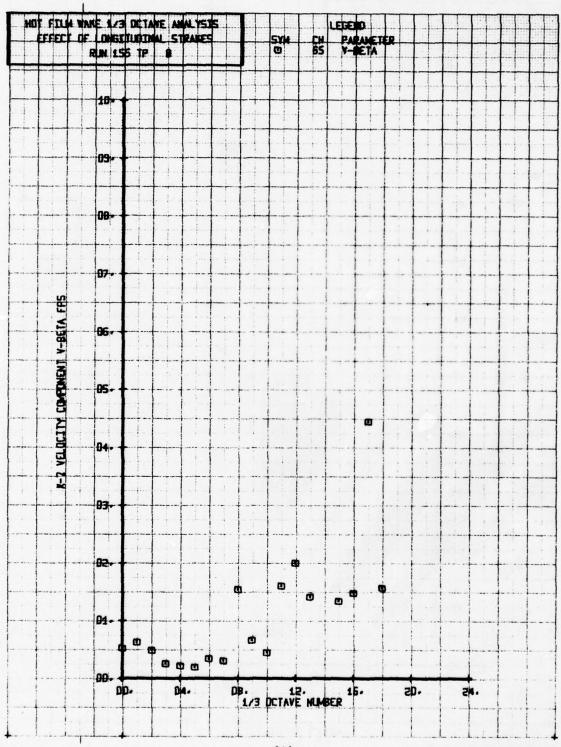


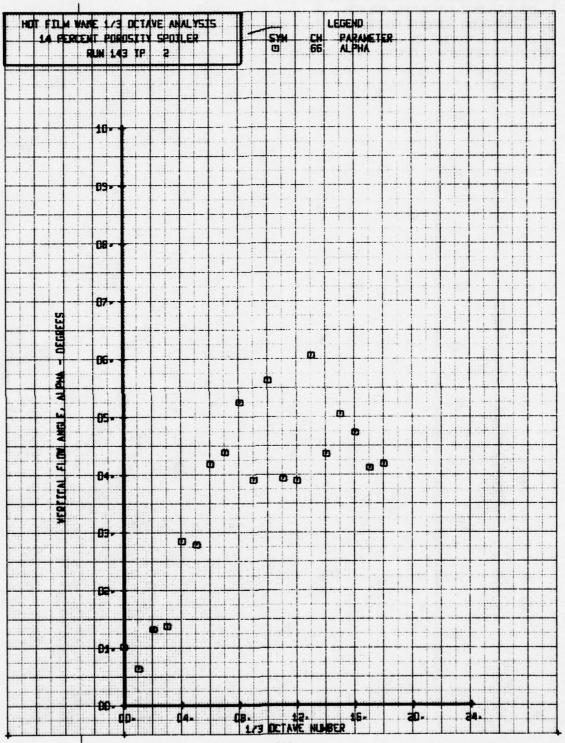


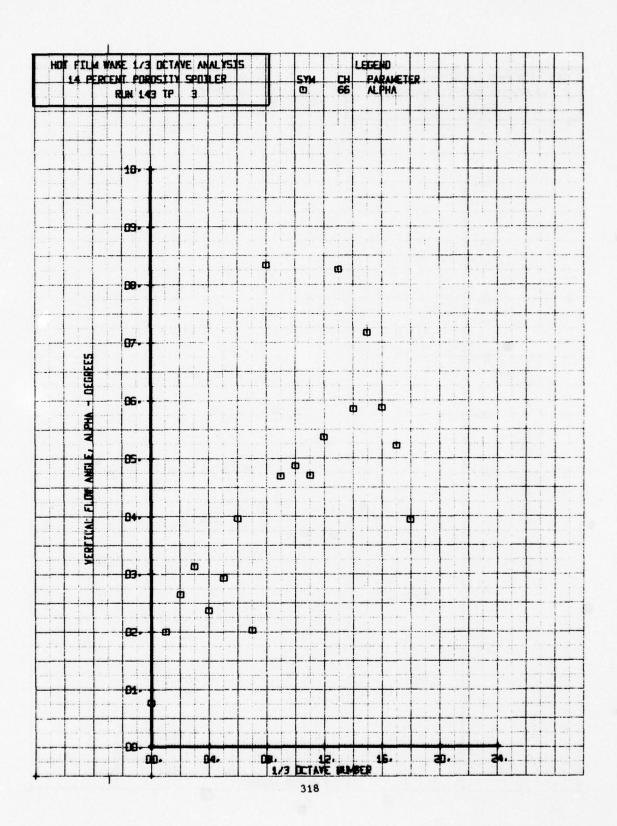


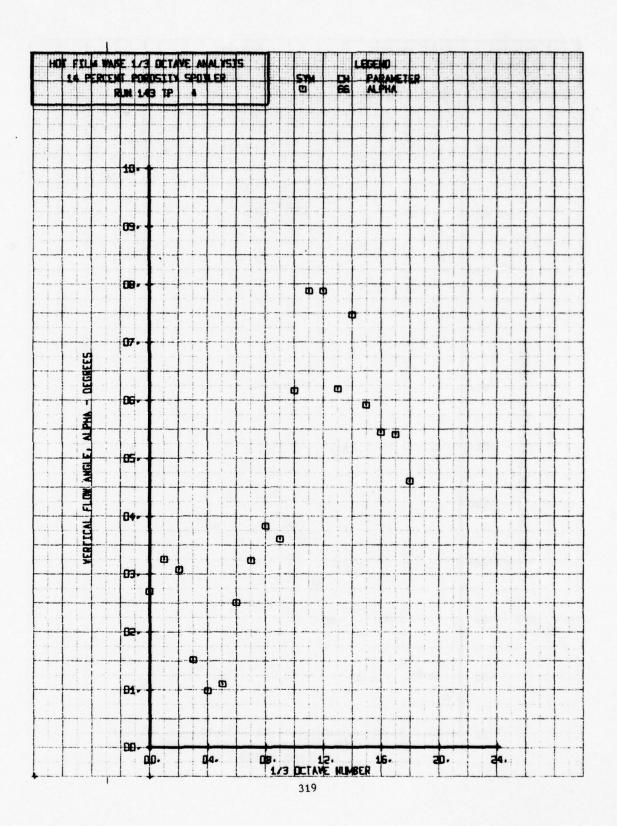


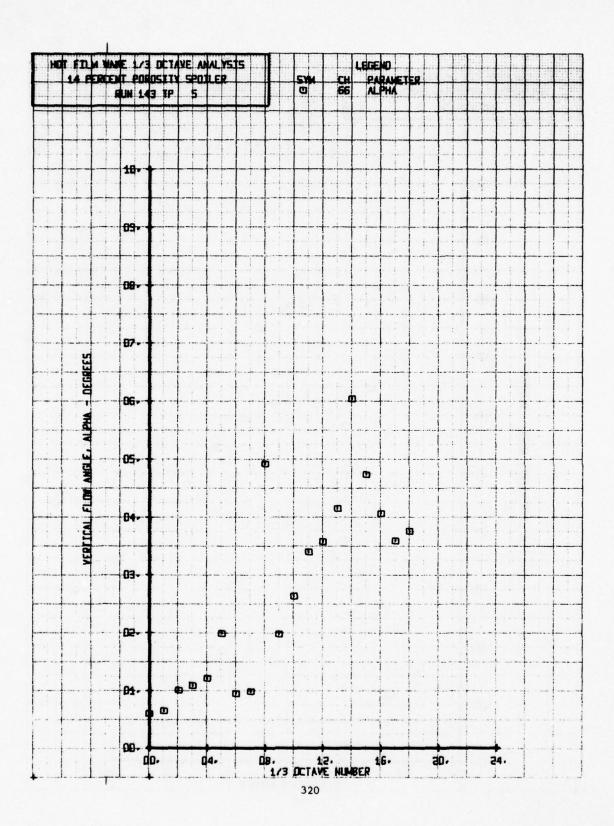


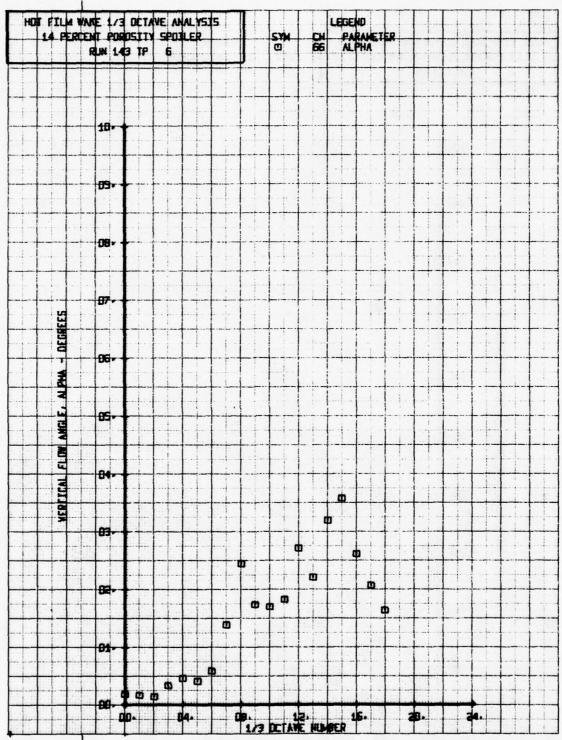


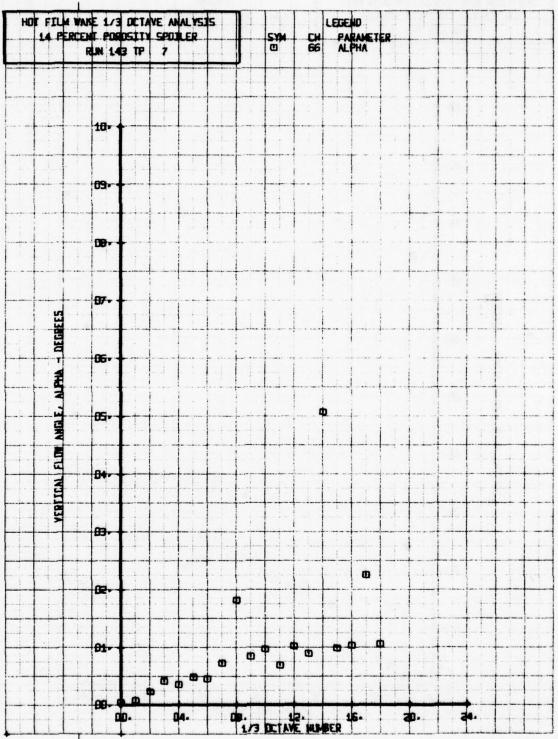


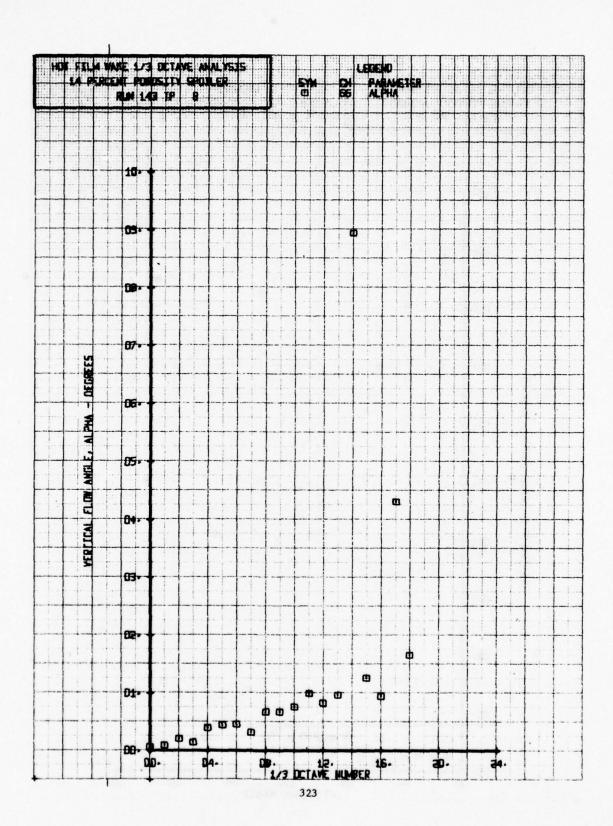


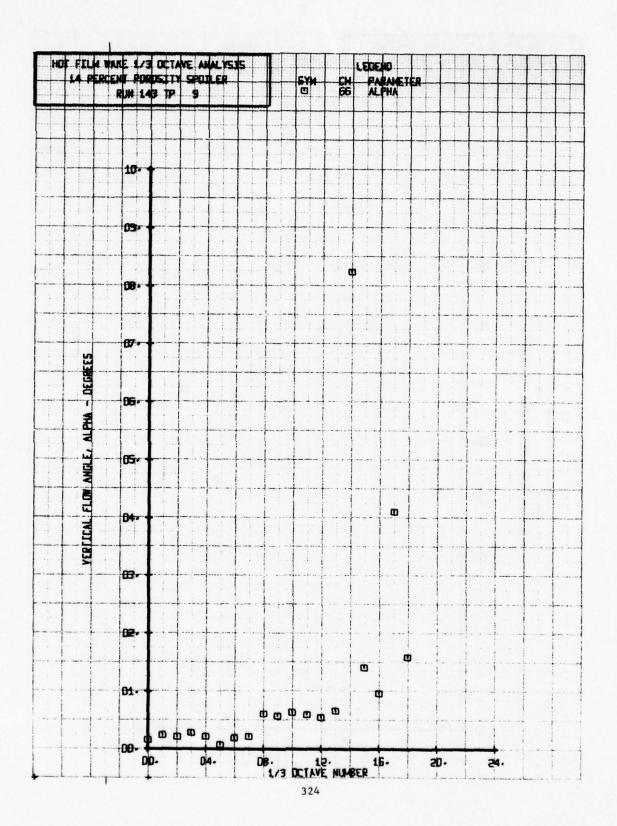


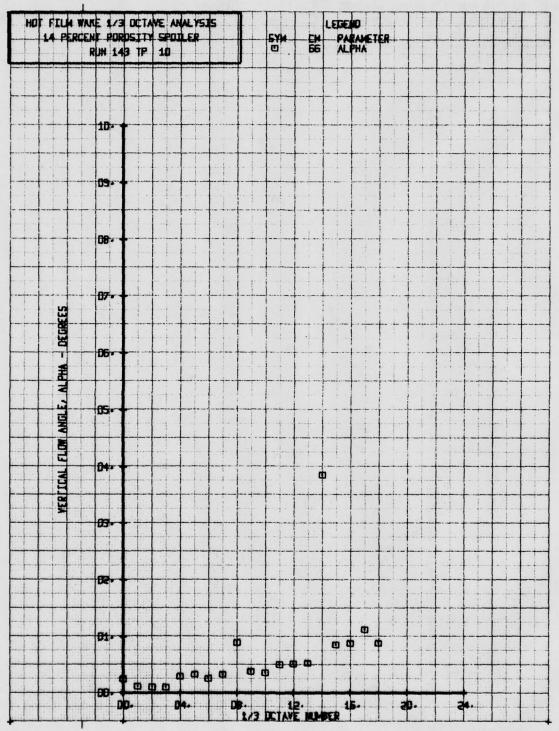


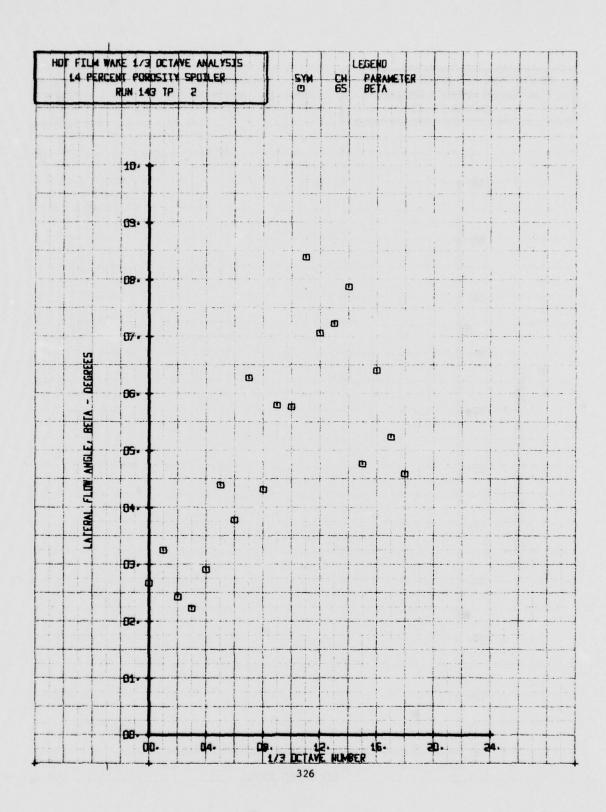


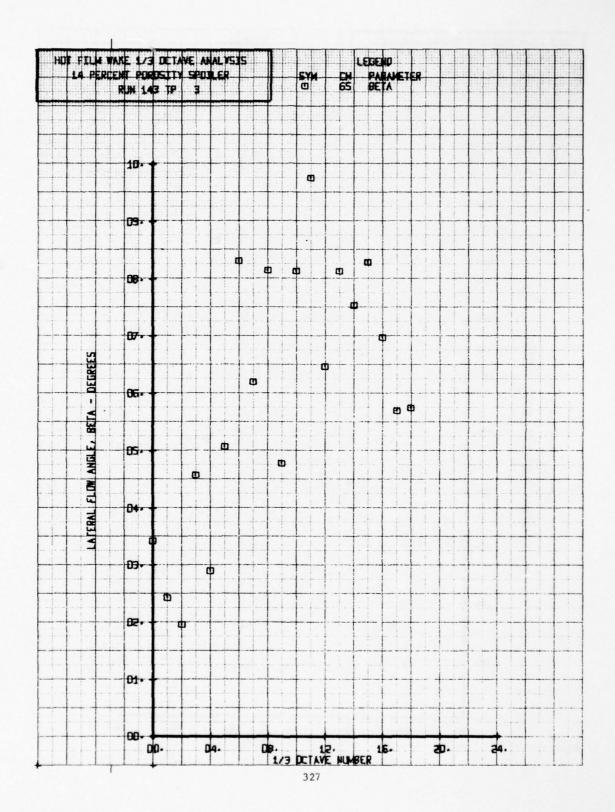


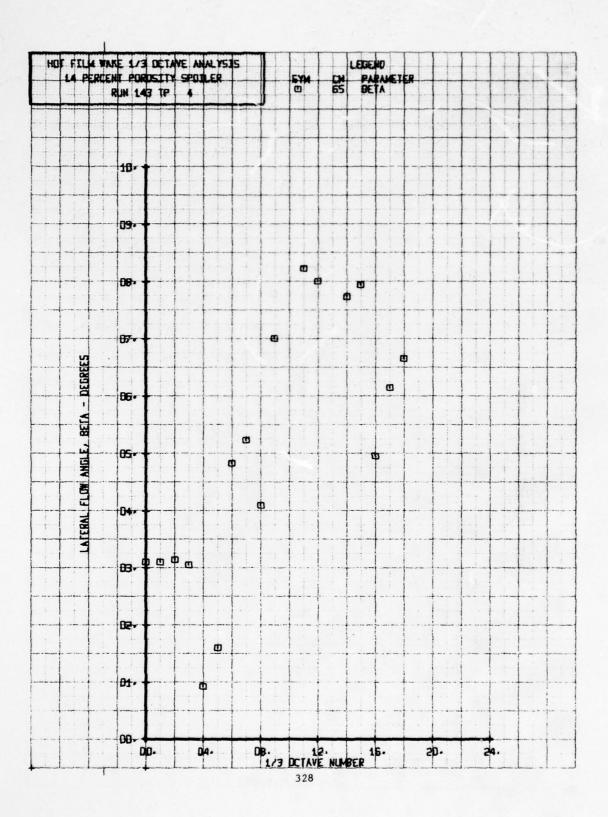


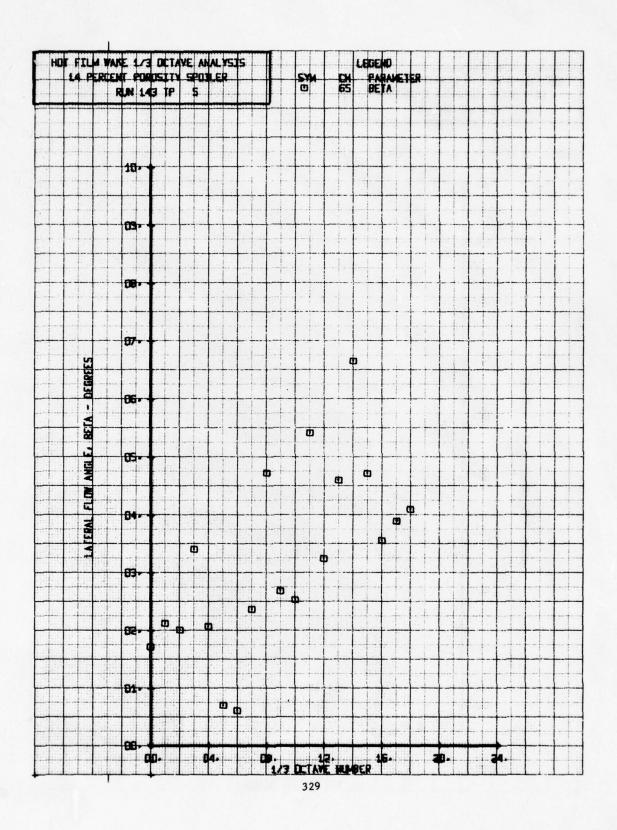


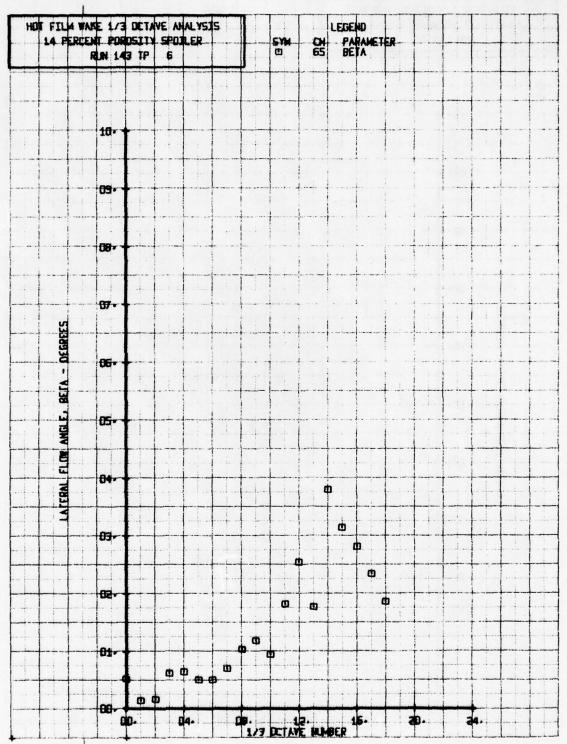


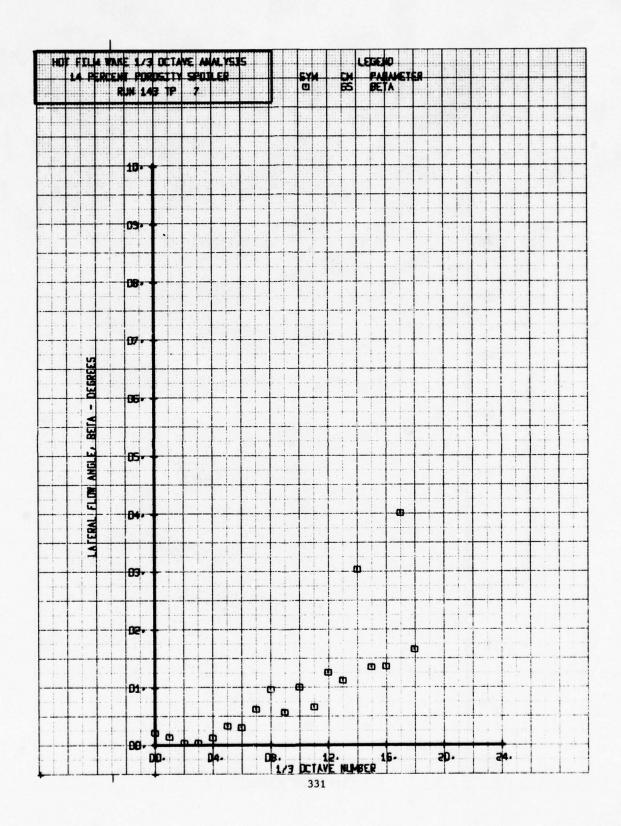


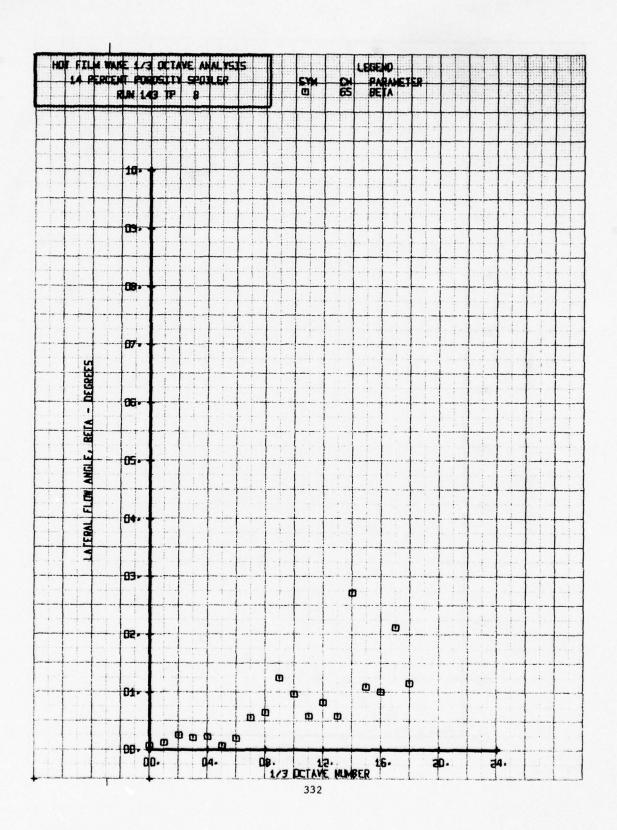


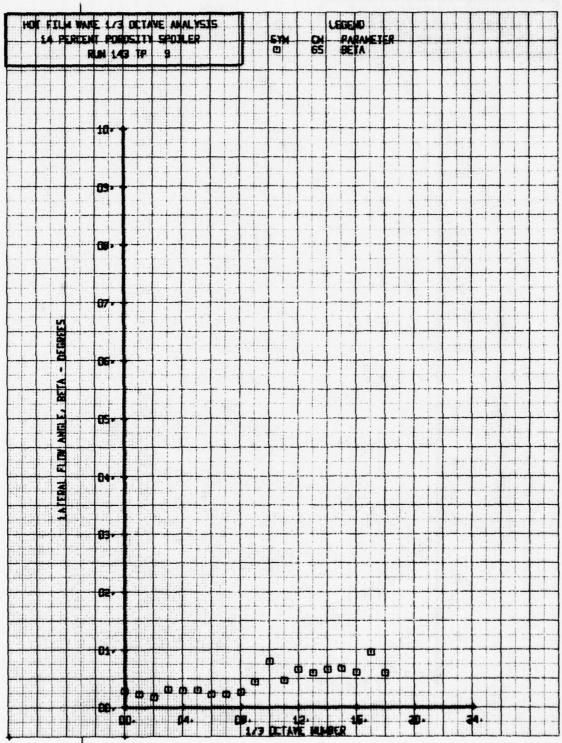


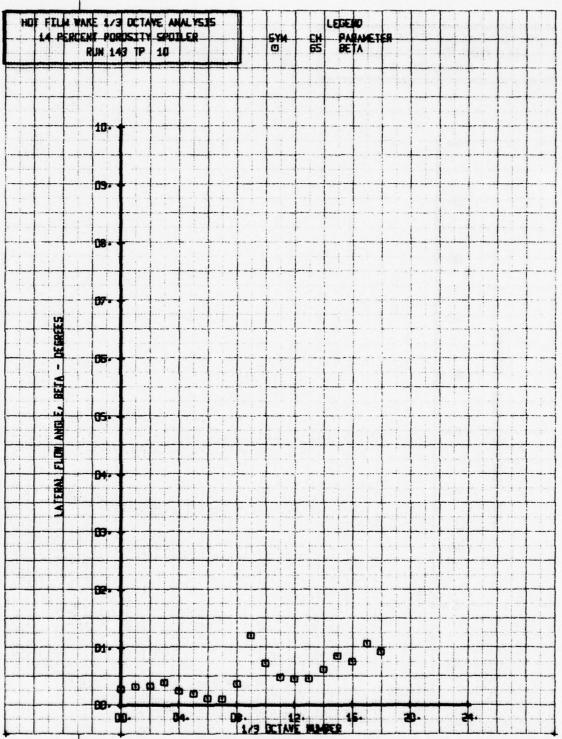


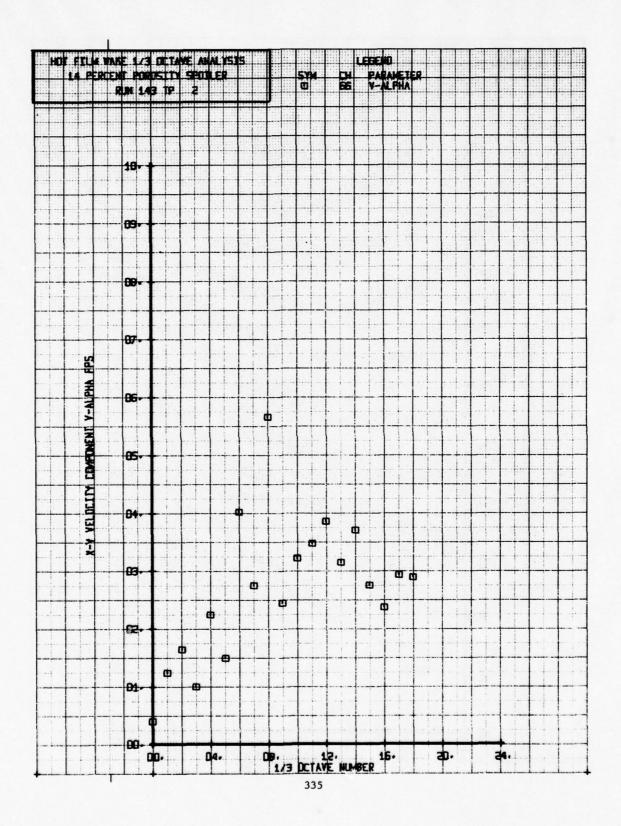


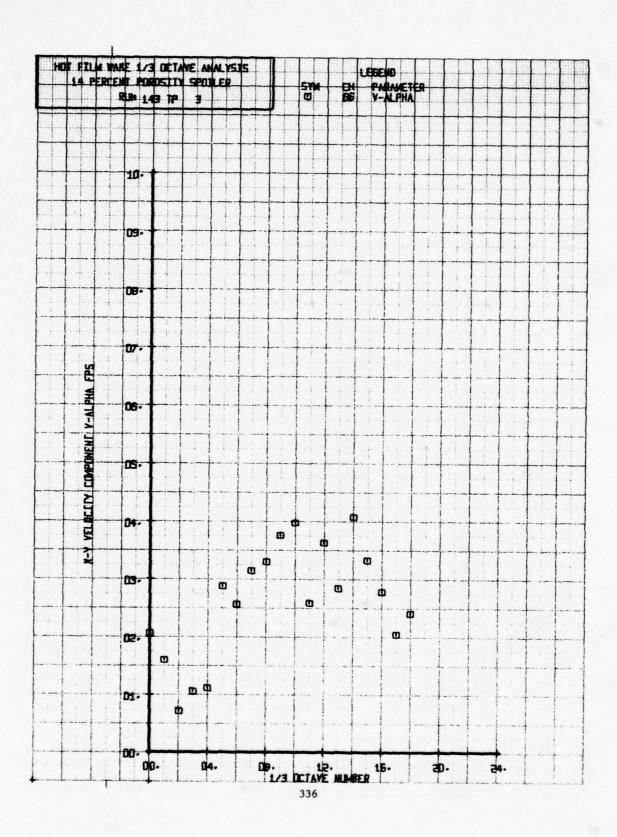


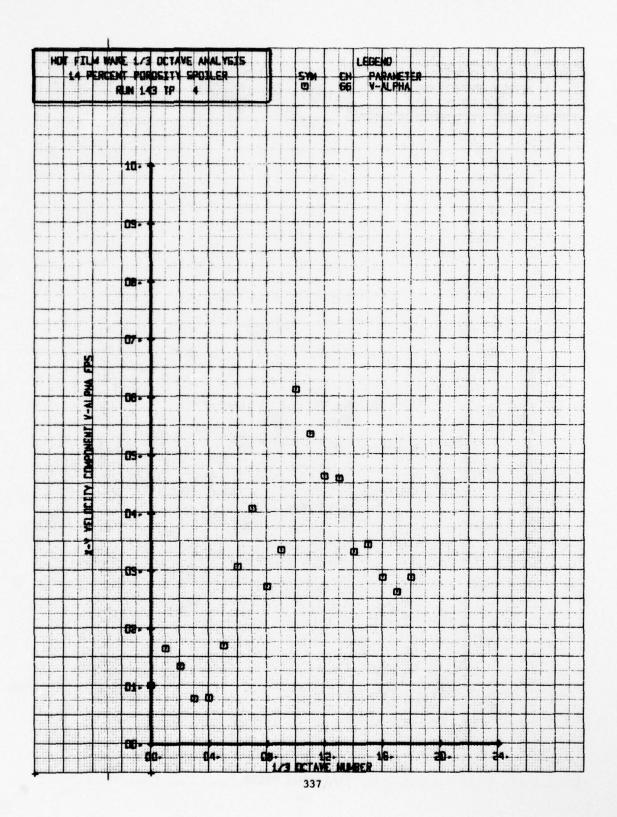


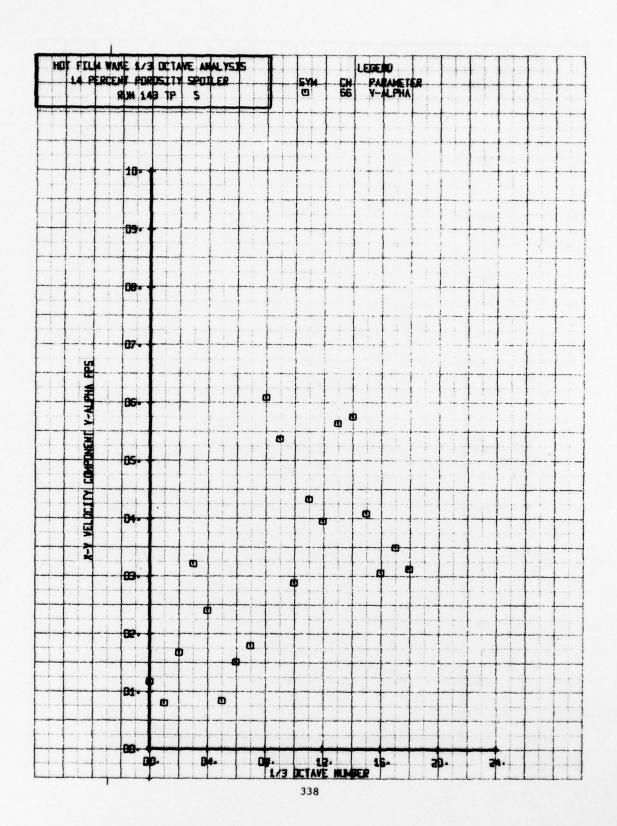


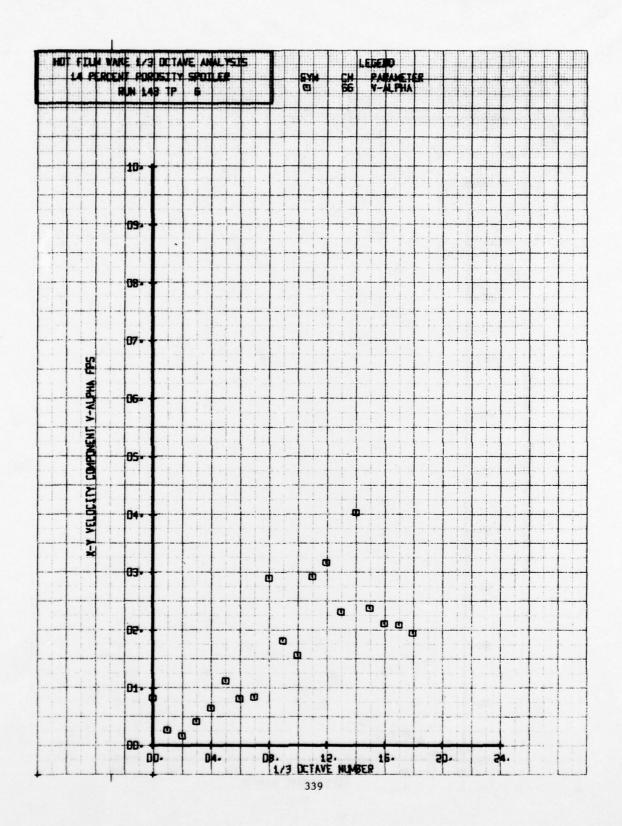


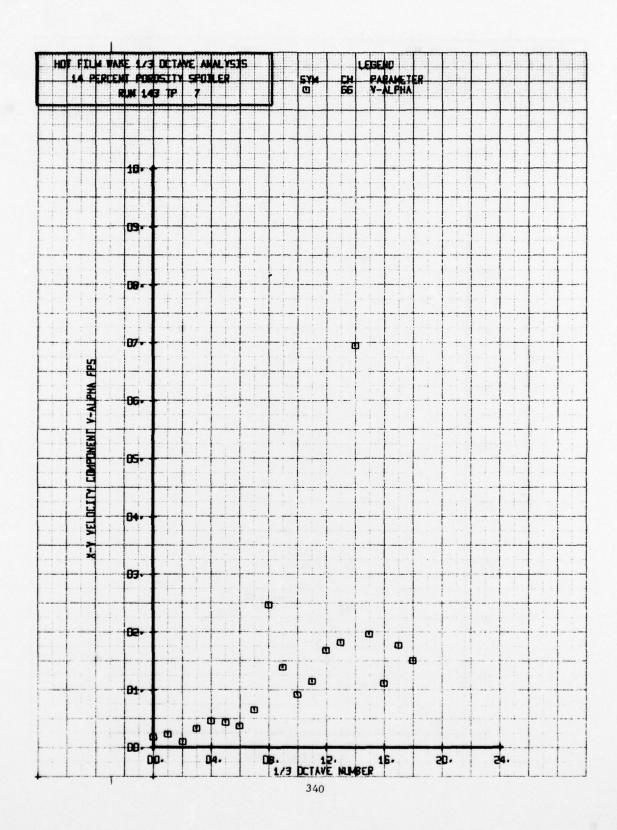


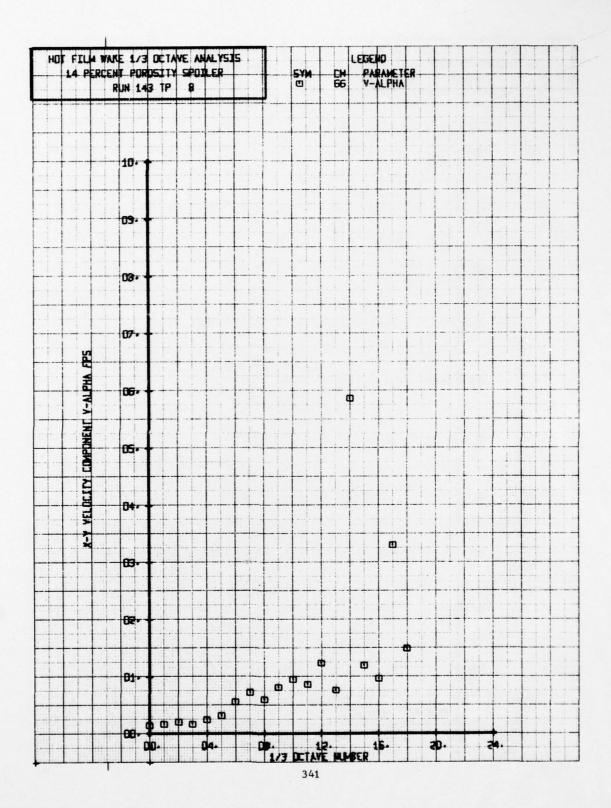


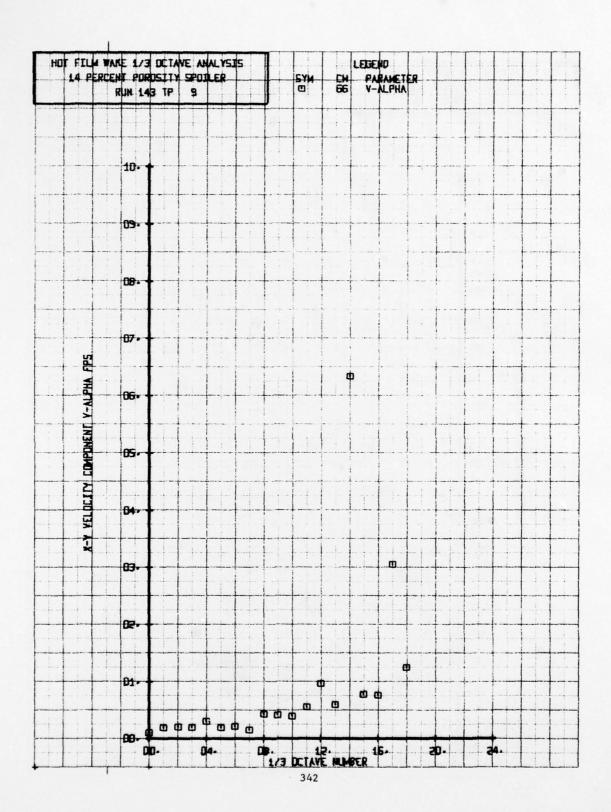


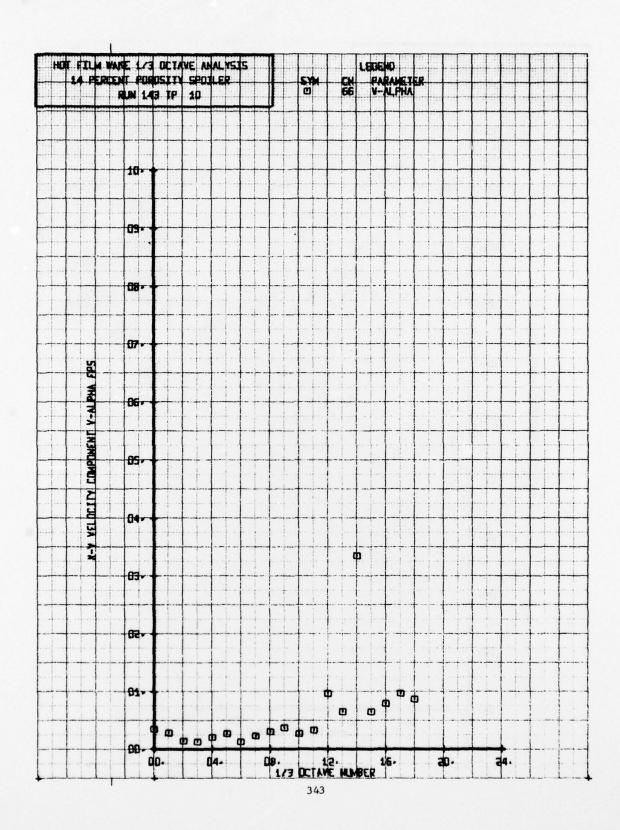


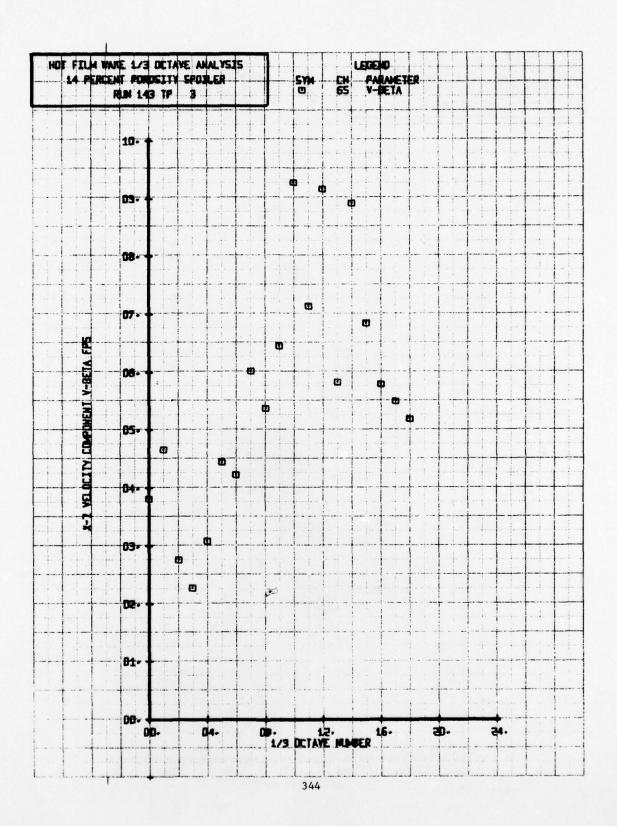


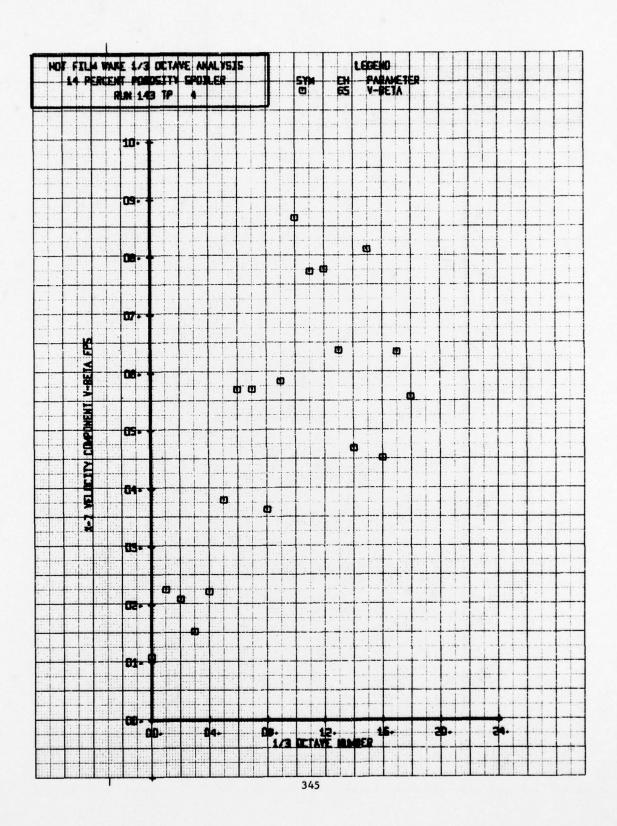


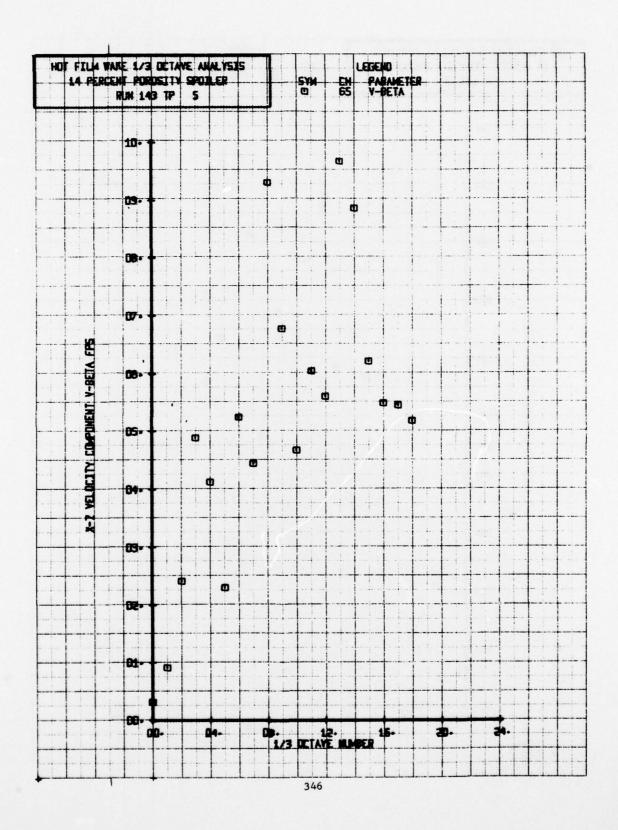


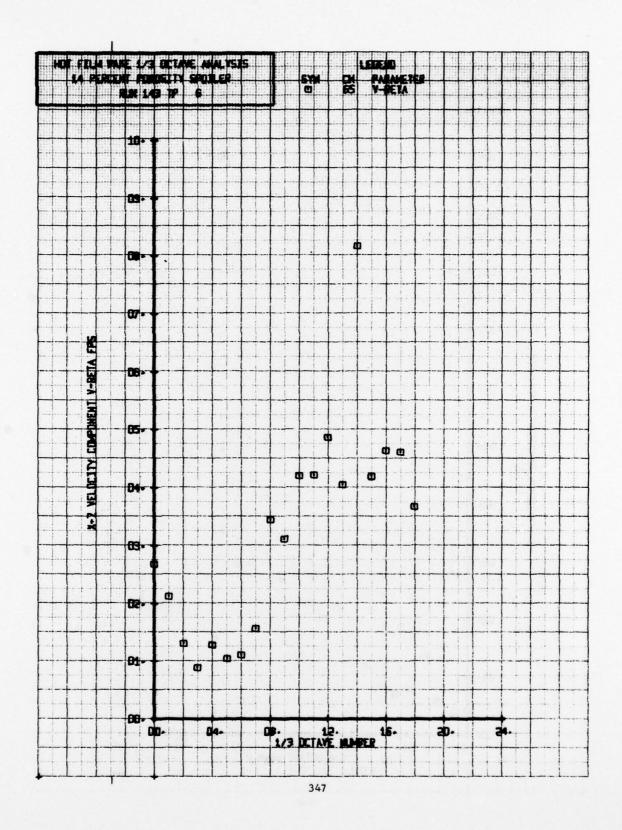


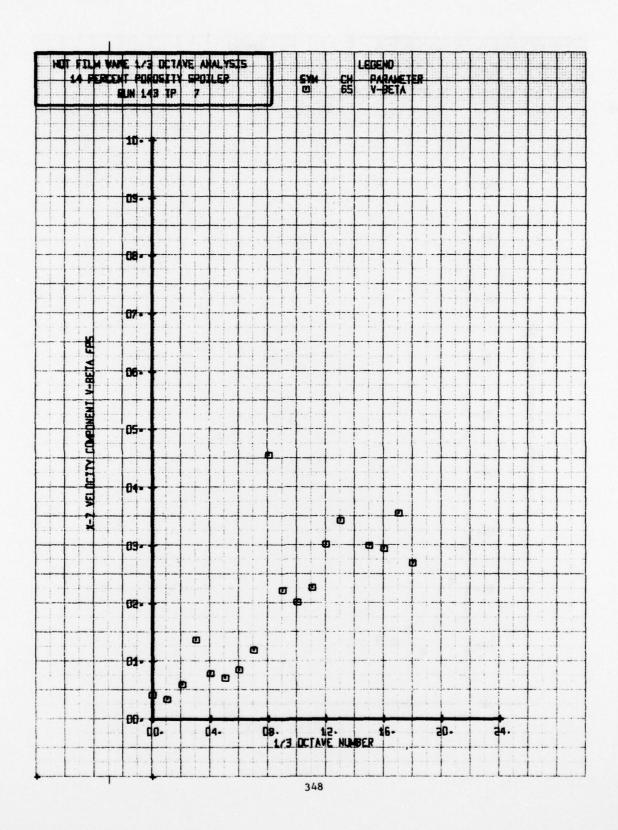


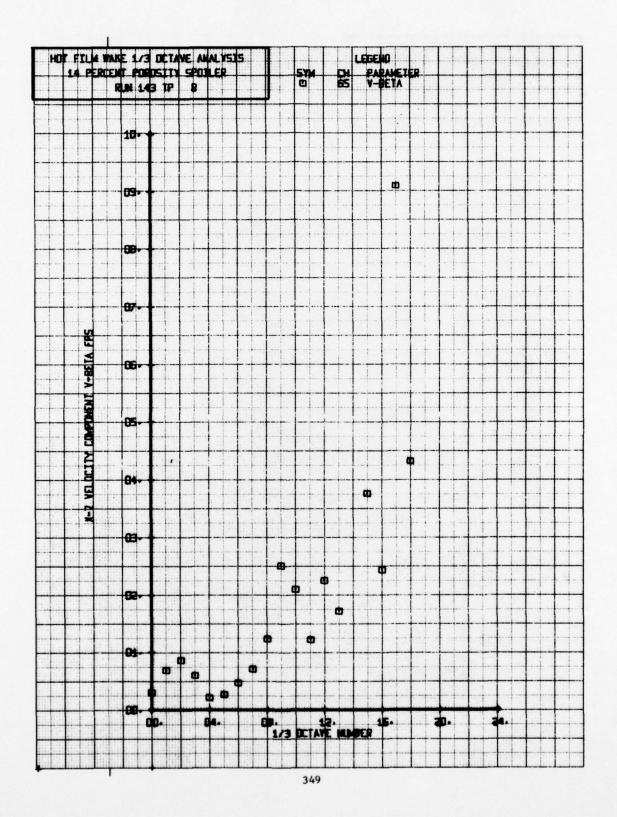


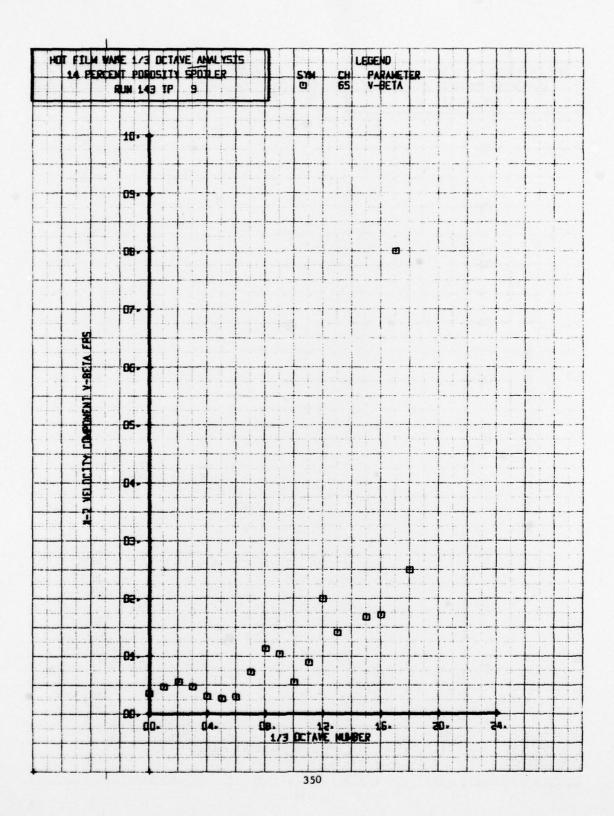


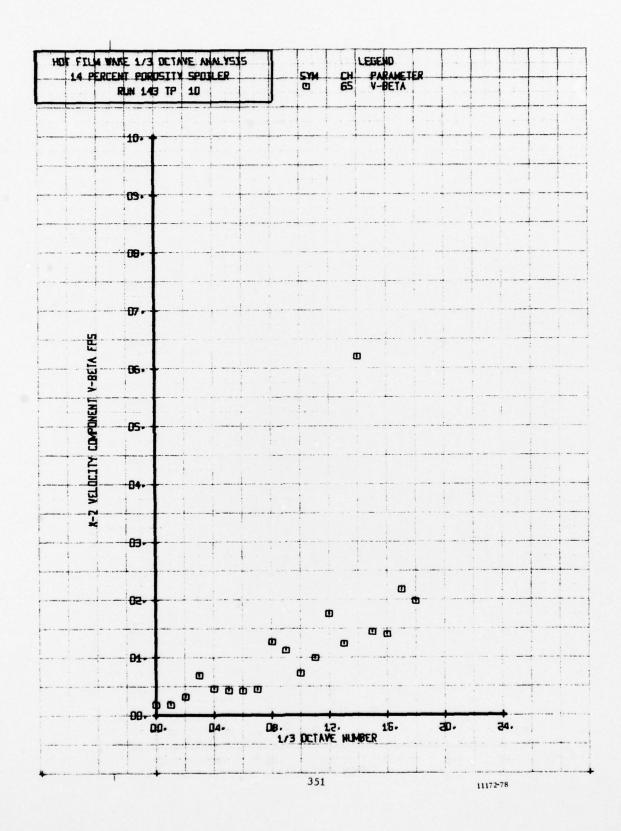












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